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TABLE 2-1

SUMMARY OF OCTOBER 1998 GEOSYNTEC FIELD INVESTIGATION PROGRAM

Boring No.	Drilling				Sampling				Instrumentation and Additional Testing	
	Location (Figure 2-1)	Total Depth	Method	Terminate	Approximate Sequence	No. Shelby Tubes	No. Pitcher Barrel	No. SPT Tests	Piezometers	D-hole Shear Wave
G-1A	Dam centerline (offset 10 ft from G-1B)	60 ft	8" bent. mud rotary	Within dam fill	None	0	0	0	1 in. PVC casing (2 installed)	
G-1B	Dam centerline	114 ft	8" bent. mud rotary	At bedrock surface	SPT - 5' intervals Tubes - 20' intervals	4-shell	1-shell 1-core	12-shell 2-core 1-saprolite	4 in. PVC casing (1 installed)	Within 4 in PVC casing
G-2	Dam centerline	68 ft	8" rotary	At bedrock surface	SPT - 5' intervals Tubes - 20' intervals	2-shell	3-shell	4-shell 1-saprolite	1 in. PVC casing (3 installed)	
G-3	115 ft west of dam centerline, above valley bottom	47 ft	HSA - 4.25" ID	Within dam fill	SPT - 5' intervals Tubes - 15' intervals	5-shell	0	6-shell	1 in. PVC casing (1 installed)	
G-4	235 ft west of dam centerline, above right abutment	55 ft	HSA - 4.25" ID (upper 30 ft) and 4" bent. mud rotary (lower 25 ft)	Within natural soil below dam fill	SPT - 5' intervals Tubes - 15' intervals	2-shell	3-shell	6-shell		
G-5	200 ft east of dam centerline, above left abutment	67 ft	8" bent. mud rotary	Within dam fill	SPT - 5' intervals Tubes - 15' intervals	5-core	1-core	2-shell 7-core		Within 4 in PVC casing

HSA = hollow stem auger, bent. = bentonite, PVC = polyvinyl chloride

TABLE 2-2

SUMMARY OF SPT N-VALUE CORRELATION TO
EFFECTIVE STRESS FRICTION ANGLE

Material	φ' from N - Kulhaway and Mayne, 1990				φ' from (N ₁) ₆₀ - Hatanaka and Uchida, 1996			
	no. tests	minimum	average.	st. deviation	No. tests	minimum	average.	st. deviation
Shell								
G-1B	14	38	41	1	14	38	41	2
G-2	2	36	39	3	2	37	39	3
G-3	5	38	42	3	7	37	40	2
G-4	5	37	40	3	7	35	38	2
G-5	-	-	-	-	1	43	43	-
	total	weighted	weighted	range	total	weighted	weighted	range
	26	avg. 37.7	avg. 40.8	1 to 3	31	avg. 37.2	avg. 40.0	2 to 3
Core								
G-1B	4	34	35	1	4	35	36	1
G-5	14	29	34	3	14	31	35	2
	total	weighted	weighted	range	total	weighted	weighted	range
	18	avg. 30.1	avg. 34.2	1 to 3	18	avg. 31.9	avg. 35.2	1 to 2
Saprolite								
G1-B	2	44	42	0	2	44	44	0

TABLE 3-1

LABORATORY TESTING RESULTS

SPECIMEN IDENTIFICATION			TRIAXIAL SHEAR TESTING										INDEX PROPERTY TESTING						
Test No.	Boring No.	Sample Depth (ft)	Core or Shell Material	Specimen Initial Conditions			Peak Strength Condition			Ultimate Strength Condition			Atterberg Limits		Grain Size Analysis (percent)			USCS Class.	
				Water Content (%)	Dry Unit Weight (pcf)	Effective Consolidation Stress ⁽¹⁾ (psi)	Deviator Stress ⁽²⁾ (psi)	Pore Pressure ⁽³⁾ (psi)	Deviator Stress ⁽²⁾ (psi)	Pore Pressure ⁽³⁾ (psi)	Deviator Stress ⁽²⁾ (psi)	Pore Pressure ⁽³⁾ (psi)	Liquid Limit	Plasticity Index	gravel	sand	silt		clay
A	G-4	47-50	shell	25.9	103.1	41.5	79.0	17.5	113.1	1.6			NP	NP	12	58	23	7	SM
B	G-4	15-16	shell	17.7	97.9	13.6	78.0 ⁽⁴⁾	-4.0	81.3 ⁽⁴⁾	-7.3									
C	G-4	30-32	shell	27.8	97.2	27.2	55.0	14.0	101.2	-8.6									
D	G-1B	20-22	shell	19.1	103.5	18.3	34.5	8.5	48.6	0.3									
E	G-1B	38-40	shell	19.8	104.8	25.7	51.0	10.5	88.3	-7.5			33	3	7	49	41	3	SM
F	G-1B	80-81.5	shell	16.5	108.1	56.5	112.0	24.5	162.6	-7.1			NP	NP	3	61	34	2	SM
G	G-1B	105-107	core	20.7	109.3	68.9	104.0	39.5	165.3	4.0			41	9	4	44	42	10	ML
H	G-5	27-30	core	17.5	114.4	21.0	40.0	10.5	84.8	-8.1			33	9	6	42	35	17	ML
I	G-5	13-15	shell	24.2	105.1	12.9	30.5	4.5	63.6	-9.0									
J	G-5	60-62	core	22.0	104.8	40.9	64.5	24.0	97.8	6.5			45	15	2	40	40	18	ML
K	G-3	15-17	shell	22.5	107.4	13.7	28.0	60.0	63.3	-7.9									
L	G-3	28-30	shell	24.1	98.5	19.8	35.5	10.5	60.7	-0.6									
M	G-2	18-20	shell	23.8	98.3	10.4	26.0	3.5	55.3	-8.1									
N	G-2	38-40	shell	18.7	106.5	27.3	47.0	15.5	81.7	-1.1									
O	G-2	58-60	shell	21.6	106.0	42.6	58.0	25.5	84.7	11.4									
P	G-1B	20-22	shell	16.9 ⁽⁵⁾	102.8 ⁽⁵⁾	18.3 ⁽⁶⁾	49.0	5.0	87.7	-12.7									

- Notes:
- (1) Effective consolidation stress was achieved using back pressures ranging from 49 to 79 psi.
 - (2) Deviator stress is equal to the vertical stress applied to the specimen during shearing.
 - (3) Reported pore pressure is the change in pore water pressure during shearing.
 - (4) During this test excess friction developed in the loading system and reported deviator stresses are believed to be larger than actual values.
 - (5) Test performed on recompacted material.
 - (6) Test specimen initially consolidated to an effective stress of 23.8 psi, then overconsolidated to an effective stress of 18.3 psi.

TABLE 4-1

SUMMARY OF STANDPIPE PIEZOMETER DATA (LAW, INSTALLED 1972)

Piezometer No.	6 Oct 97	13 Oct 97	29 Oct 97	30 Oct 98
L3	1614.01	1613.91	(1613.31)	(1613.31)
L4	1593.02	1593.02	(1593.02)	(1593.02)
L5	1581.89 ⁽¹⁾	1573.99	1580.89	1574.45

Note: ⁽¹⁾ Elevated level likely resulted from poor surface seal.
(1613.31) indicates base of piezometers, piezometer noted to be dry.

TABLE 4-2

SUMMARY OF VIBRATING WIRE PIEZOMETER DATA
(Installed 1997, 1998)

Piezometer No	Water Elevation (ft)																	
	10/17/97	1/14/98	3/19/98	4/20/98	5/19/98	6/12/98	6/19/98	6/26/98	7/2/98	7/10/98	7/16/98	7/24/98	8/21/98	8/28/98	9/4/98	9/11/98	9/18/98	10/23/98
P2-A	4.5	4.0	4.9	3.8	4.0	3.0	2.9	2.8	2.6	2.4	2.4	2.2	2.0	1.9	1.8	1.8	1.8	1.7
P2-B	26.3	25.7	26.7	26.4	26.6	25.6	25.5	25.5	25.2	25.1	24.9	24.9	24.5	24.4	24.2	24.1	24.1	23.8
P2-C	40.1	39.0	40.0	39.7	39.9	39.6	39.7	39.5	39.3	39.1	39.0	38.9	38.4	38.2	38.2	38.2	38.0	37.9
P4-A	4.7	9.1	11.2	11.6	10.4	7.9	7.4	6.9	6.5	6.0	5.6	5.3	4.1	3.7	3.3	3.3	3.0	2.4
P4-B	16.3	19.2	21.5	21.0	20.5	18.7	18.2	17.9	17.7	17.5	17.1	16.7	15.8	15.8	15.4	15.4	15.1	14.5
P4-C	35.6	36.5	38.7	38.0	38.3	37.0	36.7	36.5	36.2	35.9	35.7		34.8	34.8	34.6	34.4	34.4	34.2
P6-A					8.7	8.0	7.5	7.4	7.4	7.0	6.8	6.9	7.4	6.6	6.3	6.3	6.0	6.1
P6-B					16.6	16.6	16.4	16.4	16.3	16.3	16.3	16.0	16.1	16.1	16.0	16.0	15.9	15.8
P6-C					17.3	16.7	16.2	16.0	15.8	15.6	15.4	15.4	15.6	15.0	14.7	14.6	14.3	14.5
P7-A					6.9	6.7	6.3	6.2	6.0	5.8	5.6	5.5	6.7	6.2	5.9	5.8	5.2	5.8
P7-B					12.9	12.2	12.1	12.0	12.0	11.8	11.8	11.8	12.0	11.7	11.6	11.7	11.5	11.9
P7-C					8.8	8.2	7.9	7.8	7.5	7.3	7.2	7.0	7.9	8.0	7.8	7.7	7.8	8.1

TABLE 4-3

SUMMARY OF STANDPIPE PIEZOMETER DATA (GEOSYNTEC, INSTALLED 1998)

Piezometer No.	Elevation			
	10/22/98	10/23/98	10/26/98	10/29/98
G-1A Shallow	1593.68	1593.43	1593.42	1593.67
G-1A Deep	1577.07	1576.93	1576.51	1576.92
G-1B	1580.87 ⁽¹⁾	1583.84	1583.85	1583.89
G-2 Shallow	1566.23	1566.12	1566.06	1566.07
G-2 Intermediate	1558.90	1558.68	1558.81	1559.00
G-2 Deep	1553.41	1553.71	1553.52	1553.75
G-3	1531.94	1531.93	1531.92	1531.95

Note: ⁽¹⁾ This reading may not be representative due to unstabilized conditions.

TABLE 4-4

SUMMARY OF PIEZOMETER ELEVATION VARIATIONS AFTER INITIAL STABILIZATION

Piezometer No.	Water Elevation Variation (ft)																	
	10/17/97	1/14/98	3/19/98	4/20/98	5/19/98	6/12/98	6/19/98	6/26/98	7/2/98	7/10/98	7/16/98	7/24/98	8/21/98	8/28/98	9/4/98	9/11/98	9/18/98	10/23/98
P2-A	0.0	-0.5	0.4	-0.7	-0.5	-1.5	-1.6	-1.7	-1.9	-2.1	-2.1	-2.3	-2.5	-2.6	-2.7	-2.7	-2.7	-2.8
P2-B	0.0	-0.6	0.4	0.1	0.3	-0.7	-0.8	-0.8	-1.1	-1.2	-1.4	-1.4	-1.8	-1.9	-2.1	-2.2	-2.2	-2.5
P2-C	0.0	-1.1	-0.1	-0.4	-0.2	-0.5	-0.4	-0.6	-0.8	-1.0	-1.1	-1.2	-1.7	-1.9	-1.9	-1.9	-2.1	-2.2
P4-A	0.0	4.4	6.5	6.9	5.7	3.2	2.7	2.2	1.8	1.3	0.9	0.6	-0.6	-1.0	-1.4	-1.4	-1.7	-2.3
P4-B	0.0	2.9	5.2	4.7	4.2	2.4	1.9	1.6	1.4	1.2	0.8	0.4	-0.5	-0.5	-0.9	-0.9	-1.2	-1.8
P4-C	0.0	0.9	3.1	2.4	2.7	1.4	1.1	0.9	0.6	0.3	0.1		-0.8	-0.8	-1.0	-1.2	-1.2	-1.4
P6-A					0.0	-0.7	-1.2	-1.3	-1.3	-1.7	-1.9	-1.8	-1.3	-2.1	-2.4	-2.4	-2.7	-2.6
P6-B					0.0	0.0	-0.2	-0.2	-0.3	-0.3	-0.3	-0.6	-0.5	-0.5	-0.6	-0.6	-0.7	-0.8
P6-C					0.0	-0.6	-1.1	-1.3	-1.5	-1.7	-1.9	-1.9	-1.7	-2.3	-2.6	-2.7	-3.0	-2.8
P7-A					0.0	-0.2	-0.6	-0.7	-0.9	-1.1	-1.3	-1.4	-0.2	-0.7	-1.0	-1.1	-1.7	-1.1
P7-B					0.0	-0.7	-0.8	-0.9	-0.9	-1.1	-1.1	-1.1	-0.9	-1.2	-1.3	-1.2	-1.4	-1.0
P7-C					0.0	-0.6	-0.9	-1.0	-1.3	-1.5	-1.6	-1.8	-0.9	-0.8	-1.0	-1.1	-1.0	-0.7

TABLE 6-1**SUMMARY OF MODEL PARAMETERS FOR SEEP/W ANALYSES**

Material Type	Vertical Permeability (ft/s)	Ratio of Horizontal to Vertical Permeability
Shell	3.3×10^{-6}	1, 5, 10
Core	3.3×10^{-8} , 3.3×10^{-7} , 1.6×10^{-6} , 3.3×10^{-6}	1, 5, 10
Upstream Saprolite	3.3×10^{-9}	1
Downstream Saprolite	1.6×10^{-6}	1
Bedrock	3.3×10^{-9}	1
Ball Field Soils	1.6×10^{-6}	1
Internal Drain: Total Head = 1525 ft, 1530 ft, 1535 ft		

TABLE 6-2

SUMMARY OF BEST-FIT MATERIAL PARAMETERS

SEEP/W Analyses of 23 October 1998 and EML Scenarios

Material Type	Vertical Permeability (ft/s)	Ratio of Horizontal to Vertical Permeability
Shell	3.3×10^{-6}	10
Core	1.6×10^{-6}	10
Internal Drain: Total Head = 1535 ft		

TABLE 6-3
COMPARISON OF MEASURED AND
COMPUTED POREWATER PRESSURE HEADS
23 October 1998 Scenario

Piezometer Designation	Computed Pressure Head (ft)	Measured Pressure Head (ft)	Residual Pressure Head (ft)⁽¹⁾
P7A	6.4	5.8	-0.6
P7C	14.9	8.1	-6.8
P7B	23.0	11.9	-11.1
P6A	2.3	6.1	3.8
P6C	7.9	14.5	6.6
P6B	16.9	15.8	-1.1
G2A	3.6	1.0	-2.6
G2B	25.2	29.2	4.0
G2C	34.2	37.3	3.1
P4A	3.0	2.4	-0.6
P4B	19.8	14.5	-5.3
P4C	34.5	34.2	-.3
G1A	3.9	0.3	-3.6
G2B	22.2	10.3	-11.9
G1C	61.8	62.5	0.7
P2A	0.6	1.7	1.1
P2B	19.3	23.8	4.5
P2C	39.8	37.9	-1.9
Average Residual Pressure Head			-1.22

Note: ⁽¹⁾ Residual Pressure Head = Measured Pressure Head – Computed Pressure Head
A negative residual pressure head value indicates an overprediction when compared to measured values.

TABLE 6-4**Comparison of Measured and Computed Porewater Pressure Heads****EML Scenario**

Piezometer Designation	Computed Pressure Head (ft)	Measured Pressure Head (ft)	Residual Pressure Head (ft) ⁽¹⁾
P7A	7.5	6.9	-0.6
P7C	15.8	8.8	-7.0
P7B	23.9	12.9	-11.0
P6A	8.7	8.7	0.0
P6C	11.3	17.3	6.0
P6B	18.6	16.4	-2.2
G2A	8.5	0.0	-8.5
G2B	28.1	31.9	3.8
G2C	36.3	38.3	2.0
P4A	11.6	11.6	0.0
P4B	25.0	21.5	-3.5
P4C	38.6	38.7	0.1
G1A	4.0	0.0	-4.0
G2B	27.3	19.3	-8.0
G1C	65.5	63.5	-2.0
P2A	4.9	4.9	0.0
P2B	23.5	26.7	3.2
P2C	43.5	40.0	-3.5
Average Residual Pressure Head			-1.96

Note: (1) Residual Pressure Head = Measured Pressure Head – Computed Pressure Head
 A negative residual pressure head value indicates an overprediction when compared to measured values.

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TABLE 7-1

MATERIAL PROPERTIES FOR SLOPE STABILITY ANALYSES

Material	Unit Weight		Strength Parameters			
	γ_{moist} (lb/ft ³)	γ_{sat} (lb/ft ³)	Drained		Undrained	
			ϕ' (deg)	c' (lb/ft ²)	ϕ (deg)	c (lb/ft ²)
Shell	125	125	34	0	(1)(2)	(1)(2)
Core	130	130	32	0	(1)	(1)
Saprolite	125	125	35	0	35	0
Rock	150	150	45	10,000	45	10,000

- Note: ⁽¹⁾ Undrained shear strength parameters are described in Section 5. The parameters used for the analysis reflect a strength envelope with a slope of 0.58 and an intercept of 7 psi on a plot of vertical effective stress versus undrained shear strength.
- ⁽²⁾ The parameters used for surficial stability analysis were taken as equal to the drained strength parameters, as discussed in Section 5.2.1.

TABLE 7-2

SLOPE STABILITY ANALYSES RESULTS
MINIMUM CALCULATED FACTORS OF SAFETY
DOWNSTREAM EMBANKMENT STABILITY

Loading Condition	Porewater Pressure Scenario	
	EML	Post-Rehabilitation
Steady-State	1.52	1.74
Seismic	1.46	Not calculated ⁽¹⁾

cannot believe this

Note: ⁽¹⁾ The minimum calculated factor of safety for the seismic loading condition with the post-rehabilitation porewater pressure scenario would, if calculated, exceed the value of 1.46 obtained for the EML porewater pressure scenario.

TABLE 8-1

SUMMARY OF PRIMARY EVALUATION
PRIMARY EVALUATION CRITERIA

Rehabilitation Measure	Improvement to Minimum F.S.	Constructibility	Schedule	Ability to Monitor Effectiveness	Capital Cost	O&M Cost	Total Score	Comments
Drainage								
Toe Drains	1	2	5	4	4	4	20	Reject
Buttress Drains	1	4	5	4	4	3	21	Retain
Pressure Relief Wells	3	4	4	4	3	1	19	Reject
Trench Drains	4	4	4	4	4	4	24	Retain
Horizontal Wells	3	3	3	3	3	3	18	Reject
Top Buttress								
Earth Fill	5	4	1	4	2	4	20	Retain for Comparison
Reinforced Soil or Rock	5	3	2	4	2	3	19	Reject
Retaining Wall and Backfill	3	3	3	4	1	4	18	Reject

TABLE 8-1 (continued)

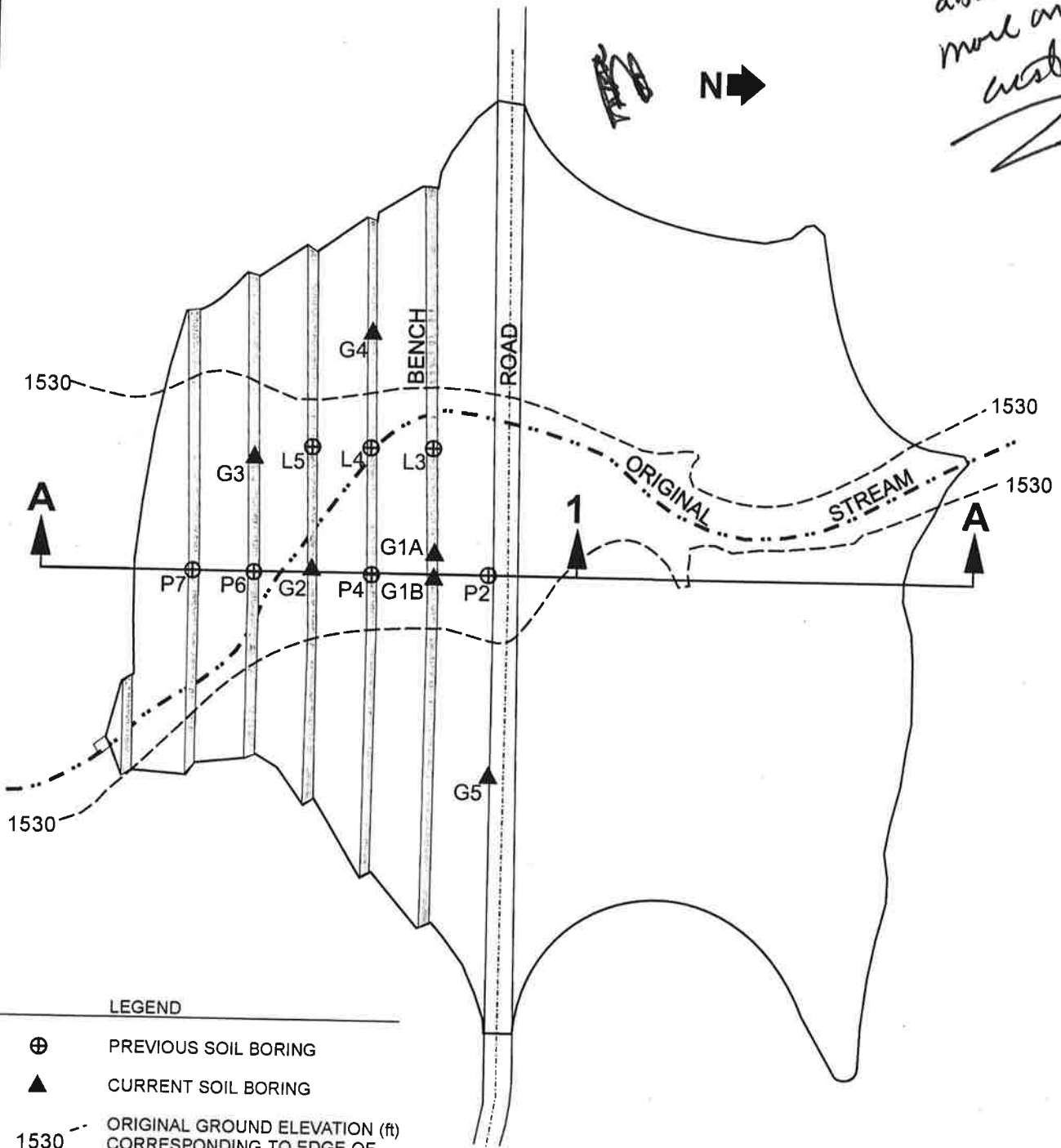
SUMMARY OF PRIMARY EVALUATION
PRIMARY EVALUATION CRITERIA

Rehabilitation Measure	Improvement to Minimum F.S.	Constructibility	Schedule	Ability to Monitor Effectiveness	Capital Cost	O&M Cost	Total Score	Comments
Seepage Cutoff								
Grouting	1	2	2	3	2	3	13	Reject
Subsurface Barrier	4	2	1	4	1	4	16	Reject
Upgradient Impermeable Barrier	2	1	2	4	2	2	13	Reject
Infiltration Control								
Impermeable Membrane (entire slope)	2	4	4	3	2	3	18	Reject
Surface Water Drainage	1	5	5	3	4	5	23	Retain
Paved Benches	2 ⁽¹⁾	5	5	3	3	5	23	Retain

Notes: (1) Significant depth required to provide required factors of safety.

PETIT COVE DAM PLAN VIEW

*Look @
abutments
more on
sheet
2*



LEGEND

- ⊕ PREVIOUS SOIL BORING
- ▲ CURRENT SOIL BORING

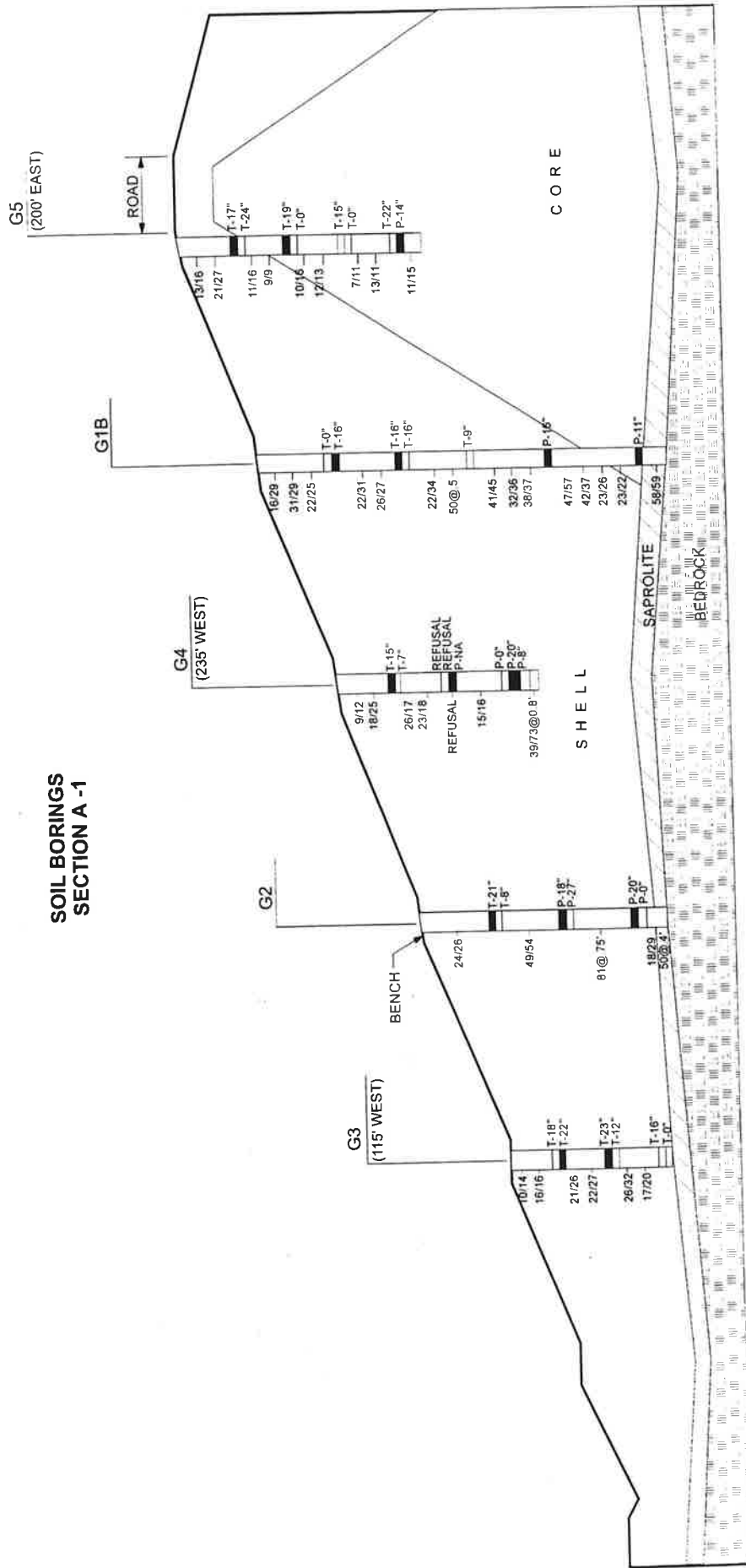
1530 --- ORIGINAL GROUND ELEVATION (ft)
CORRESPONDING TO EDGE OF
VALLEY BOTTOM



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FIGURE NO.	2-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	Plan.cdr

SOIL BORINGS SECTION A -1



- LEGEND**
- 10/14 10 = SUM OF 2ND AND 3RD SPT* BLOWCOUNTS
 - 14 = SUM OF 3RD AND 4TH SPT* BLOWCOUNTS
 - T-18" T = SHELBY TUBE SAMPLE
 - P-18" P = PITCHER BARREL SAMPLE
 - 18" = SAMPLE RECOVERY
 - NA NOT AVAILABLE
 - SAMPLE USED FOR LABORATORY TRIAXIAL SHEAR TESTING
 - * STANDARD PENETRATION TEST

NOTE:
BORINGS SHOWN FROM GEOSYNTEC
FIELD INVESTIGATION PROGRAM, OCTOBER 1998

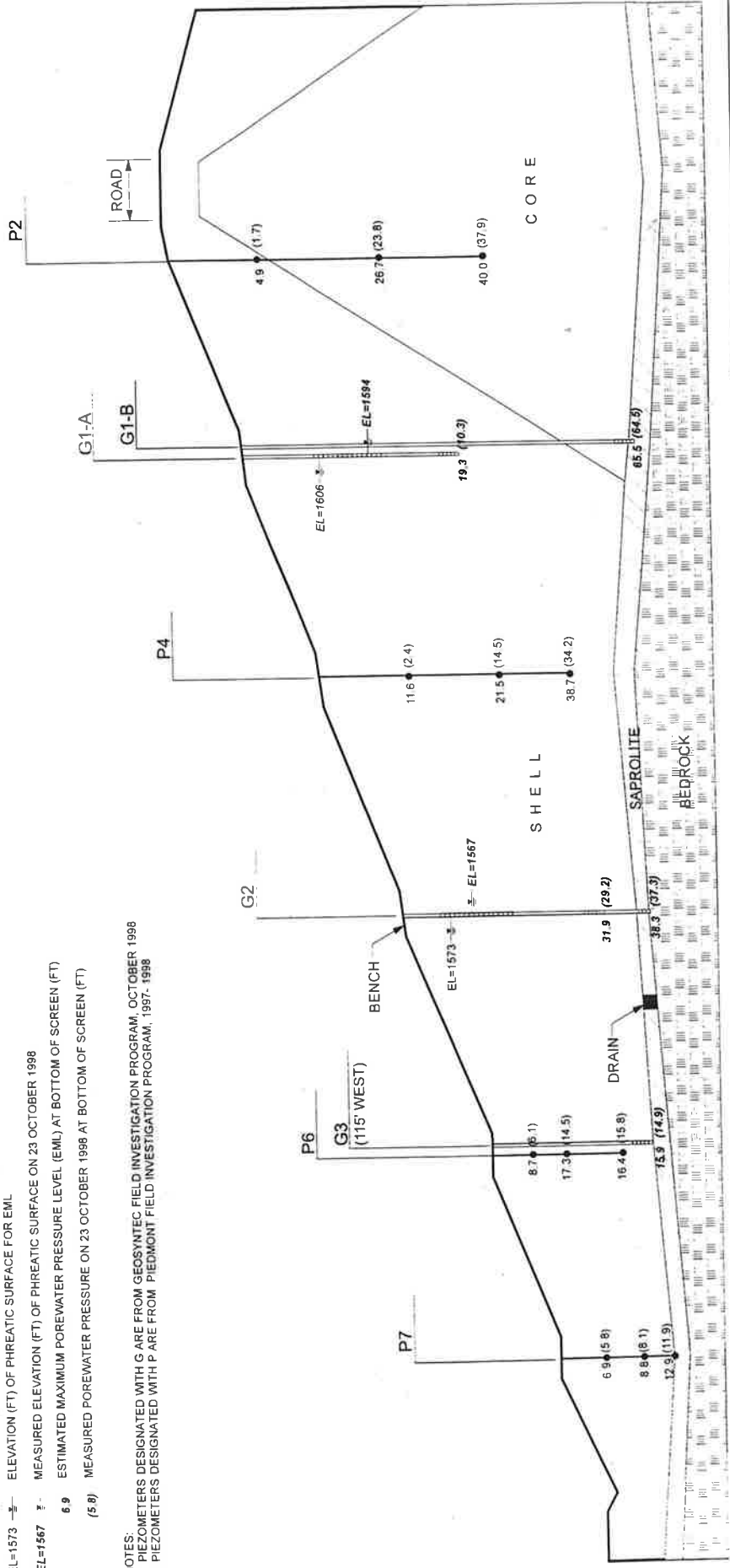
GEOSYNTEC CONSULTANTS
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PROJECT NO.	GL 0625-15	FIGURE NO.	2-2
DOCUMENT NO.	GA981181	FILE NO.	SEC-A CDR

PIEZOMETER LOCATIONS AND MEASUREMENTS SECTION A - 1

- LEGEND**
- VIBRATING WIRE PIEZOMETER
 - 6.9 ESTIMATED MAXIMUM POREWATER PRESSURE LEVEL (EML) (FT)
 - (5.8) MEASURED POREWATER PRESSURE ON 23 OCTOBER 1998 (FT)
 - ▬ SCREEN INTERVAL FOR STANDPIPE PIEZOMETER
 - EL=1573 → ELEVATION (FT) OF PHREATIC SURFACE ON 23 OCTOBER 1998
 - EL=1567 → MEASURED ELEVATION (FT) OF PHREATIC SURFACE ON 23 OCTOBER 1998
 - 6.9 ESTIMATED MAXIMUM POREWATER PRESSURE LEVEL (EML) AT BOTTOM OF SCREEN (FT)
 - (5.8) MEASURED POREWATER PRESSURE ON 23 OCTOBER 1998 AT BOTTOM OF SCREEN (FT)

NOTES:
 1. PIEZOMETERS DESIGNATED WITH G ARE FROM GEOSYNTEC FIELD INVESTIGATION PROGRAM, OCTOBER 1998
 2. PIEZOMETERS DESIGNATED WITH P ARE FROM 'PIEDMONT FIELD INVESTIGATION PROGRAM', 1997-1998

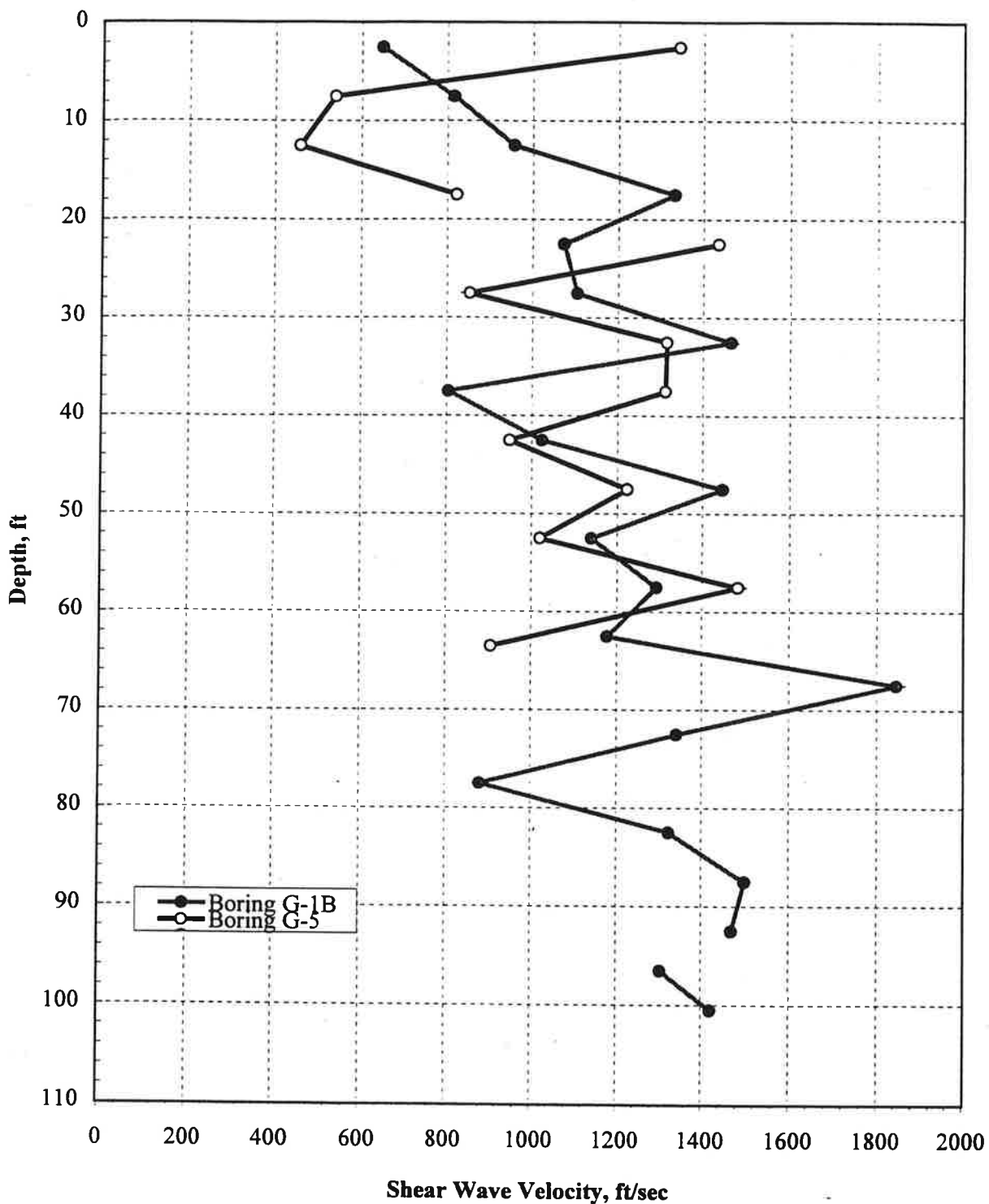




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PROJECT NO. GL0625-15	FIGURE NO. 2-3	FILE NO. SEC-A3 CD
DOCUMENT NO. GA981181		

SHEAR WAVE VELOCITY PROFILES

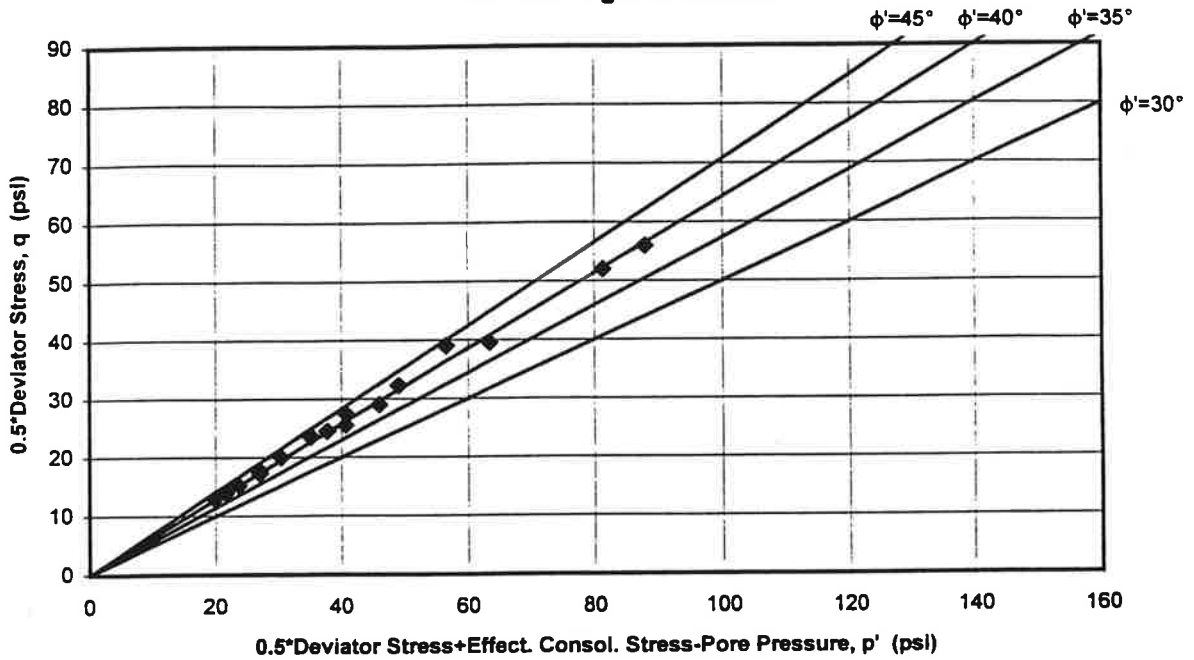


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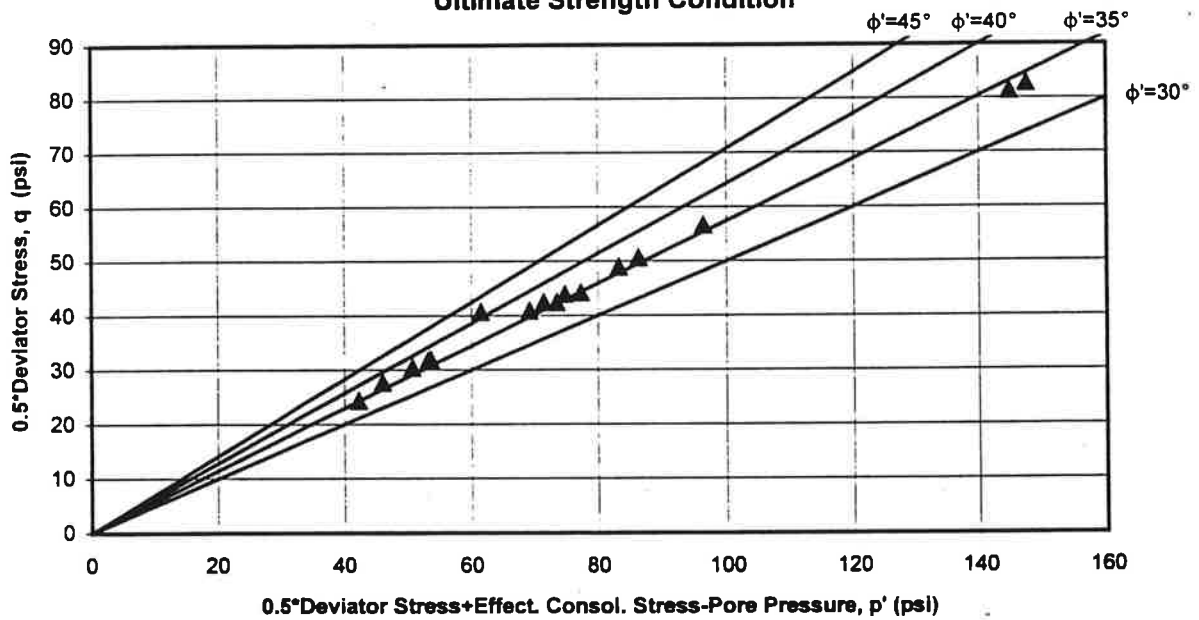
FIGURE NO.	2-4
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

TRIAXIAL SHEAR TESTING RESULTS EFFECTIVE STRESS SHEAR STRENGTH PARAMETERS

Peak Strength Condition



Ultimate Strength Condition



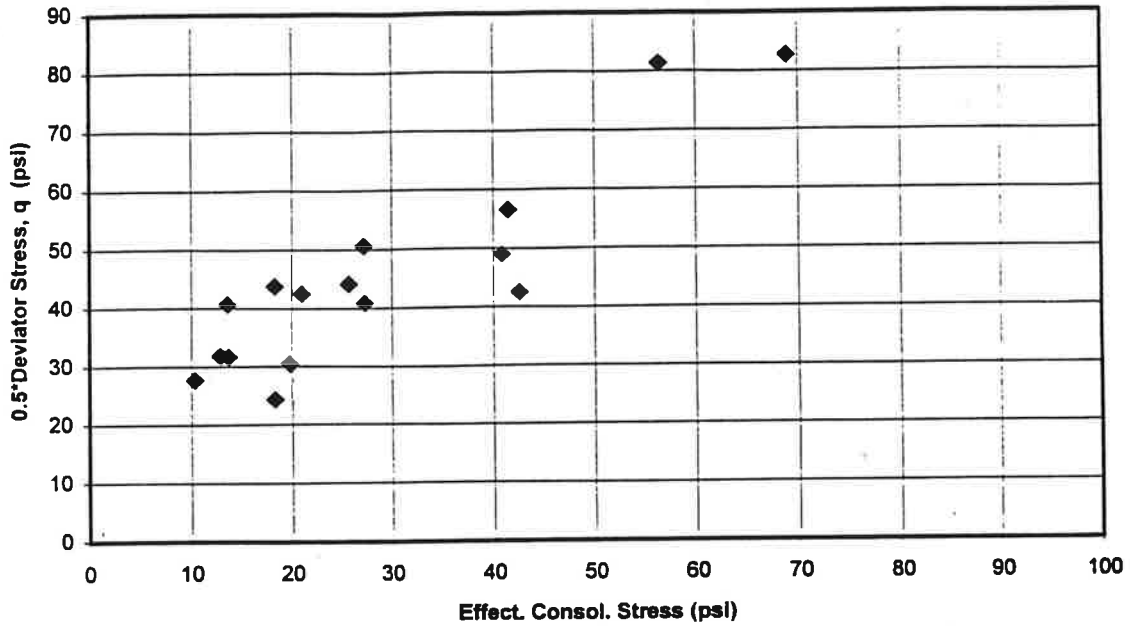
GEO SYNTEC CONSULTANTS

ATLANTA, GEORGIA

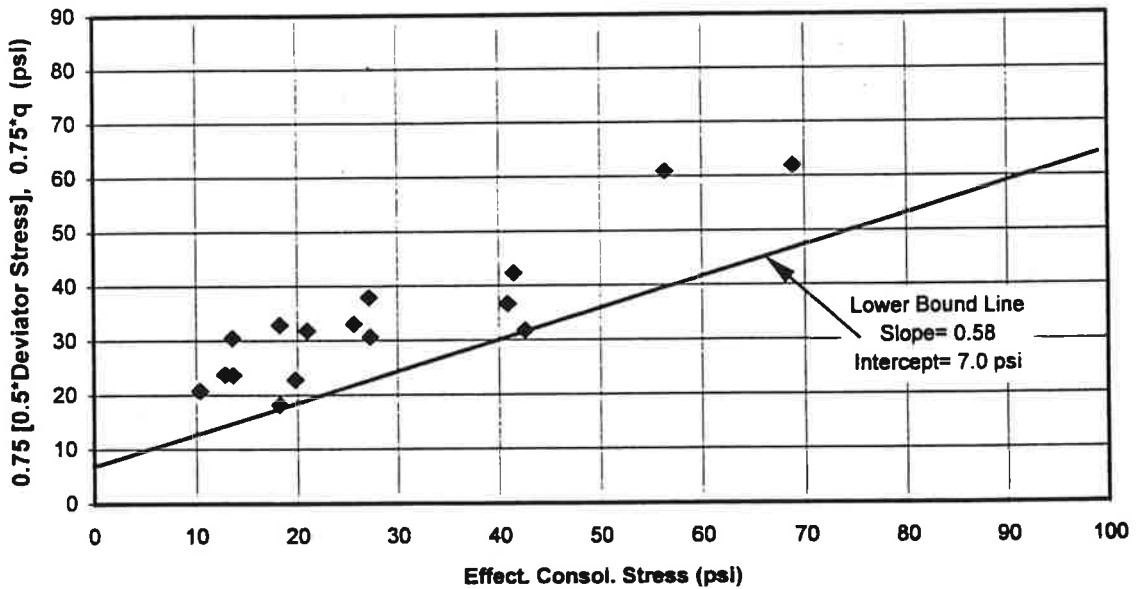
FIGURE NO.	3-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

TRIAxIAL SHEAR TESTING RESULTS TOTAL STRESS SHEAR STRENGTH PARAMETERS

Ultimate Strength Condition



Ultimate Strength Condition with 25% Strength Reduction

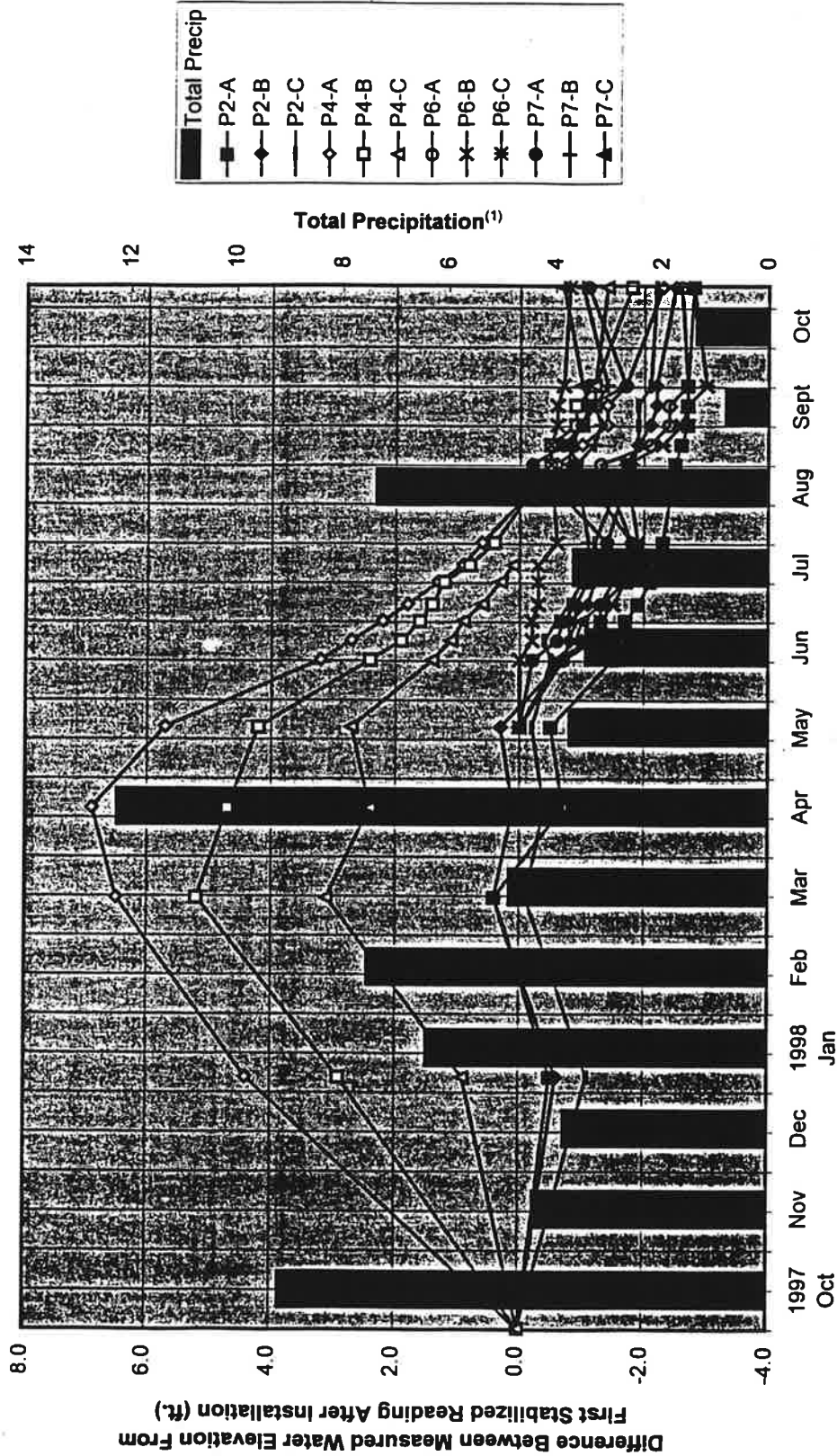


GEO SYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	3-2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

COMPARISON OF PIEZOMETRIC ELEVATION VARIATIONS AND PRECIPITATION DATA



Oct 1997 - Oct 1998

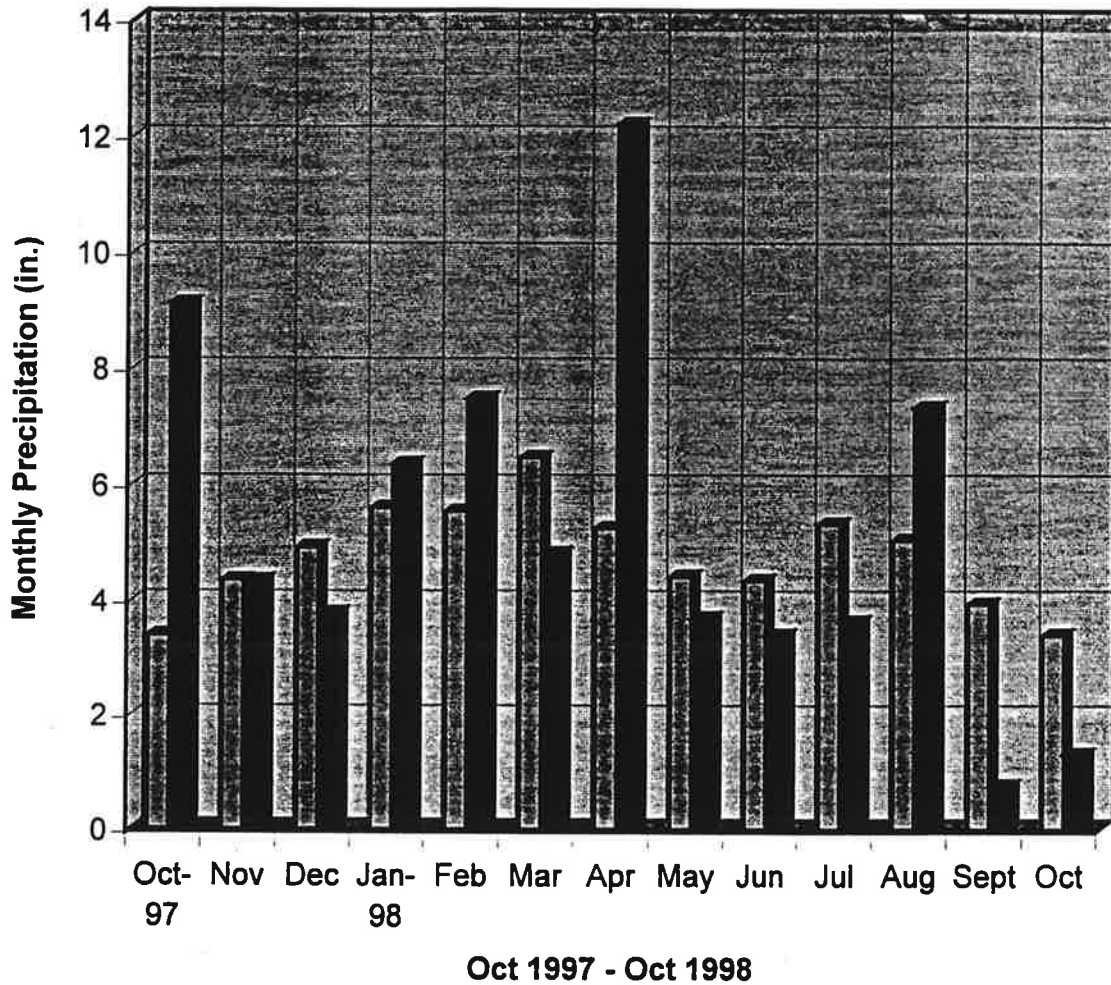
Notes

(1) Monthly precipitation based on precipitation data from Jasper, Georgia



FIGURE NO.	4-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

SUMMARY OF MONTHLY PRECIPITATION DATA JASPER, GEORGIA



■ 30-year average between 6/37 and 10/98 ■ Total Monthly Precipitation for 1998

Notes

Precipitation data obtained from the National Climatic Data Center and the South East Regional Climatic Center

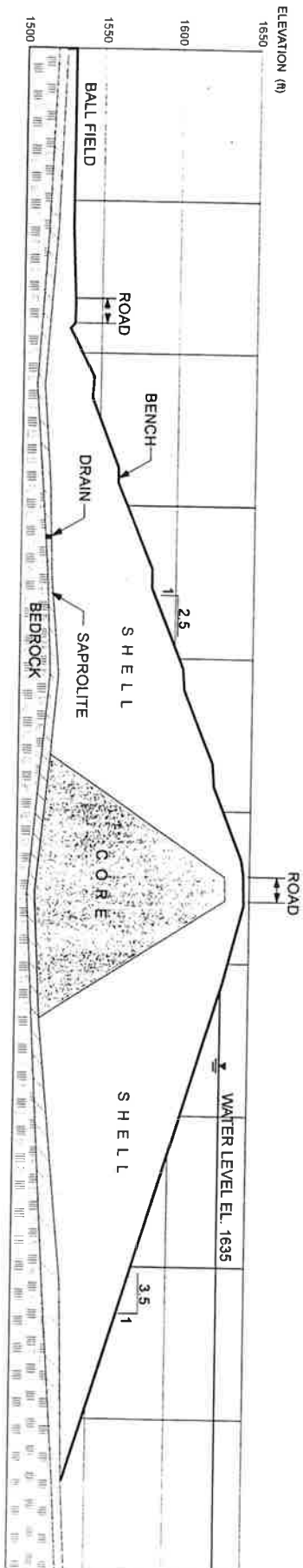



GEO SYNTEC CONSULTANTS

ATLANTA, GEORGIA

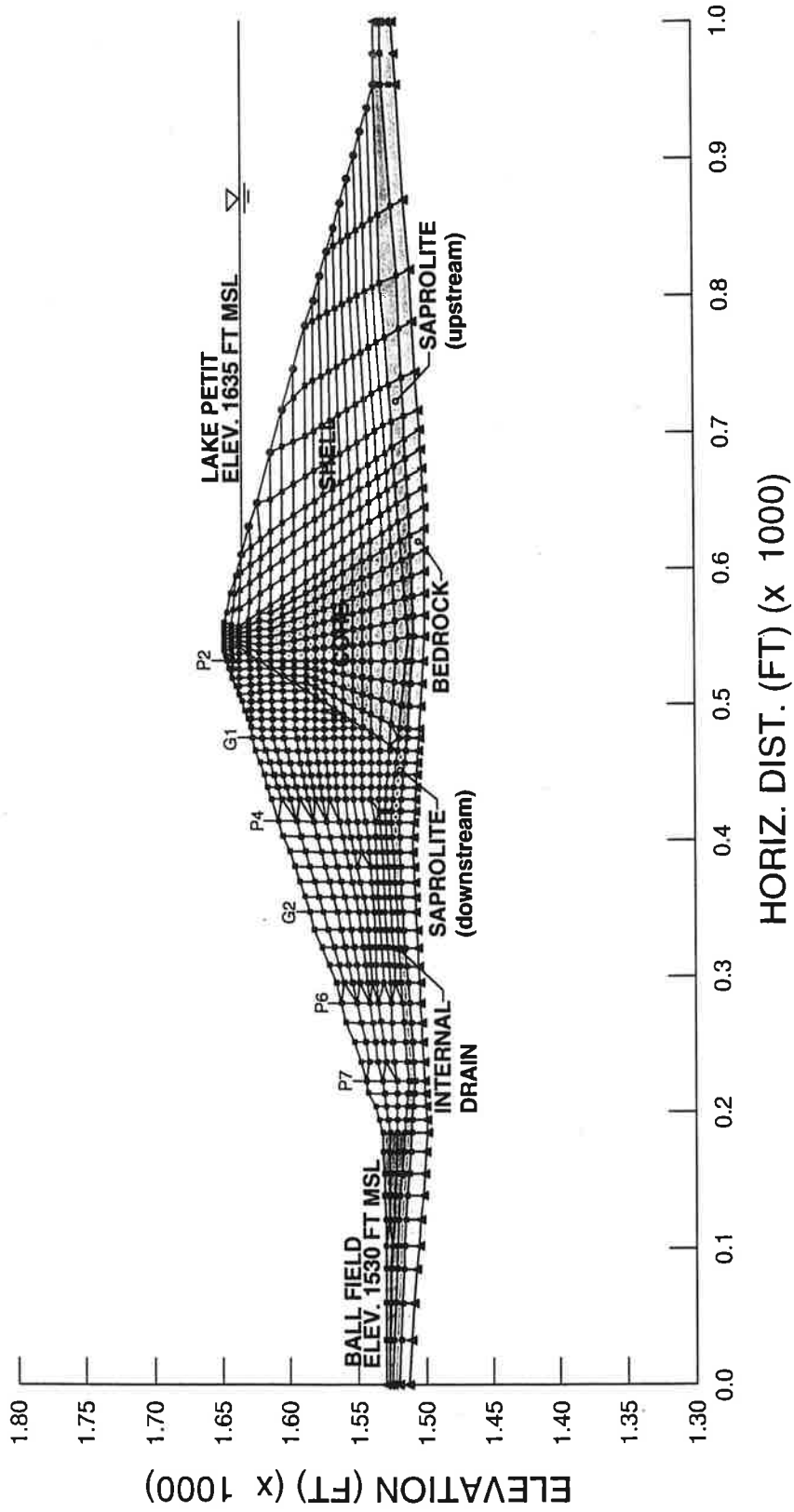
FIGURE NO.	4-2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

**SITE PHYSICAL CONDITIONS MODEL
SECTION A - A**



 GEO SYNTEC CONSULTANTS ATLANTA, GEORGIA			
PROJECT NO.	GL0625-15	FIGURE NO.	5-1
DOCUMENT NO.	GA981181	FILE NO.	SEC-A-CDR

FINITE ELEMENT MESH FOR SEEP/W ANALYSES

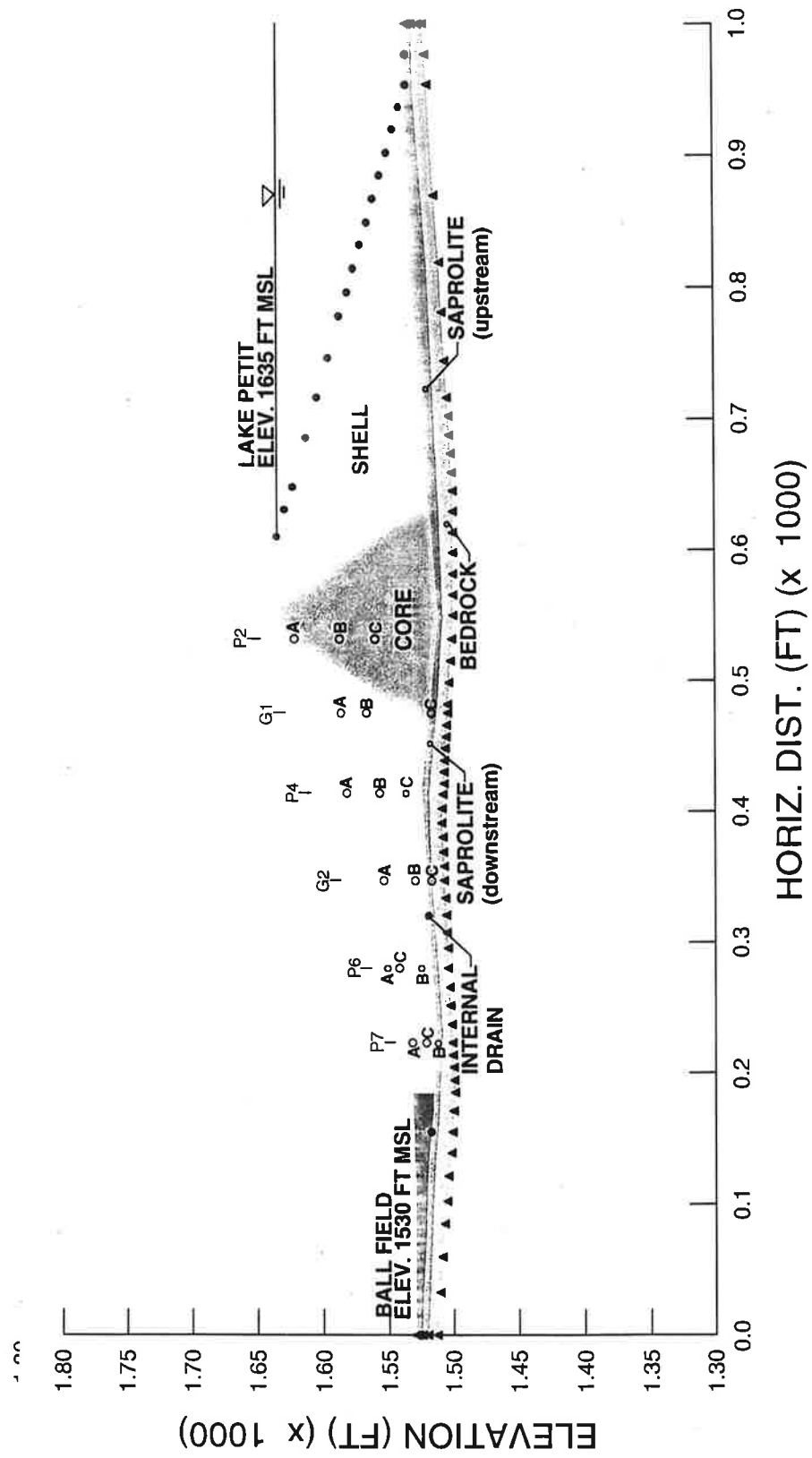


GEO SYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	6-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

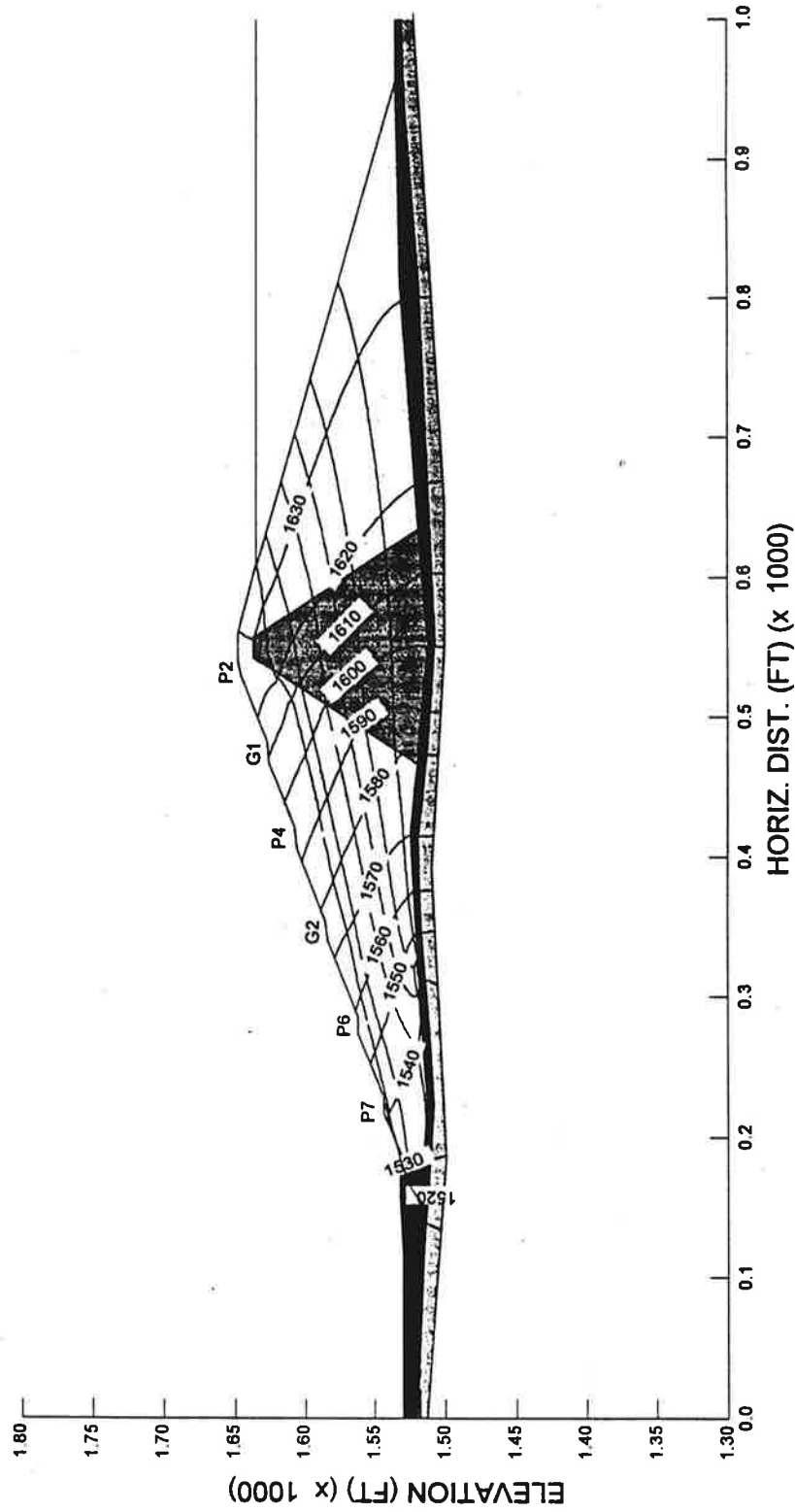
PIEZOMETER LOCATIONS



GEO SYNTEC CONSULTANTS
ATLANTA, GEORGIA

FIGURE NO.	6-2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

**EQUIPOTENTIAL LINES AND FLOW PATHS
23 OCTOBER 1998 SCENARIO**

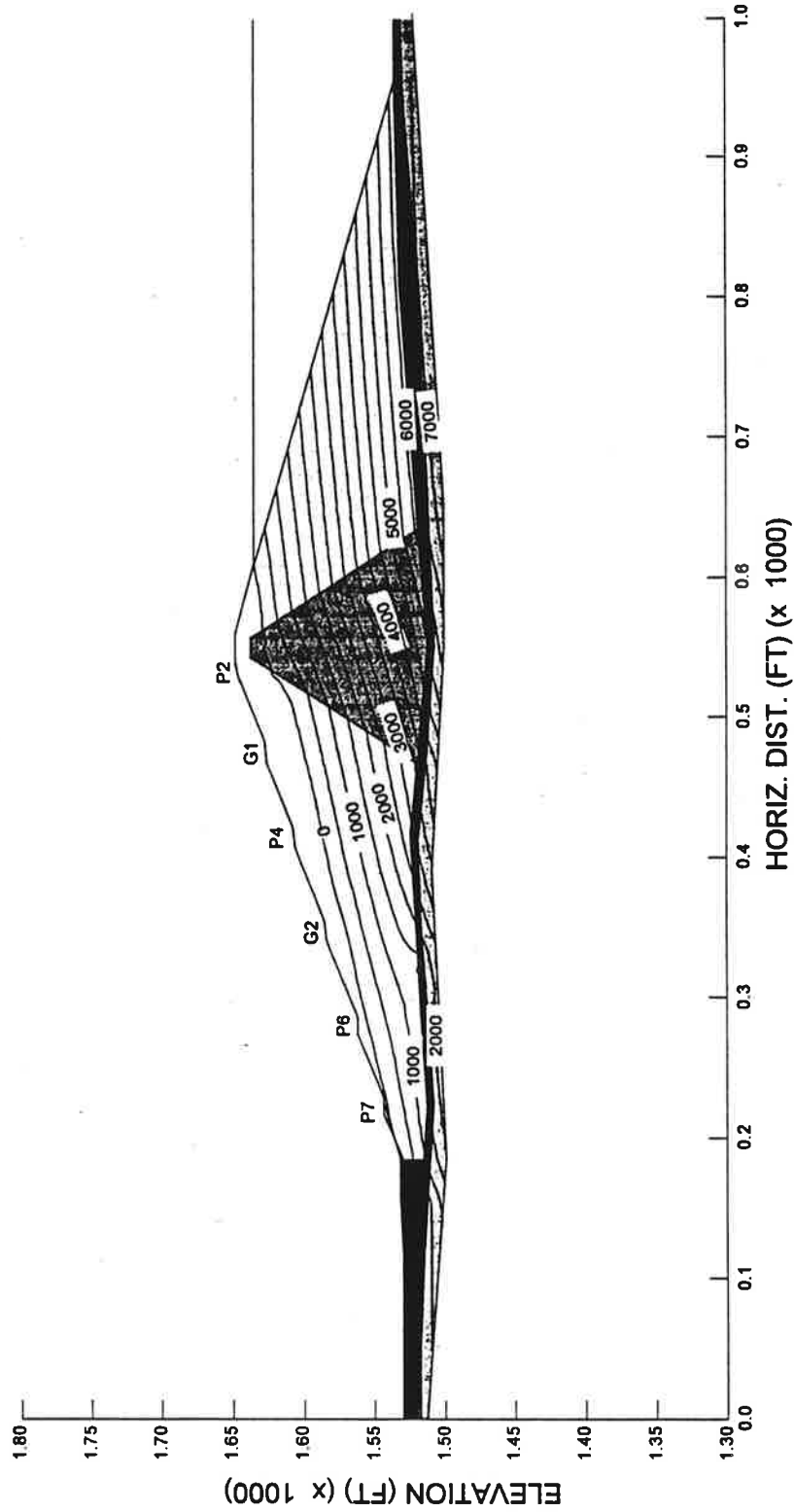


GEO SYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	6-3
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

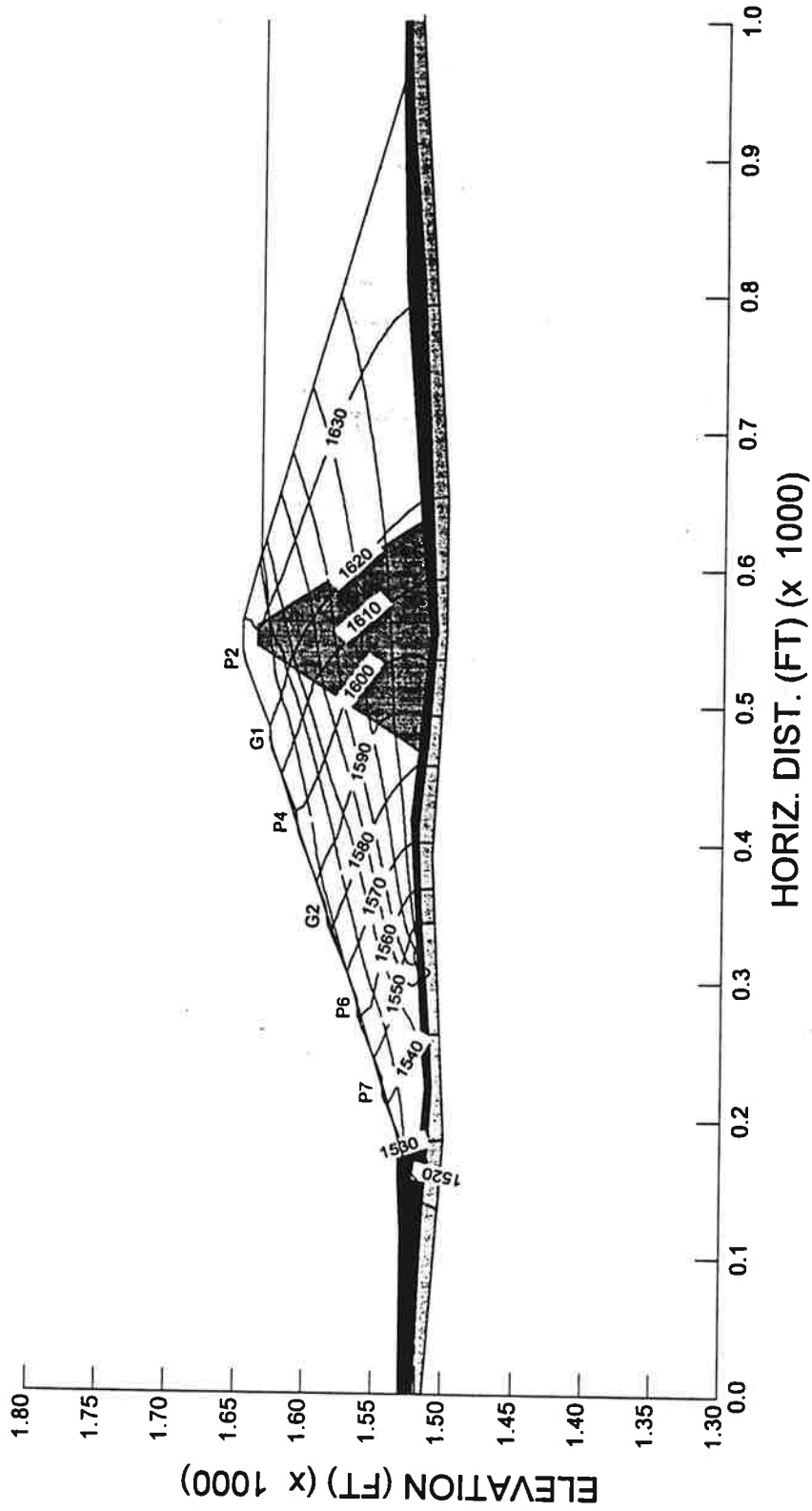
POREWATER PRESSURE DISTRIBUTION 23 OCTOBER 1998 SCENARIO



GEOSYNTEC CONSULTANTS
ATLANTA, GEORGIA

FIGURE NO.	6-4
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

EQUIPOTENTIAL LINES AND FLOW PATHS EML SCENARIO



GEOSYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	6-5
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

POREWATER PRESSURE DISTRIBUTION EML SCENARIO

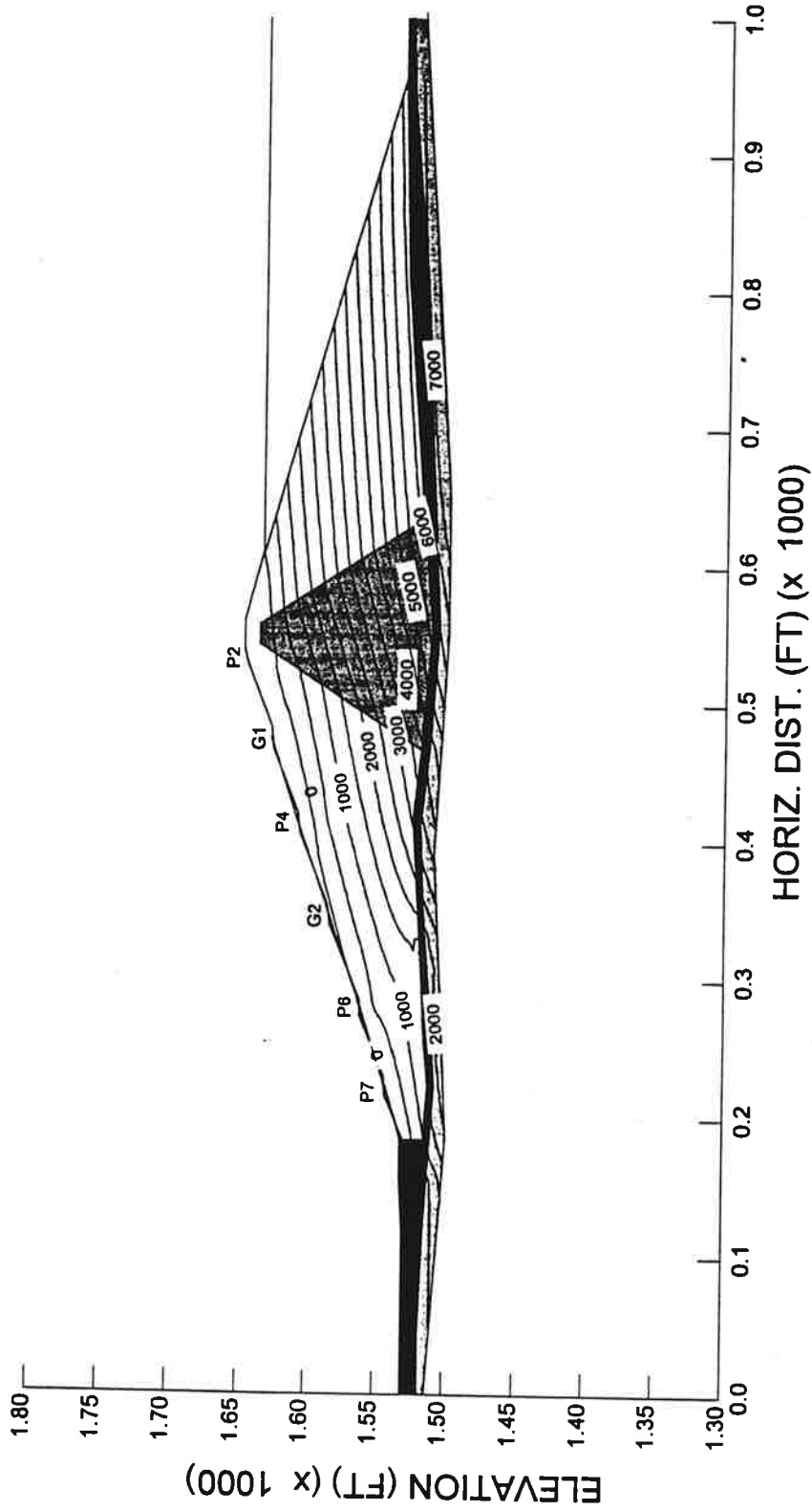
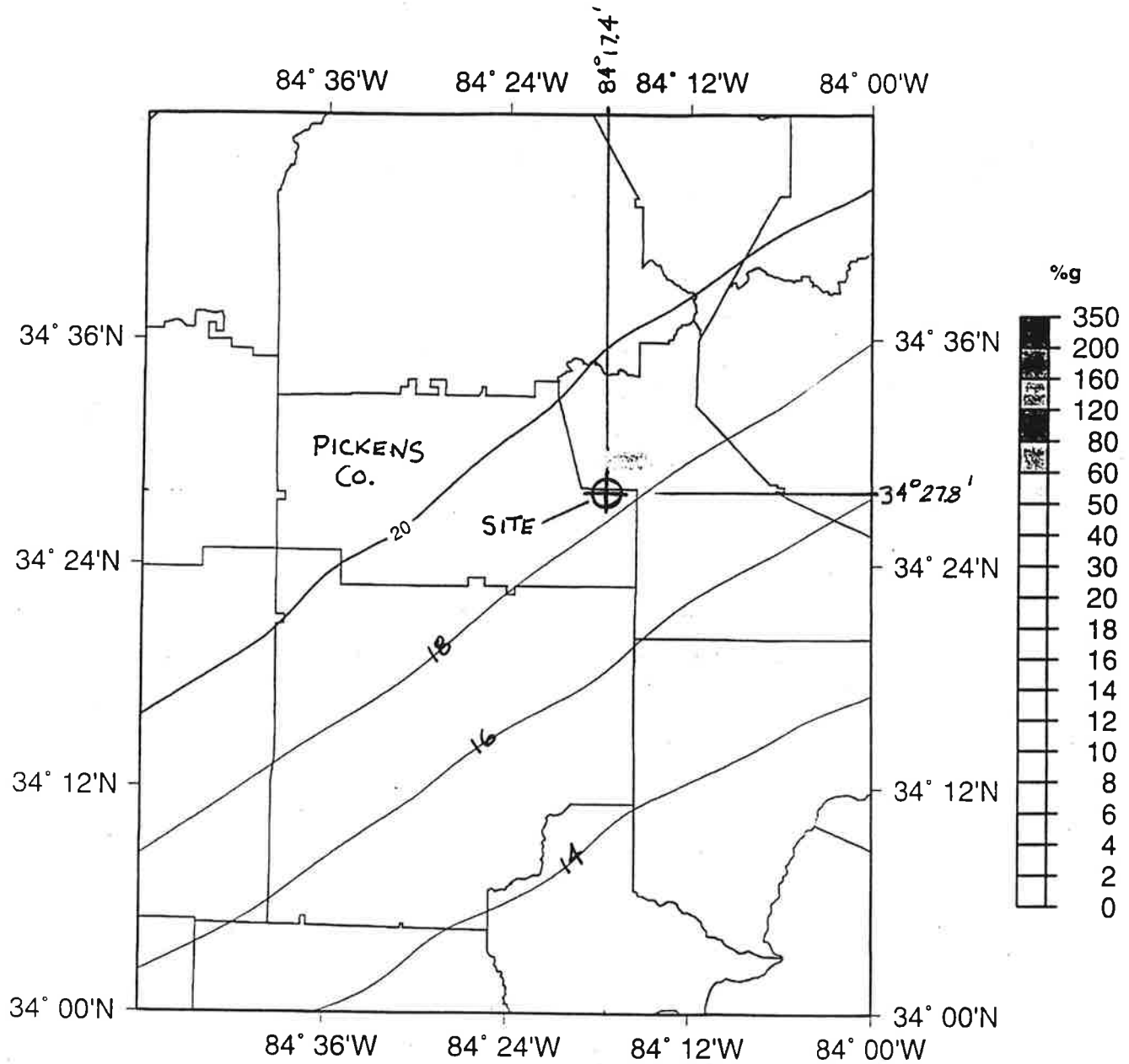


FIGURE NO.	6-6
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

PEAK ACCELERATION MAP



Peak Acceleration (%g) with 2% Probability of Exceedance in 50 Years
 site: NEHRP B-C boundary

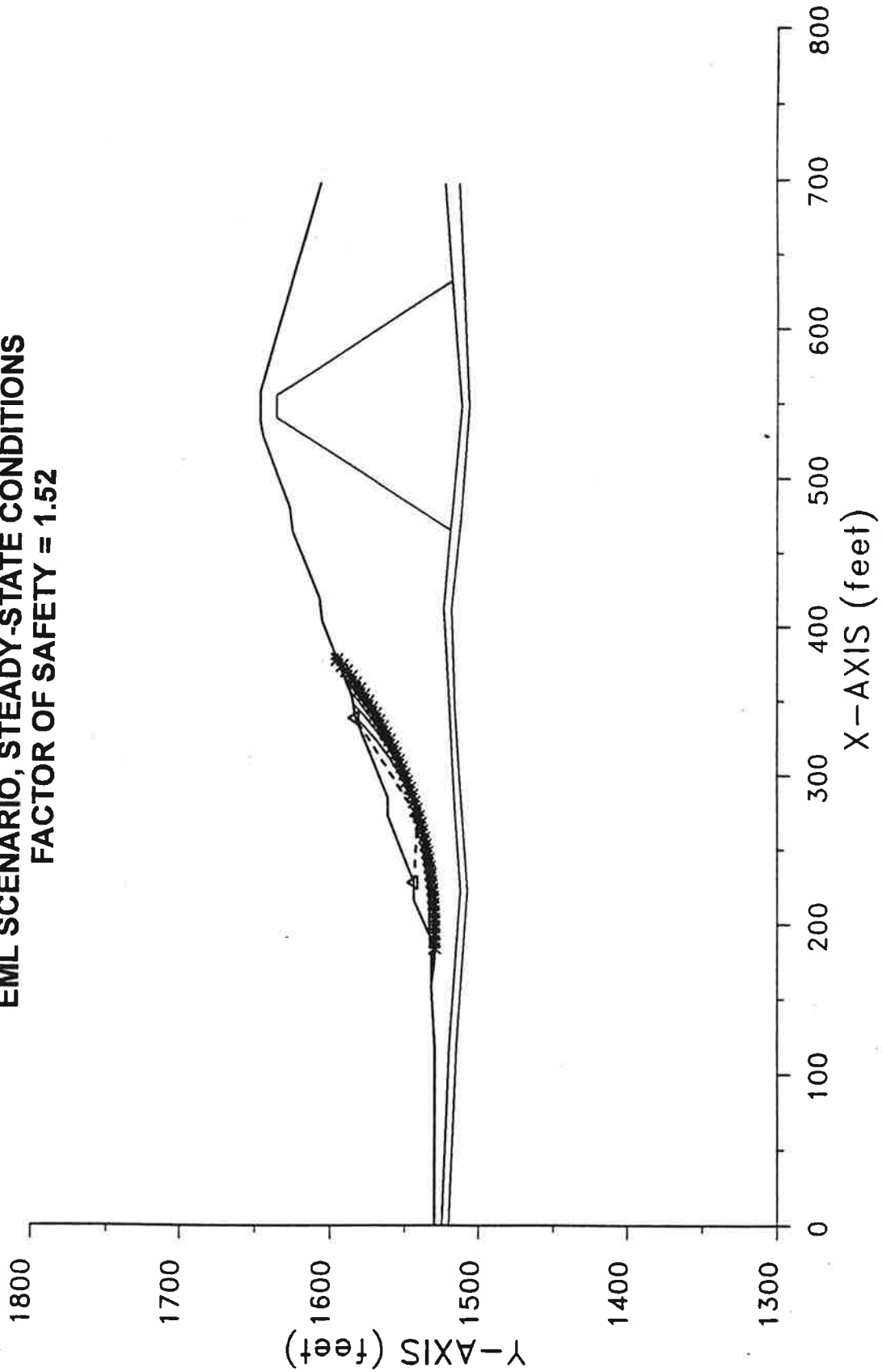
U.S. Geological Survey
 National Seismic Hazard Mapping Project

Albers Conic Equal-Area Projection
 Standard Parallels: 29.5 and 45.5 degrees



FIGURE NO.	7-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIGS.cdr/df

**CRITICAL POTENTIAL SLIP SURFACES
DOWNSTREAM EMBANKMENT SLOPE STABILITY
EML SCENARIO, STEADY-STATE CONDITIONS
FACTOR OF SAFETY = 1.52**

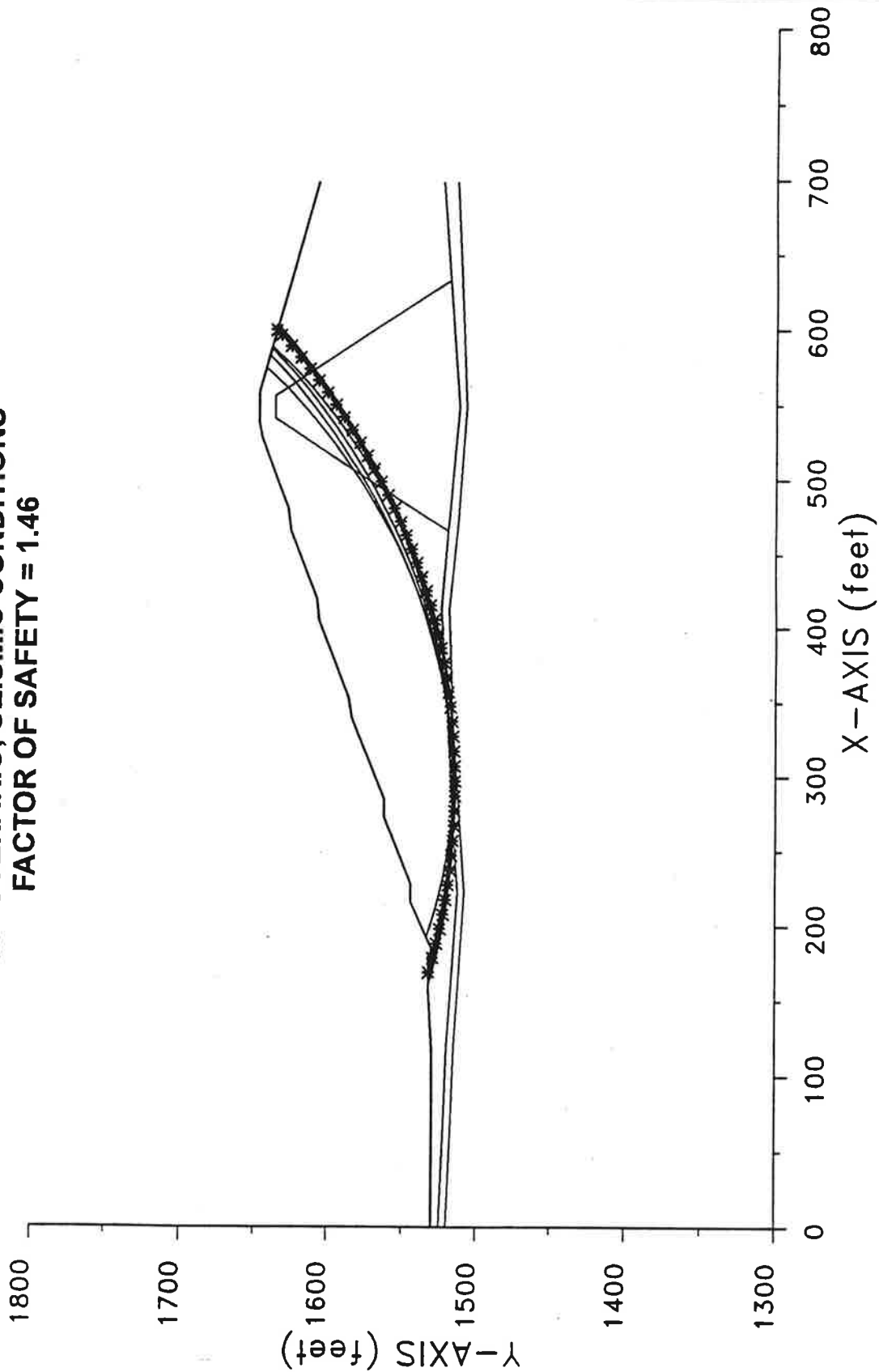


GEOSYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	7-2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	LPD.cdr/df

**CRITICAL POTENTIAL SLIP SURFACES
DOWNSTREAM EMBANKMENT SLOPE STABILITY
EML SCENARIO, SEISMIC CONDITIONS
FACTOR OF SAFETY = 1.46**

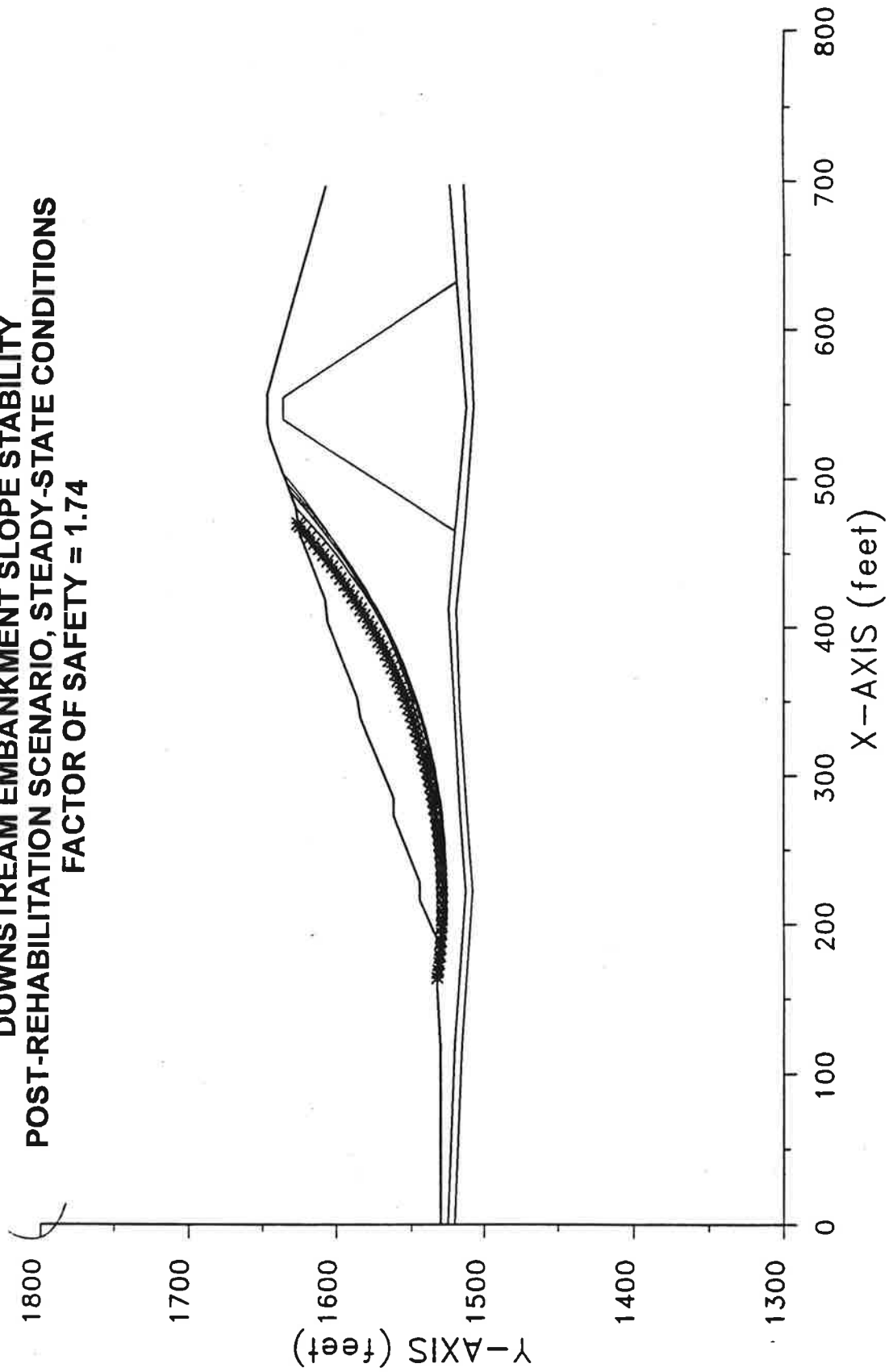


GEOSYNTEC CONSULTANTS

ATLANTA, GEORGIA

FIGURE NO.	7-3
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	LPD.cdr/df

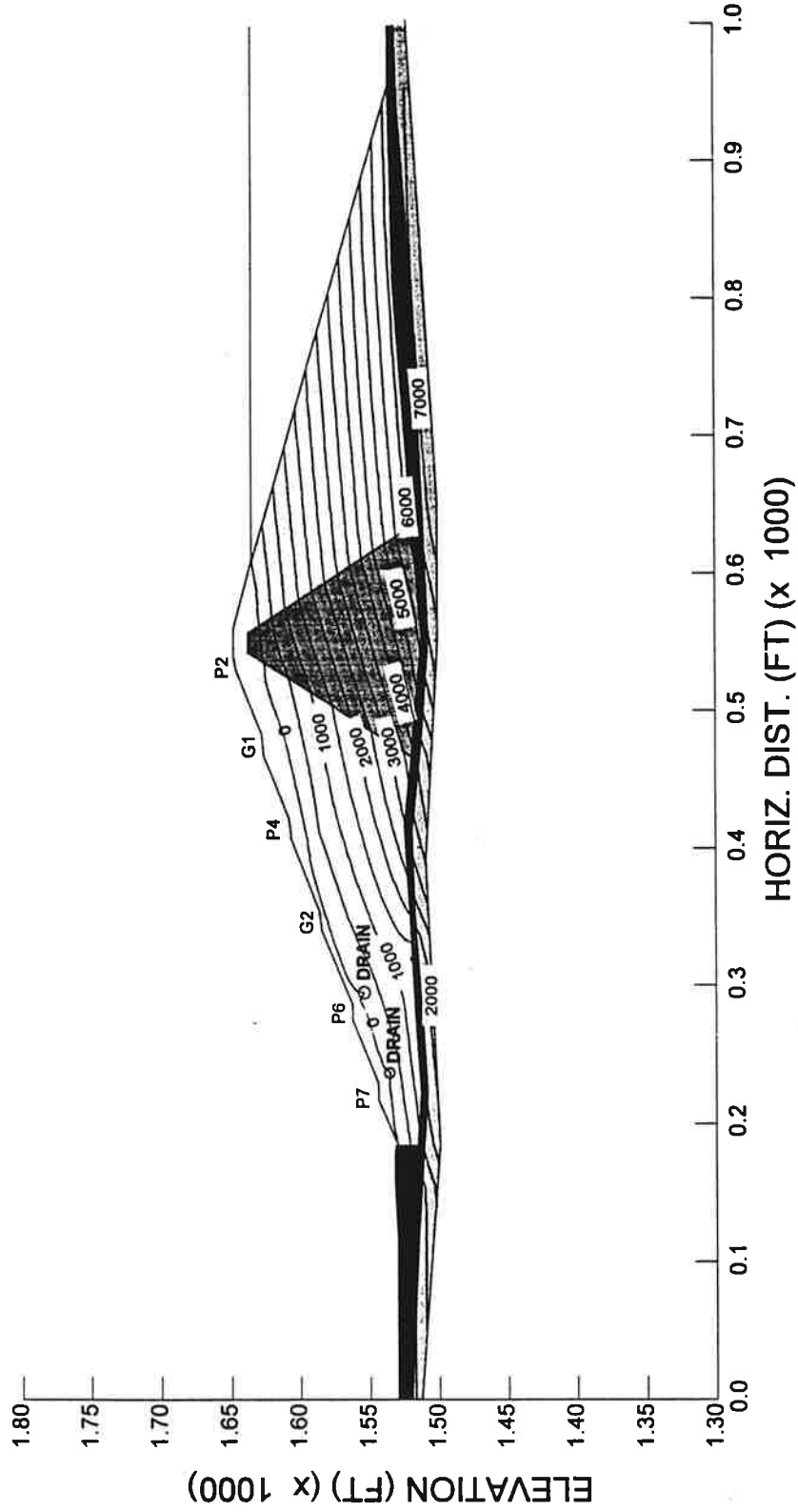
**CRITICAL POTENTIAL SLIP SURFACES
 DOWNSTREAM EMBANKMENT SLOPE STABILITY
 POST-REHABILITATION SCENARIO, STEADY-STATE CONDITIONS
 FACTOR OF SAFETY = 1.74**



GEO SYNTEC CONSULTANTS
 ATLANTA, GEORGIA

FIGURE NO.	7-4
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	LPD.cdr/df

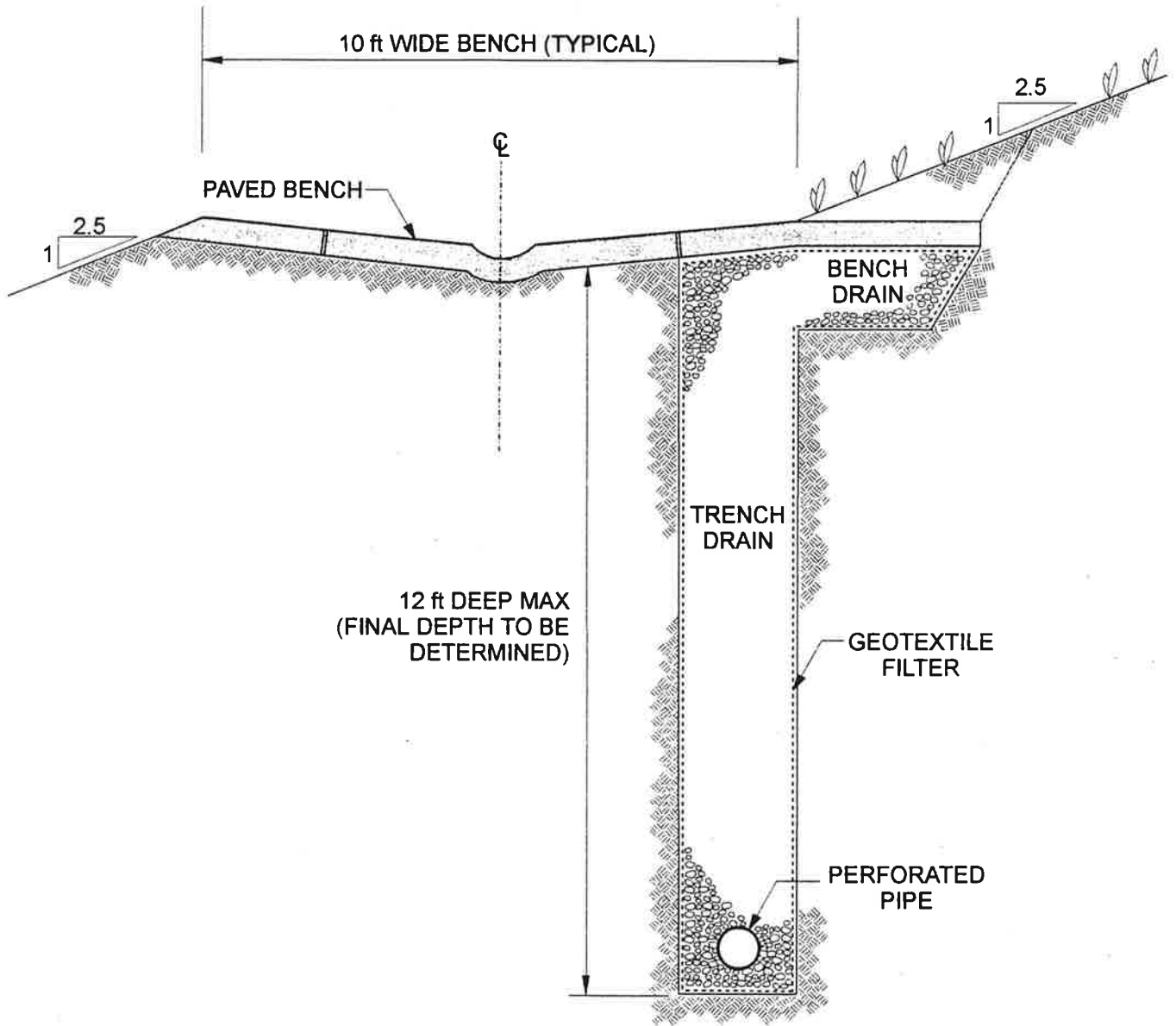
INFLUENCE OF TRENCH DRAIN ON POREWATER PRESSURE DISTRIBUTION



GEO SYNTEC CONSULTANTS
ATLANTA, GEORGIA

FIGURE NO.	8-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FINITE.cdr/df

TYPICAL DETAIL OF PAVED BENCH AND DRAINAGE SYSTEMS

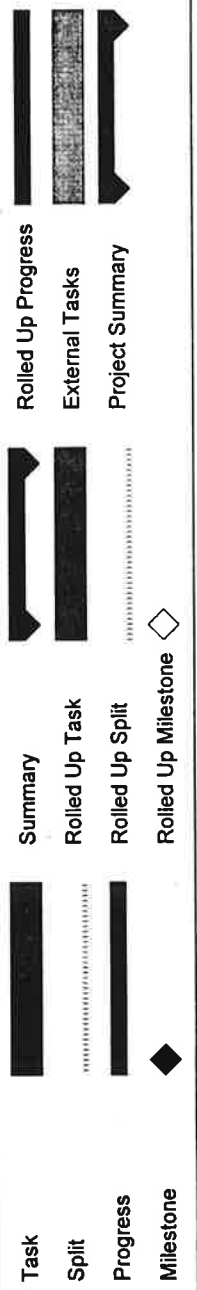
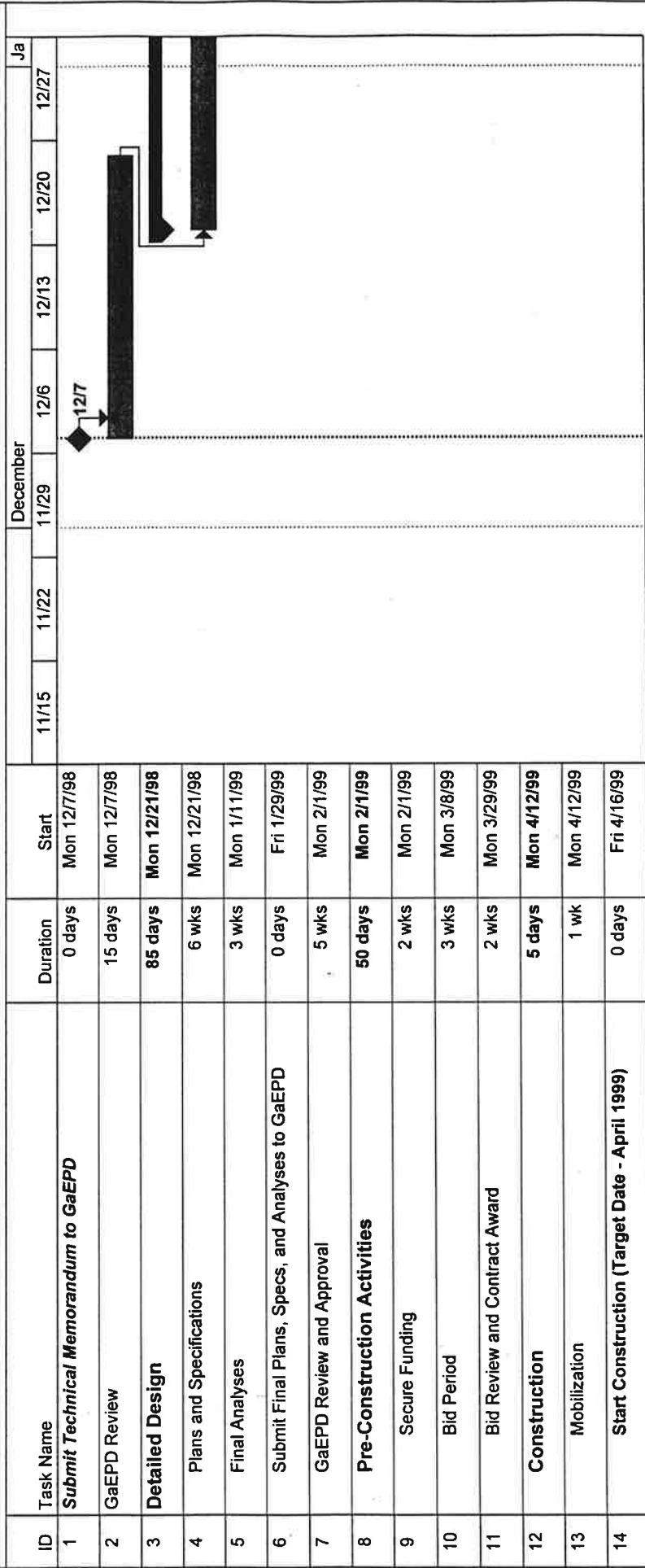


GEOSYNTEC CONSULTANTS

ATLANTA, GEORGIA

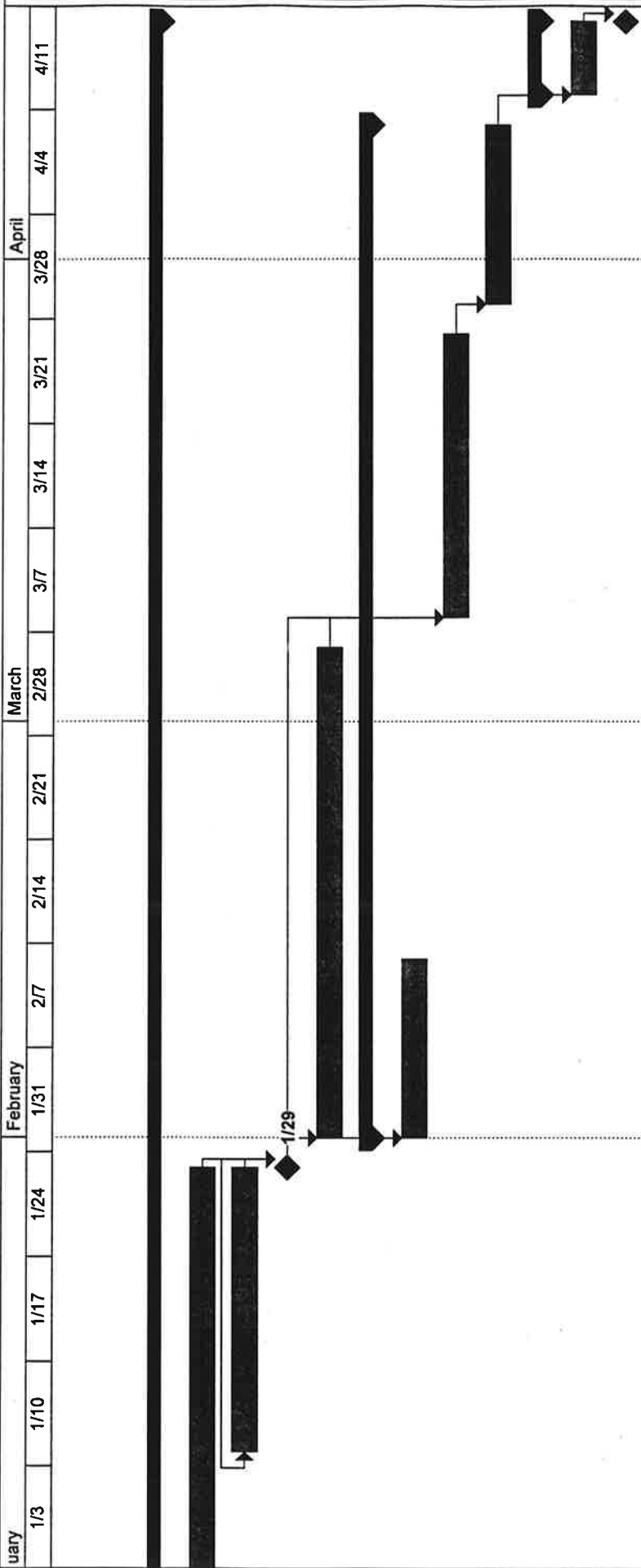
FIGURE NO.	8 - 2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	FIG-8-2.cdr

Figure 8-3
Proposed Schedule
Implementation Of Rehabilitation Measures, Lake Petit Dam



Project: Tech Memorandum Schedule
Date: Mon 12/7/98

Figure 8-3
Proposed Schedule
Implementation Of Rehabilitation Measures, Lake Petit Dam



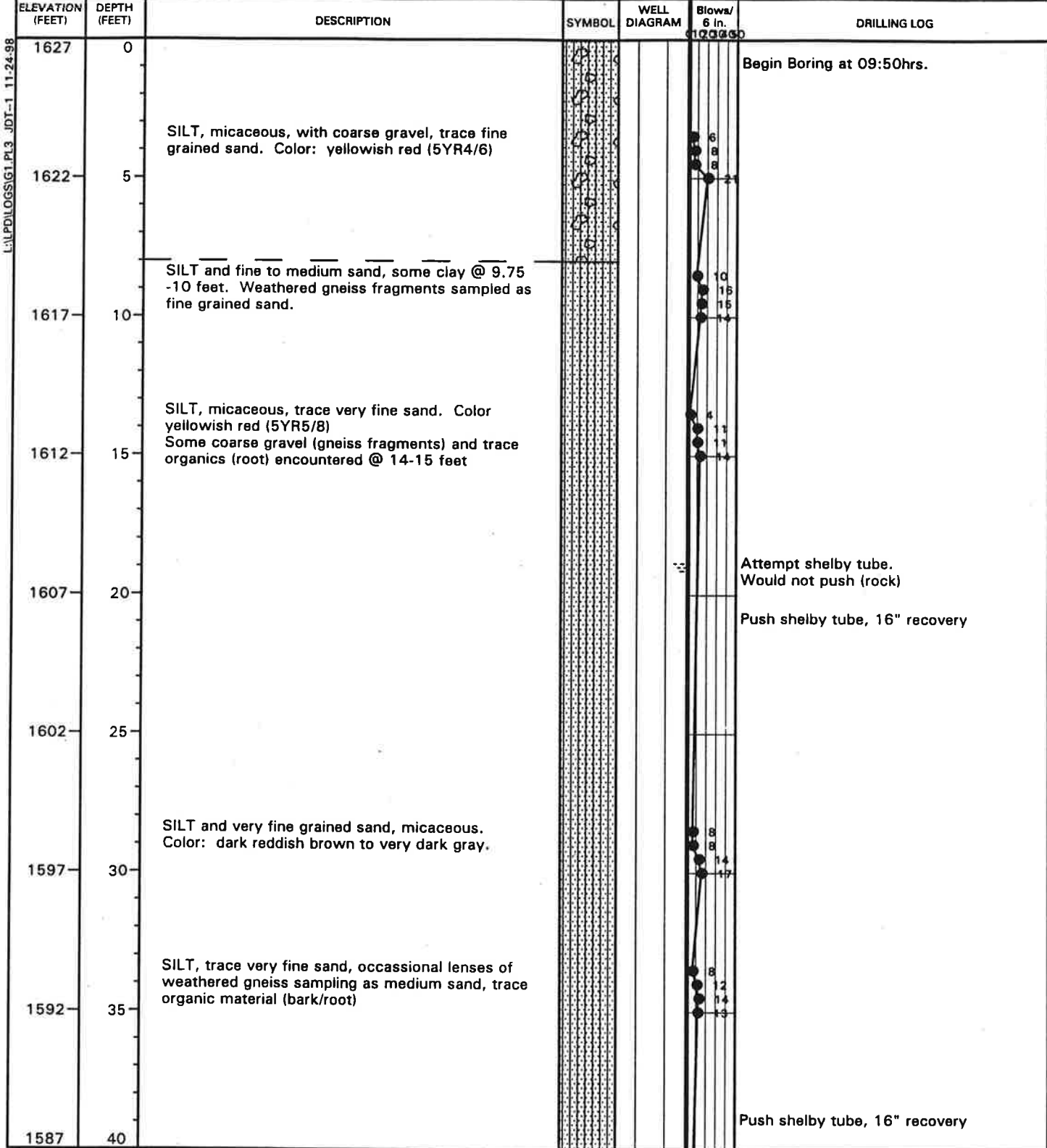
Task		Summary		Rolled Up Progress	
Split		Rolled Up Task		External Tasks	
Progress		Rolled Up Split		Project Summary	
Milestone		Rolled Up Milestone			

Project: Tech Memorandum Schedule
Date: Mon 12/7/98

APPENDIX A

BORING LOGS AND
PIEZOMETER CONSTRUCTION LOGS

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-1B
LOCATION: G-1	N: E:	GROUND ELEV.: 1627.0
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 6 Oct 98	COMPLETED- 12 Oct 98	CHECKED BY: G. Schmertmann



REMARKS:
 3-WELL PIEZOMETER CLUSTER CONSTRUCTED AS FOLLOWS:
 SHALLOW - 1-INCH PVC CASING SCREENED @ 20-40
 MIDDLE - 1-INCH PVC CASING SCREENED @ 55-60
 DEEP - 4-IN. PVC CASING SCREENED @ 105.5-110.5

SEE ATTACHED FIGURE FOR CONSTRUCTION DETAILS

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-1B
LOCATION: G-1	N:	E:
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 6 Oct 98	COMPLETED- 12 Oct 98	CHECKED BY: G. Schmertmann

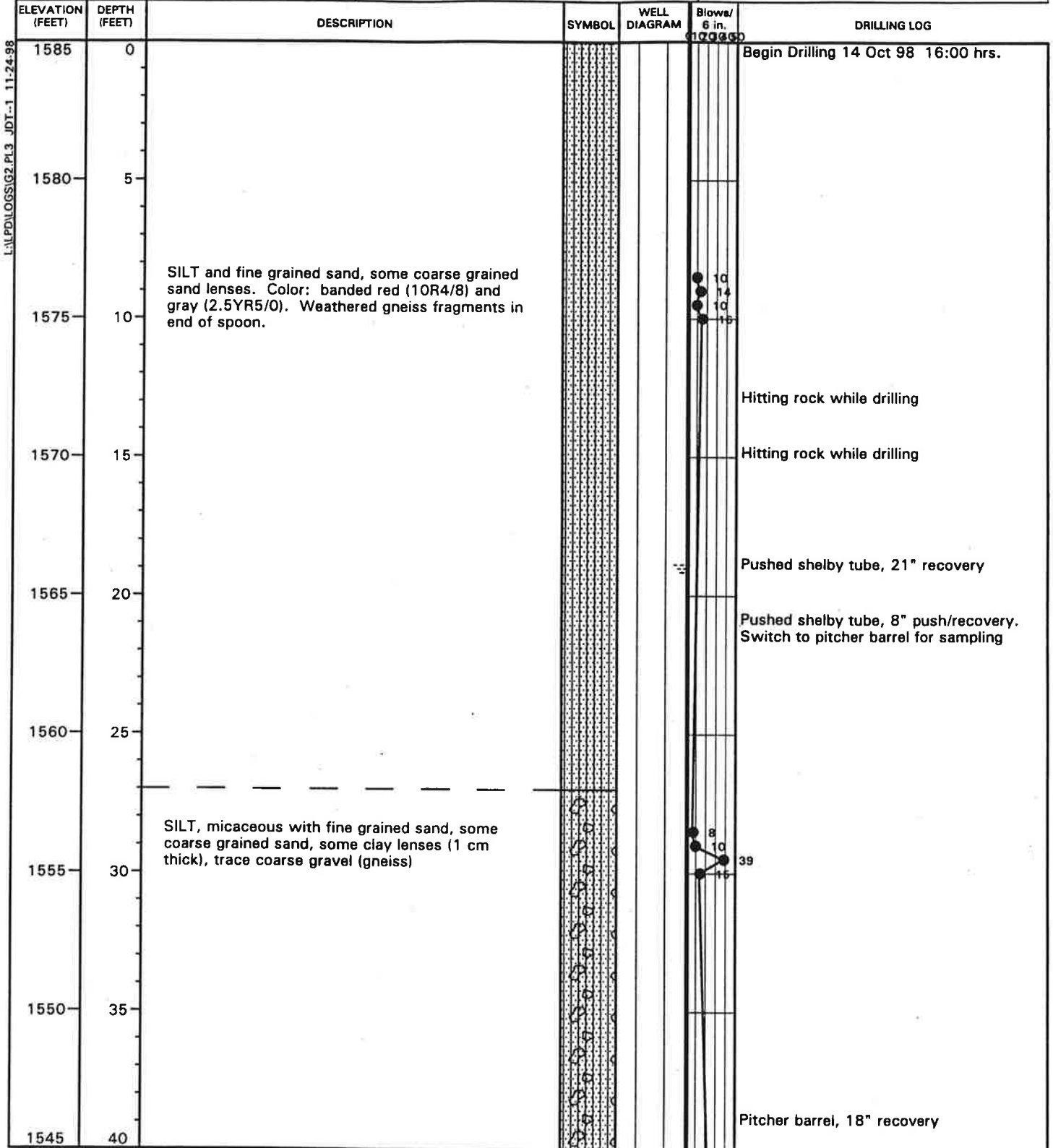
ELEVATION (FEET)	DEPTH (FEET)	DESCRIPTION	SYMBOL	WELL DIAGRAM	Blows/6 in.	DRILLING LOG
1587	40					Push shelby tube, 16" recovery.
1582	45					
1577	50	SILT, trace very fine sand, micaceous (muscovite). Color: red (2.5YR4/8) and very dark gray (10YR3/1)			5 8 14 20	Hard drilling @ 51-52 feet.
		SILT, some very fine sand, some medium to coarse gravel (weathered gneiss and schist fragments).			14	Split spoon bouncing on wood 50/5
1572	55					Hard drilling (rock) @ 57.5-58 feet
						Push shelby tube, 16" recovery
1567	60					
1562	65	SILT, some very fine sand, some medium to coarse gravel (weathered gneiss and schist). Increasing size and number with depth in the spoon.			12 21 20 25	
1557	70				14 14 18 18	
1552	75	SAND, very fine to fine grained, and silt, some fine to medium gravel (weathered gneiss and schist fragments). Silty clay in end of spoon.			14 19 19 18	
1547	80					

L:\PD\LOGS\G1\Pl.3_JDT--1_11-24-98

REMARKS:

TEST BORING RECORD

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-2
LOCATION: G-2	N:	E:
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 14 Oct 98	COMPLETED- 15 Oct 98	CHECKED BY: G. Schmertmann

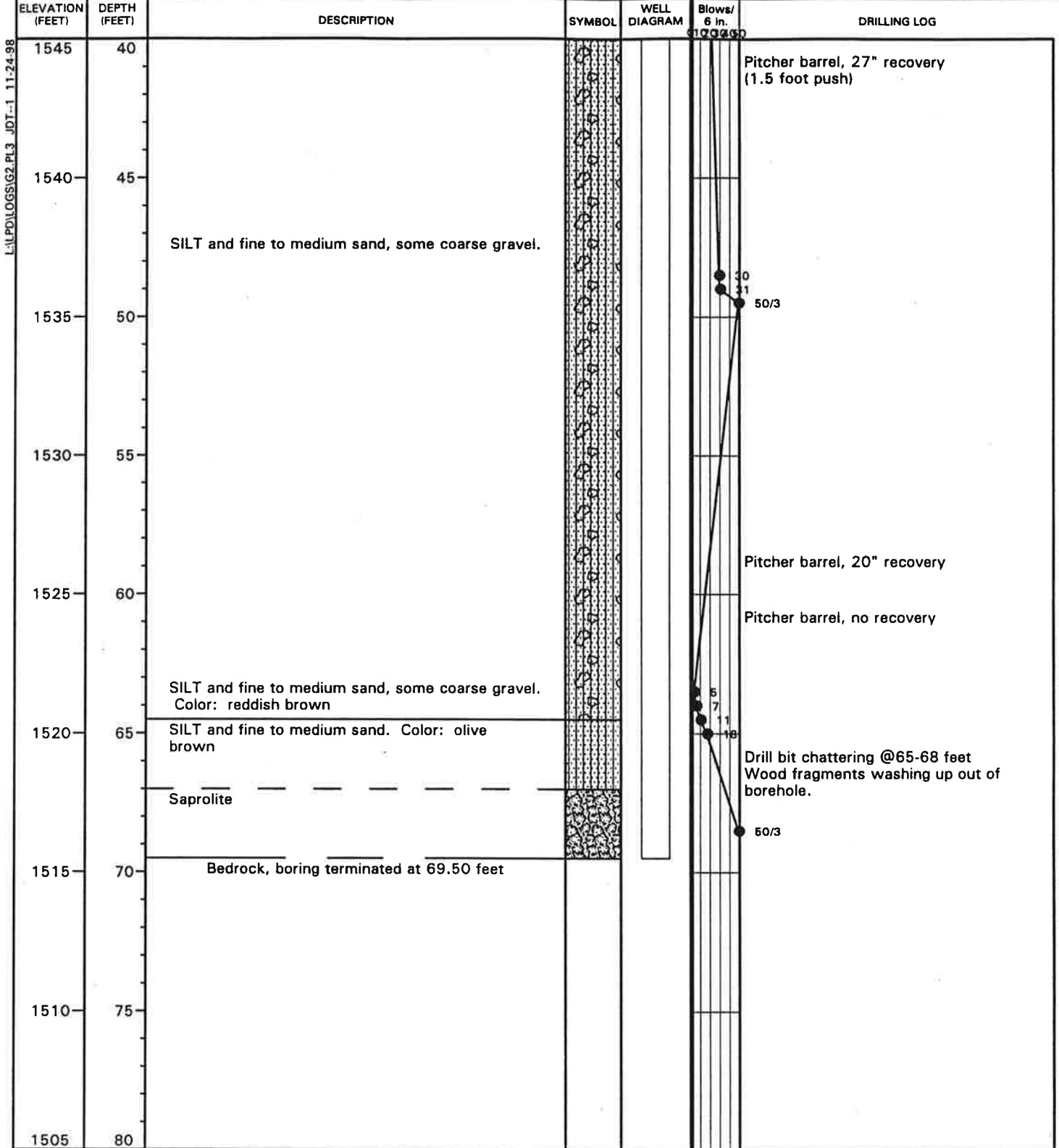


REMARKS:
 3-WELL PIEZOMETER CLUSTER CONSTRUCTED AS FOLLOWS:
 SHALLOW - 1-IN. PVC CASING SCREENED @ 10-30
 MIDDLE - 1-IN. PVC CASING SCREENED @ 50-55
 DEEP - 1-IN. PVC CASING SCREENED @ 65.5-68.5

SEE ATTACHED FIGURE FOR CONSTRUCTION DETAILS

TEST BORING RECORD

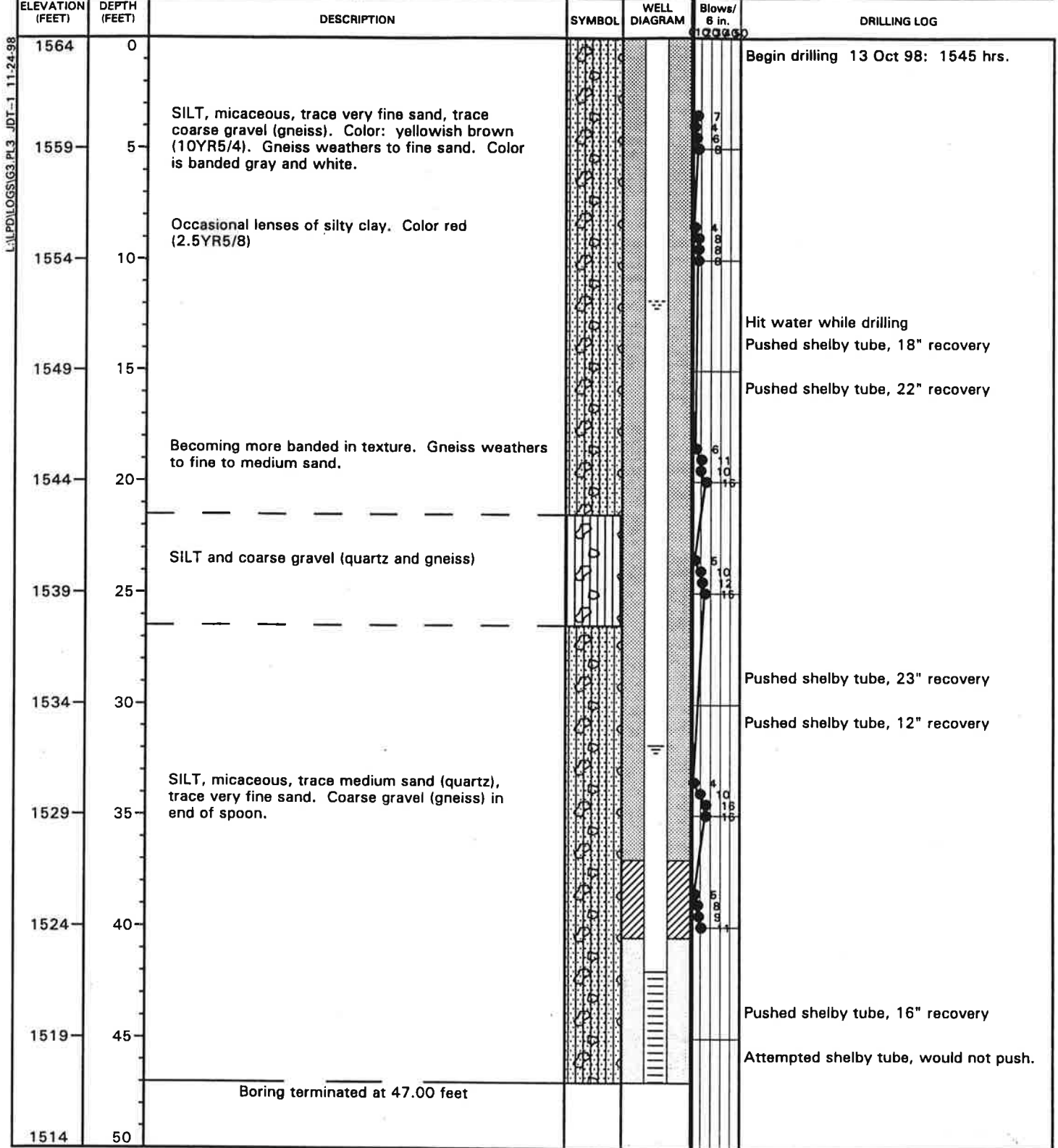
PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-2
LOCATION: G-2	N:	E:
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 14 Oct 98	COMPLETED- 15 Oct 98	CHECKED BY: G. Schmetmann



REMARKS:

TEST BORING RECORD

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-3
LOCATION: G-3	N: _____ E: _____	GROUND ELEV.: 1564.03
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: 4-1/4 ID HSA		LOGGED BY: J. Titus
DATE: STARTED- 13 Oct 98	COMPLETED- 13 Oct 98	CHECKED BY: G. Schmertmann



REMARKS:
SHALLOW PIEZOMETER SCREENED IN FILL MATERIAL

CONSTRUCTION: 1-INCH ID PVC PIPE WITH 5-FEET OF 0.010-INCH SLOTTED SCREEN.

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-4
LOCATION: G-4	N: _____ E: _____	GROUND ELEV.: 1605.8
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: HSA/4" Mud Rotary		LOGGED BY: GS / JDT
DATE: STARTED- 2 Oct 98	COMPLETED- 5 Oct 98	CHECKED BY: G. Schmertmann

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ELEVATION (FEET)	DEPTH (FEET)	DESCRIPTION	SYMBOL	WELL DIAGRAM	Blows/6 in.	DRILLING LOG
1606	0					20CT98 Beging drilling using 4-1/4 ID HSA
1601	5	SILT, some sand. Color: brown			3 4 5 7	
1596	10	SILT, some sand, some medium gravel, micaceous, dry			6 5 5 15	Push shelby tube, 15" recovery
1591	15					Push shelby tube, 7" recovery
1586	20	SILT, some sand, some gravel. Medium gravel (weathered gneiss and schist) concentrated in upper 6" spoon, more silt in lower 9". dry. Color: dark brown.			17 18 8 5	
1581	25				4 13 10 8	Attempted shelby tube, would not push
1576	30					Attempted shelby tube, would not push Resume drilling on 5OCT98 at 10:45 hrs using 4-3/4 OD mud rotary. Boring has been offset by 5 feet from original location.
1571	35					30-32 ft. - Pitcher barrel sample
1566	40	SILT, some sand. Trace gravel in upper 3" of spoon. micaceous, dark brown.			7 7 8	

REMARKS:

TEST BORING RECORD

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-4
LOCATION: G-4	N: E:	GROUND ELEV.: 1605.8
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: HSA/4" Mud Rotary		LOGGED BY: GS / JDT
DATE: STARTED- 2 Oct 98	COMPLETED- 5 Oct 98	CHECKED BY: G. Schmertmann

L:\L\PD\LOGS\G4 PL3 _JDT--1 11-24-98

ELEVATION (FEET)	DEPTH (FEET)	DESCRIPTION	SYMBOL	WELL DIAGRAM	Blows/ 6 in.	DRILLING LOG
1566	40				8	Push shelby tube, 5" recovery.
1561	45	SILT, some sand, some fine to meduim gravel, micaceous				Push shelby tube, no recovery Pitcher barrel sample, 20" recovery
1556	50	SILT, some sand, trace gravel (FILL)				Pitcher barrel sample, 8" recovery
		Saprolite			10 15 25	
1551	55	Boring terminated at 55.00 feet			50/4	
1546	60					
1541	65					
1536	70					
1531	75					
1526	80					

REMARKS:

TEST BORING RECORD

PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-5
LOCATION: G-5	N:	E:
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 12 Oct 98	COMPLETED- 14 Oct 98	CHECKED BY: G. Schmertmann

ELEVATION (FEET)	DEPTH (FEET)	DESCRIPTION	SYMBOL	WELL DIAGRAM	Blows/ 8 in.	DRILLING LOG
1647	0					Begin drilling on 12OCT98: 13:50 hrs.
		SILT some fine to medium sand, some fine to medium gravel. Dry, Color: brown (7.5YR4/4)			4 6 7 8	
1642	5					
		SILT, some very fine to fine sand, micaceous. Color: banded strong brown (7.5YR5/6) and dark gray (7.5YR4/0).			8 9 12 15	
1637	10					Push Shelby tube, 17" recovery
1632	15					Pushed Shelby tube 1 foot, 24" recovery (wash out)
		SILT, trace very fine sand. Color: dark gray to very dark gray (10YR4/1 - 3/1)			4 4 7 8	
1627	20					
		SILT, trace clay, micaceous, Color: red (10R4/8) Extremely weathered schist (to silt) in end of spoon.			5 5 4 5	
1622	25					Push Shelby tube, 19" recovery
		SILT, some very fine sand, micaceous. Trace clay in lower 6" of spoon.				
1617	30					Push Shelby tube, no recovery
		SILT, some fine to medium quartz sand, trace clay, micaceous. Color: red (2.5YR4/8).			2 4 6 8	
1612	35					
		SILT and sand (weathered gneiss)			5 6 6	
1607	40					
		SILT, and clay. Wood fragments at 29 feet.				

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REMARKS:
Blank casing installed (no screen) for downhole geophysics applications.

TEST BORING RECORD

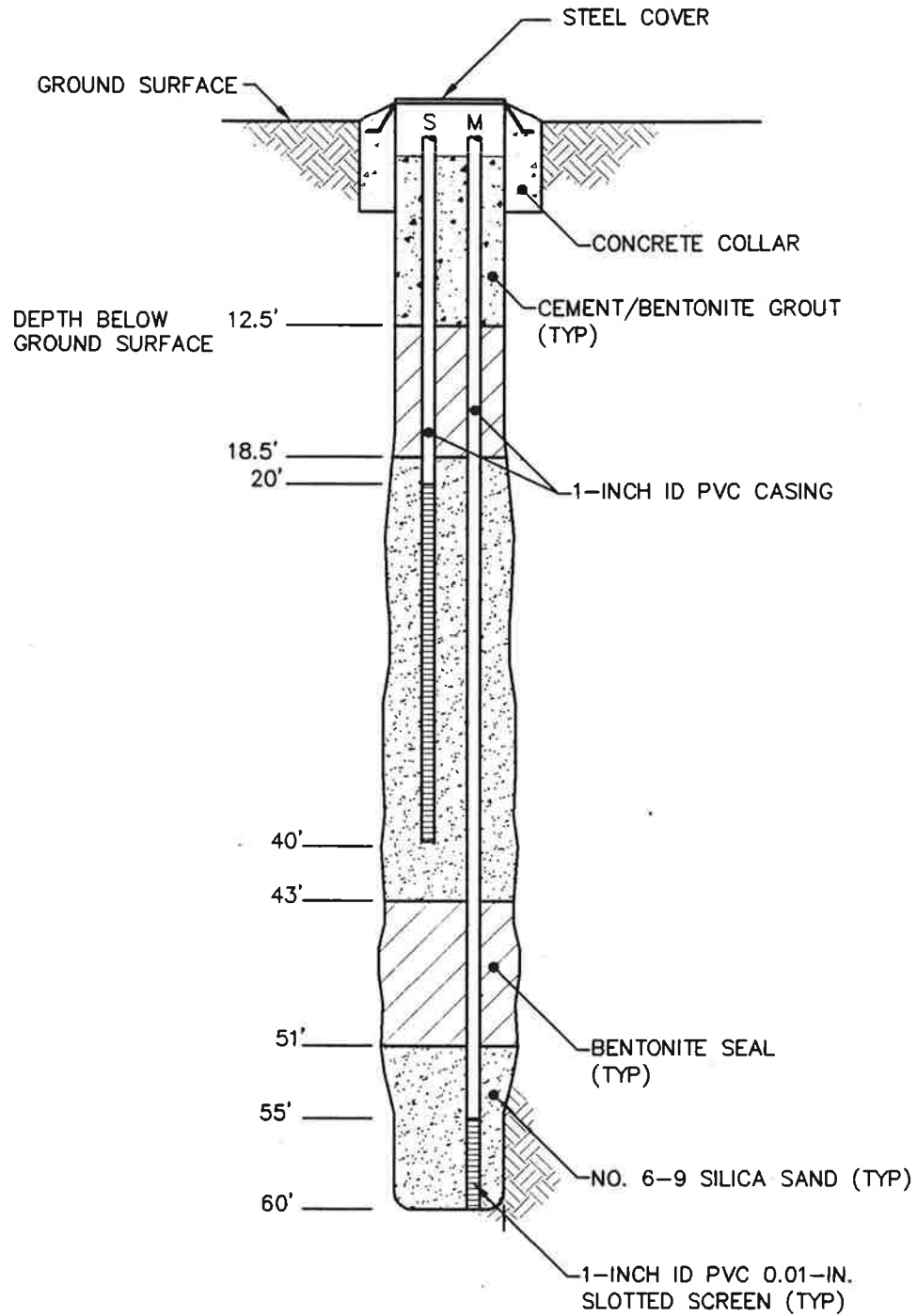
PROJECT NAME: Lake Petit Dam	PROJECT NO.: GL0625	BORING ID: G-5
LOCATION: G-5	N:	E:
DRILLING CO.: AT&E	RIG: CME 750	DRILLER: P. Bergman
METHOD & DIAMETER: Mud Rotary (8-in.)		LOGGED BY: J. Titus
DATE: STARTED- 12 Oct 98	COMPLETED- 14 Oct 98	CHECKED BY: G. Schmertmann

ELEVATION (FEET)	DEPTH (FEET)	DESCRIPTION	SYMBOL	WELL DIAGRAM	Blows/ 6 in.	DRILLING LOG
1607	40				7	Wood debris washing up out of borehole
						Push shelby tube, 15" recovery
1602	45					Pushed shelby tube 6". No recovery. wood debris in end of tube
		SILT, micaceous, trace clay, trace very fine sand, trace wood/roots. Color: red (10R4/8)			2 3 4 7	
1597	50					Increasing wood fragments up to 1" diam.
					4 8 5 6	
1592	55					
						Push shelby tube, 22" recovery
1587	60					Push shelby tube, 14" recovery
		SILT, some clay, trace very fine sand. Color: @ 63-64.5 - red (10R4/8) @ 64.5-65 - dark gray (5YR4/1)			4 5 6 8	
1582	65					
		Boring terminated at 67.00 feet				
1577	70					
1572	75					
1567	80					

L:\LPD\LOGS\G5.P1.3 JD1-1 11-24-98

REMARKS:

G-1A PIEZOMETER CLUSTER CONSTRUCTION DETAIL

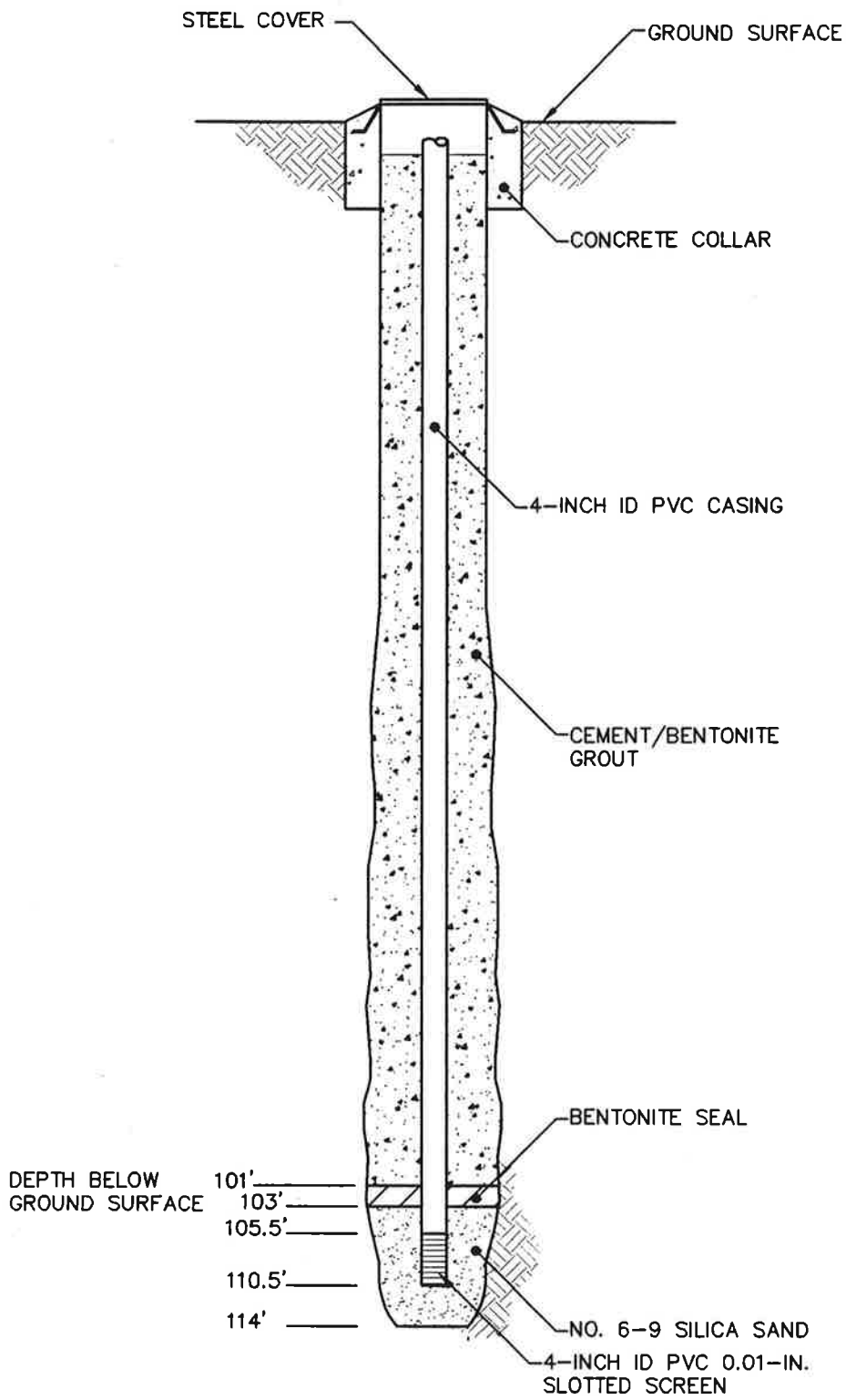


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FIGURE NO.	A-1
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	0625F003.DWG

G-1B PIEZOMETER CONSTRUCTION DETAIL

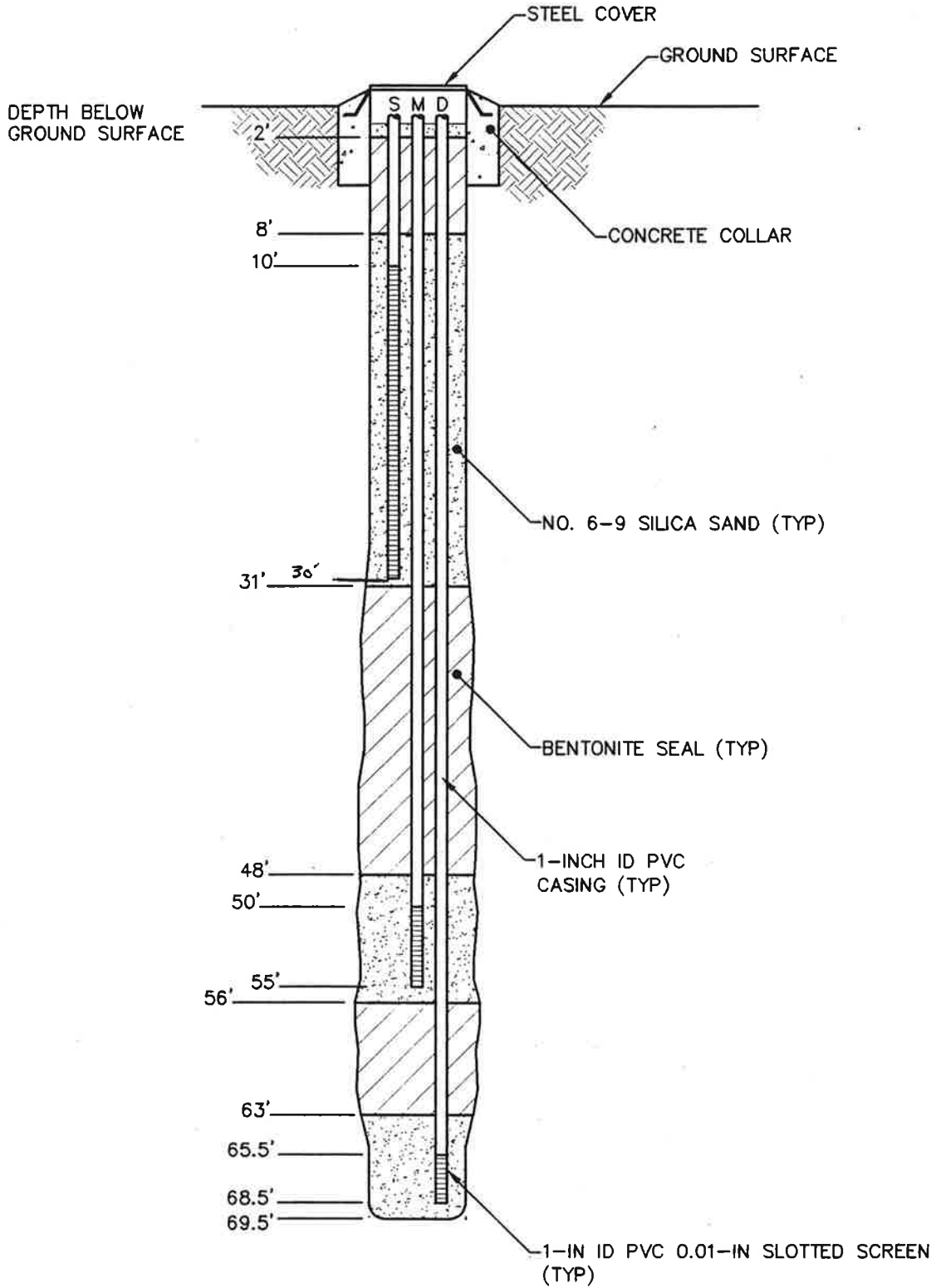


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FIGURE NO.	A-2
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	0625F002.DWG

G-2 PIEZOMETER CLUSTER CONSTRUCTION DETAIL



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FIGURE NO.	A-3
PROJECT NO.	GL0625-15
DOCUMENT NO.	GA981181
FILE NO.	0625F001.DWG

TABLE

**ELEVATIONS FOR STANDPIPE PIEZOMETERS
(GEOSYNTEC, INSTALLED 1998)**

Piezometer ID	Top of Casing Elevation ⁽¹⁾ (feet above MSL)	Ground Elevation ⁽¹⁾ (feet above MSL)
G-1As	1626.70	1626.8
G-1Ad	1626.81	1626.9
G-1B	1626.84	1626.9
G-2s	1584.7	1584.8
G-2m	1584.7	1584.8
G-2d	1584.7	1584.8
G-3	1563.84	1564.0

Note: (1) Elevations from GPS survey performed by GeoSyntec on 15 October 1998.
MSL - Mean Sea Level

APPENDIX II

SEISMIC DOWNHOLE TESTING REPORT

October 21, 1998

John M. Callaham
Geosyntec Consultants
1100 Lake Hern Drive NE, Suite 200
Atlanta, Georgia 30342-1523

Subject: **Report of Seismic Downhole Testing
Lake Petit Dam
Big Canoe, Georgia
Law Project No. 12000-8-0078 Phase 02**

Dear Mr. Callaham:

Seismic downhole testing was conducted at the Lake Petit dam in the Big Canoe private community in northern Georgia. The work in this report was outlined in Law Engineering and Environmental Services (LAW) Proposal Number 12050-8-9000 Task 18. The purpose of the seismic downhole testing was to gather compression and shear wave velocities of the in situ materials to enable earthquake response analysis of the dam.

Field Investigation

The field investigation consisted of seismic downhole tests to measure seismic velocities. The field work was conducted by John Chulick and Brian Black of Law on October 8, 1998. Seismic downhole tests were performed in two borings (G-1A and G-5). Each boring had been drilled and 4-inch PVC casing had been installed and grouted in place in preparation for the seismic downhole testing.

Boring G-1A was located on the downstream slope of the dam about one-fifth of the distance below the crest. Drilling records provided by Geosyntec showed that the boring was terminated about 114 feet in depth and was completed as a monitoring well with a final depth of 110 feet. At the time of the seismic downhole testing, G-1A had water at 27 feet and the borehole geophones could not be lowered below 103 feet.

Boring G-5 was located on the crest of the dam at the downstream edge of the road that crosses the dam. Drilling records provided by Geosyntec show that the boring was drilled to 67 feet and had PVC casing installed with a final depth of 66.5 feet.

The test equipment consisted of a Geometrics Strataview digital seismograph, three triaxial borehole geophones, and surface energy sources. In a given test measurement, the three triaxial geophones were separated by five feet and temporarily fixed to the borehole casing using bladders inflated by nitrogen. Recordings were made with all three geophones for each measurement setup in the boring. The geophone cables were marked at even increments to allow accurate positioning of the geophones. Recordings were made at ten-foot intervals, giving complete coverage of the boring and providing repeated data every ten feet.

Three recordings were made at each test depth. One recording was optimized for compression waves and two recordings were optimized for shear waves at each test depth. The recorded signals were stored digitally for later processing and analysis. The compression wave source consisted of a vertical hammer blow on a metal plate placed ten feet from the boring. The shear wave source consisted of horizontal hammer blows made from each end of an eight-foot wooden beam placed about ten feet from the boring and fixed in place by the weight of a vehicle.

Seismic Data Analysis

The seismic downhole data were analyzed by viewing each recording on a computer and identifying the first arrival time of the compression and shear waves at each geophone component. Nine channels of data (one for each component of three triaxial geophones) were examined for each recording and the arrival times of the compression and shear waves were identified. Then, the arrival times were used with the source to receiver distances to compute seismic wave velocities at various depths.

Seismic velocities were computed using five and ten foot intervals between geophones. Compression and shear wave velocities were computed by dividing by the differences in the arrival times at two geophones by the differences in the distances between the geophones and the source. Because of the relatively short time intervals between compression wave arrivals, it was sometimes necessary to compute velocities from recordings taken at larger differential depths. Direct source-geophone velocities were computed near the surface. Poisson's Ratio can be calculated for each depth interval where both compression and shear wave velocities have been computed. The dimensionless value of Poisson's Ratio (μ) is given by the following relationship:

$$\mu = \frac{1 - 1/2 \left(\frac{V_p}{V_s} \right)^2}{1 - \left(\frac{V_p}{V_s} \right)^2}$$

where V_p is the compression wave velocity and V_s is the shear wave velocity. For ideal elastic materials, Poisson's Ratio ranges from 0 to 0.5. Values are frequently near 0.5 in saturated unconsolidated soils. Rock often has Poisson's Ratio values near the middle part of the range (0.2 to 0.3), although a value in this range does not necessarily denote rock. Very low (and negative) values may be due to the seismic wave velocities not measuring the same materials, i.e., rock on one side of the boring and soil on the other at the same depths.

Seismic Downhole Test Results

The compression and shear wave velocities and the Poisson's ratios at borings G-1A and G-5 are presented on Tables 1 and 2. Figures 1 and 2 show the compression and shear wave velocities plotted versus depth. Compression wave velocities ranged from 1,212 to 6,142 feet per second (ft/s).

October 21, 1998

Shear wave velocities ranged from 457 to 1,846 ft/s. Shallow soils generally yield lower velocities; however, slightly higher velocities were observed at the top of G-5 probably due to the road and roadbed. Shear wave velocities exceeding 2,500 ft/s are generally considered to represent sound rock, which was not encountered with the seismic downhole testing.

It has been our pleasure to provide our services to Geosyntec Consultants in the preparation of this report. If you have any questions concerning this report, or when we may be of further service, we hope that you will contact us at your convenience.

Sincerely,



John A. Chulick, P.G.
Senior Geophysicist



Joseph R. Wilson, Ph.D., P.G.
Principal

Table 1: Seismic Velocities at G-1A

Depth Range	Midpoint (ft)	Vp (ft/s)	Vs (ft/s)	Poisson's Ratio
0-5	2.5	1212	648	0.30
5-10	7.5	1889	816	0.39
10-15	12.5	1317	957	-0.06
15-20	17.5	1693	1333	-0.32
20-25	22.5	1976	1074	0.29
25-30	27.5	1725	1105	0.15
30-35	32.5	4049	1466	0.42
35-40	37.5	1455	805	0.28
40-45	42.5	1737	1025	0.23
45-50	47.5	3262	1447	0.38
50-55	52.5	1589	1140	-0.03
55-60	57.5	1924	1293	0.09
60-65	62.5	1849	1178	0.16
65-70	67.5	2123	1846	-1.05
70-75	72.5	2566	1342	0.31
75-80	77.5	3042	882	0.45
80-85	82.5	4206	1324	0.45
85-90	87.5	3600	1501	0.39
90-95	92.5	1890	1471	-0.27
95-98	96.5	1990	1305	0.12
98-103	100.5	6142	1422	0.47

Table 2: Seismic Velocities at G-5

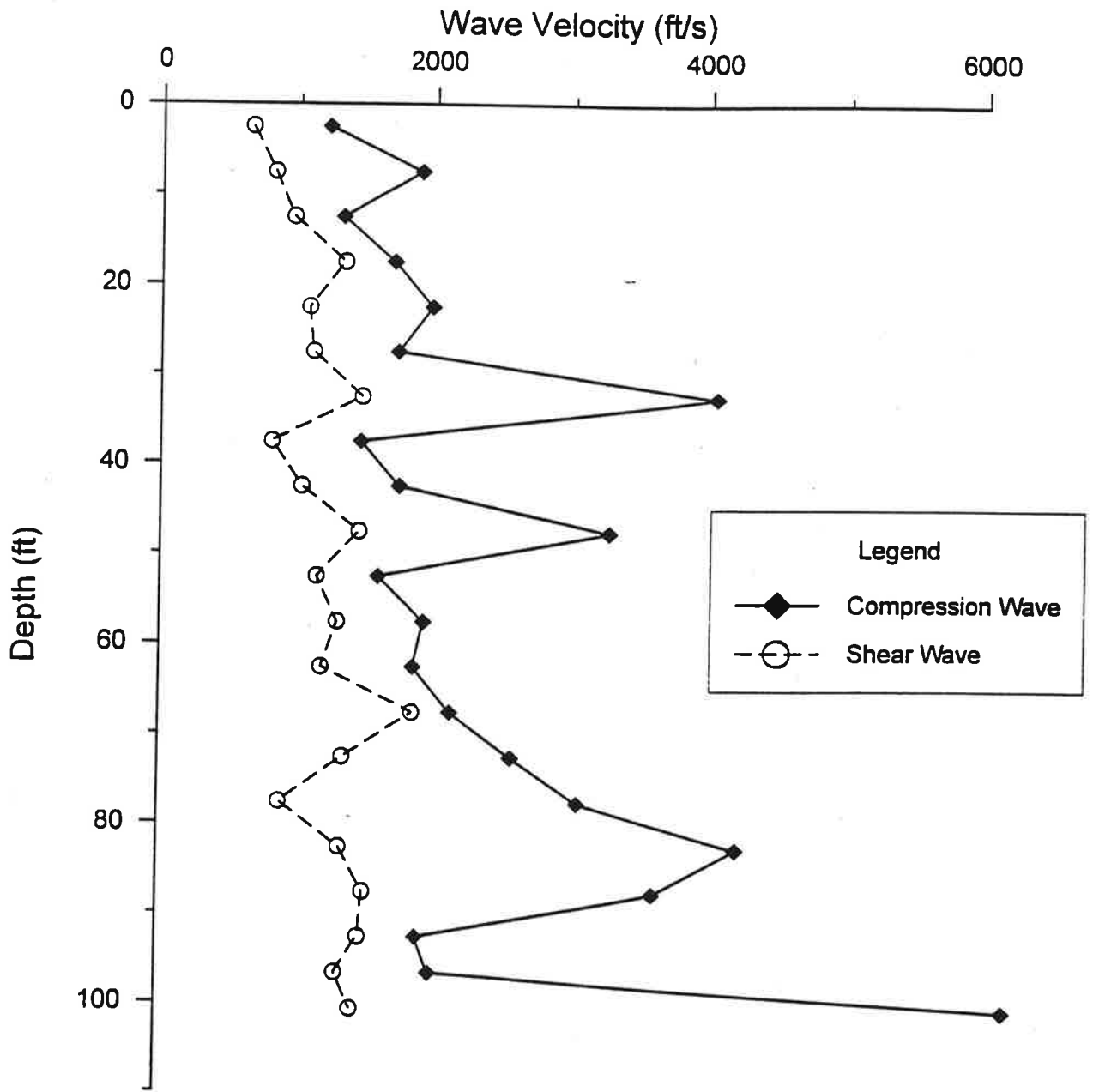
Depth Range	Midpoint (ft)	Vp (ft/s)	Vs (ft/s)	Poisson's Ratio
0-5	2.5	2055	1344	0.13
5-10	7.5	2055	539	0.46
10-15	12.5	1554	457	0.45
15-20	17.5	1444	822	0.26
20-25	22.5	2216	1436	0.14
25-30	27.5	2421	854	0.43
30-35	32.5	1958	1316	0.09
35-40	37.5	4557	1313	0.45
40-45	42.5	1415	949	0.09
45-50	47.5	2375	1223	0.32
50-55	52.5	1965	1021	0.32
55-60	57.5	4398	1484	0.44
61-66	63.5	5254	908	0.48

Table 1: Seismic Velocities at G-1A

Depth Range	Midpoint (ft)	Vp (ft/s)	Vs (ft/s)	Poisson's Ratio
0-5	2.5	1212	648	0.30
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30-35	32.5	4049	1466	0.42
35-40	37.5	1455	805	0.28
40-45	42.5	1737	1025	0.23
45-50	47.5	3262	1447	0.38
50-55	52.5	1589	1140	-0.03
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60-65	62.5	1849	1178	0.16
65-70	67.5	2123	1846	-1.05
70-75	72.5	2566	1342	0.31
75-80	77.5	3042	882	0.45
80-85	82.5	4206	1324	0.45
85-90	87.5	3600	1501	0.39
90-95	92.5	1890	1471	-0.27
95-98	96.5	1990	1305	0.12
98-103	100.5	6142	1422	0.47

Table 2: Seismic Velocities at G-5

Depth Range	Midpoint (ft)	Vp (ft/s)	Vs (ft/s)	Poisson's Ratio
0-5	2.5	2055	1344	0.13
5-10	7.5	2055	539	0.46
10-15	12.5	1554	457	0.45
15-20	17.5	1444	822	0.26
20-25	22.5	2216	1436	0.14
25-30	27.5	2421	854	0.43
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50-55	52.5	1965	1021	0.32
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61-66	63.5	5254	908	0.48



GEOSYNTEC CONSULTANTS
BIG CANOE, GEORGIA

LAW

LAWGIBB Group Member



G-1A
SEISMIC VELOCITIES

Job No. 12000-8-0078 Figure 1