

APPENDIX C

LABORATORY TEST RESULTS



GEO SYNTEC CONSULTANTS

Geomechanics and Environmental
Laboratory

Sample ID: G-4 (D) (15'-16')

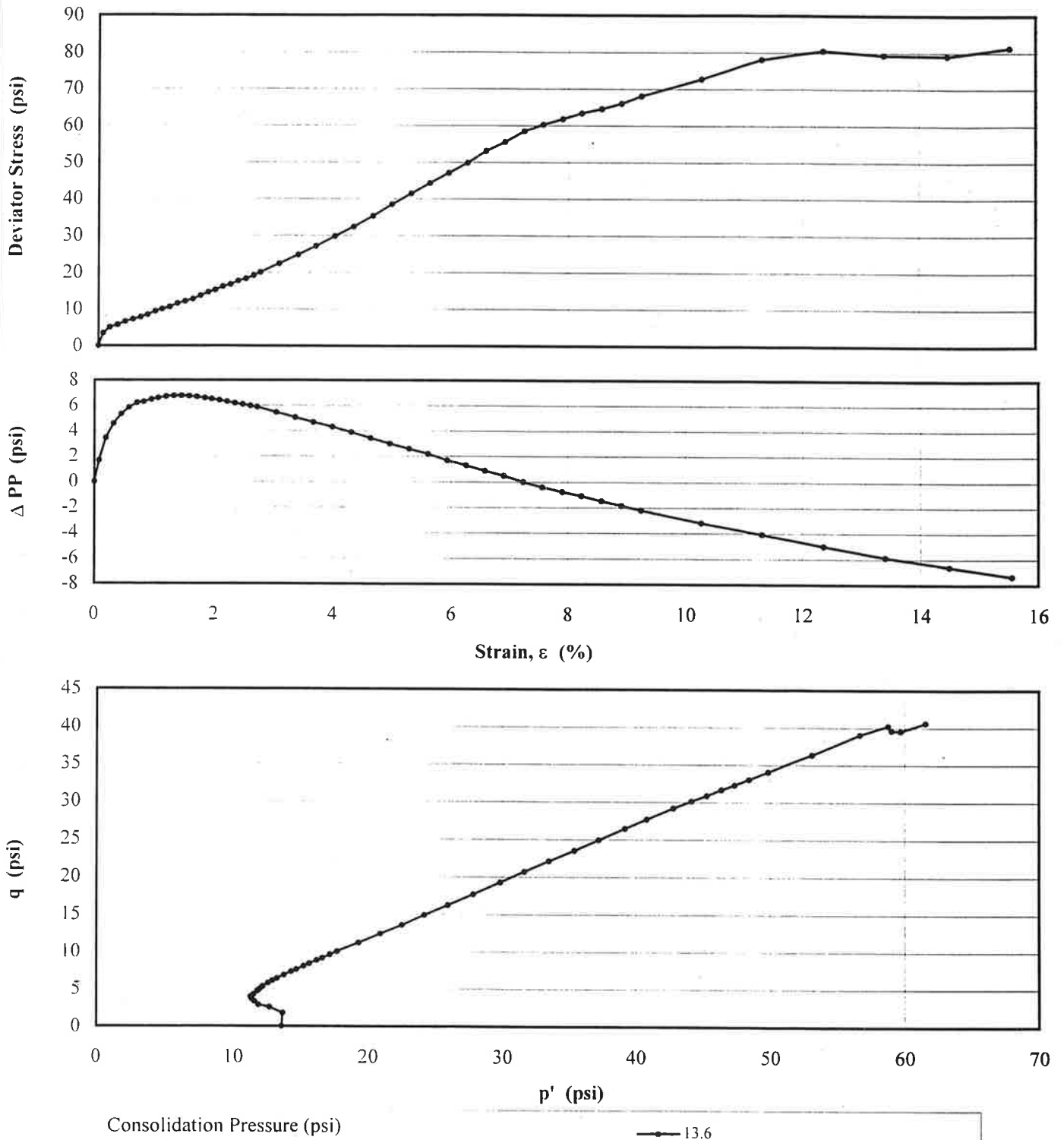
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 1



Note:

1. Due to equipment malfunctioning, axial load piston generated friction forces beyond the recommended standard practice resulting in very high zero load correction.

TABLE 1

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) ⁽¹⁾

Site Sample ID	Lab Sample No.	Specimen Initial Conditions			σ'_c (psi)	Peak				Ultimate				Figure No.	Remarks			
		Height (in.)	Diameter (in.)	Moisture Content (%)		Dry Unit Weight (pcf)	σ'_{1-0} (psi)	σ'_1 (psi)	ϵ_a (%)	u (psi)	σ'_{1-0} (psi)	σ'_1 (psi)	ϵ_a (%)			u (psi)		
G-4 (D) (15'-16')	98J21.1	6.19	2.85	17.7	97.9	50.4	13.6											

Notes:

- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)

1. Due to equipment malfunctioning, axial load piston generated friction forces beyond the recommended standard practice resulting in very high zero load correction.



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Laboratory

Sample ID: G-4 (L) (30'-32')

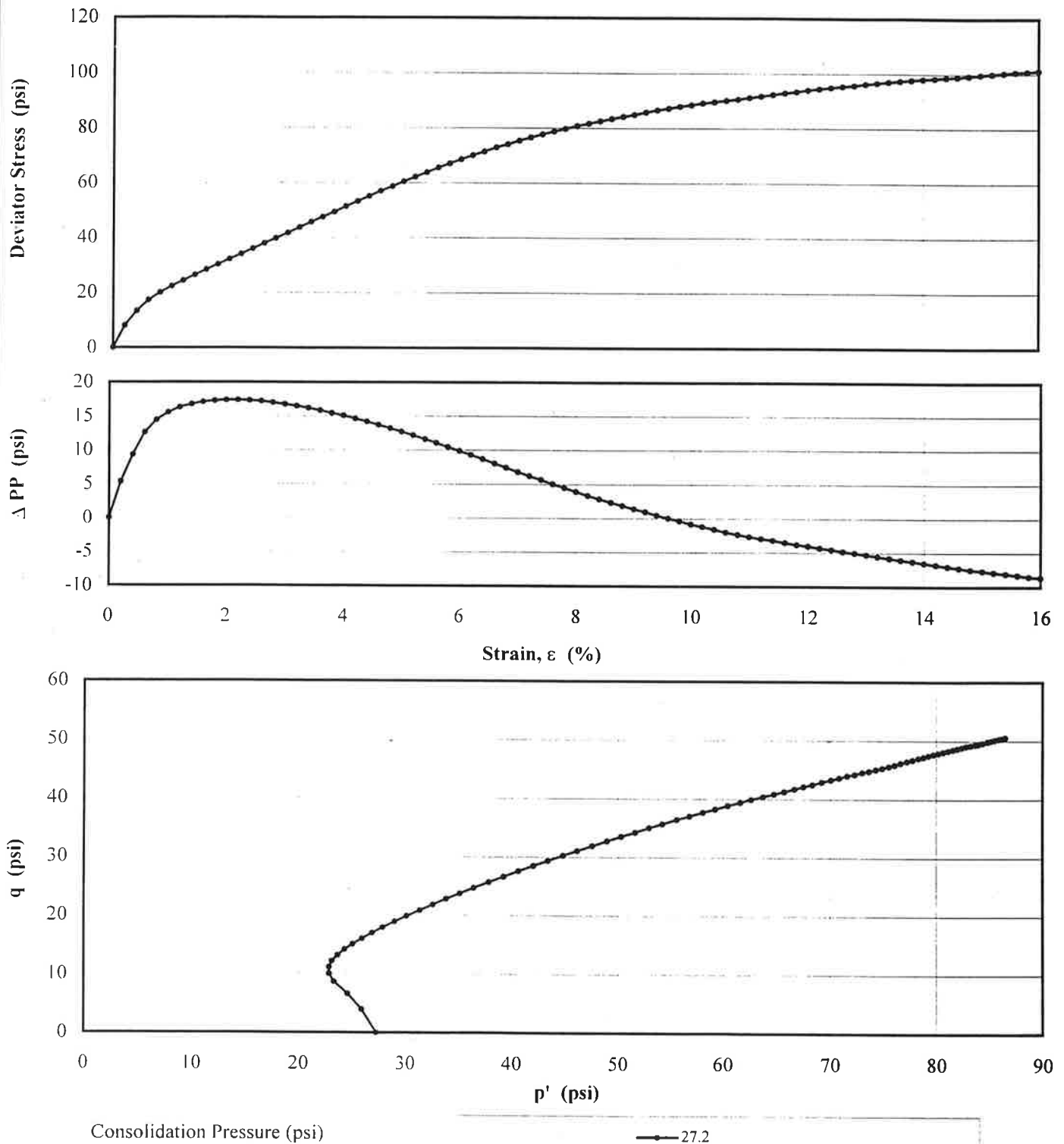
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 2



Note:

TABLE 2

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) ⁽¹⁾

Site Sample ID	Lab Sample No.	Specimen Initial Conditions			σ'_c (psi)	Peak				Ultimate				Figure No.	Remarks					
		Height (in.)	Diameter (in.)	Moisture Content (%)		Dry Unit Weight (pcf)	u_i (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)	u (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)			ϵ_a (%)	u (psi)			
																		$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)
G-4 (I.) (30'-32')	98J41.1	6.73	2.89	27.8	97.2	51.2	27.2												2	

Notes:

- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)

1.



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Sample ID: G-4 (H) (47'-50')

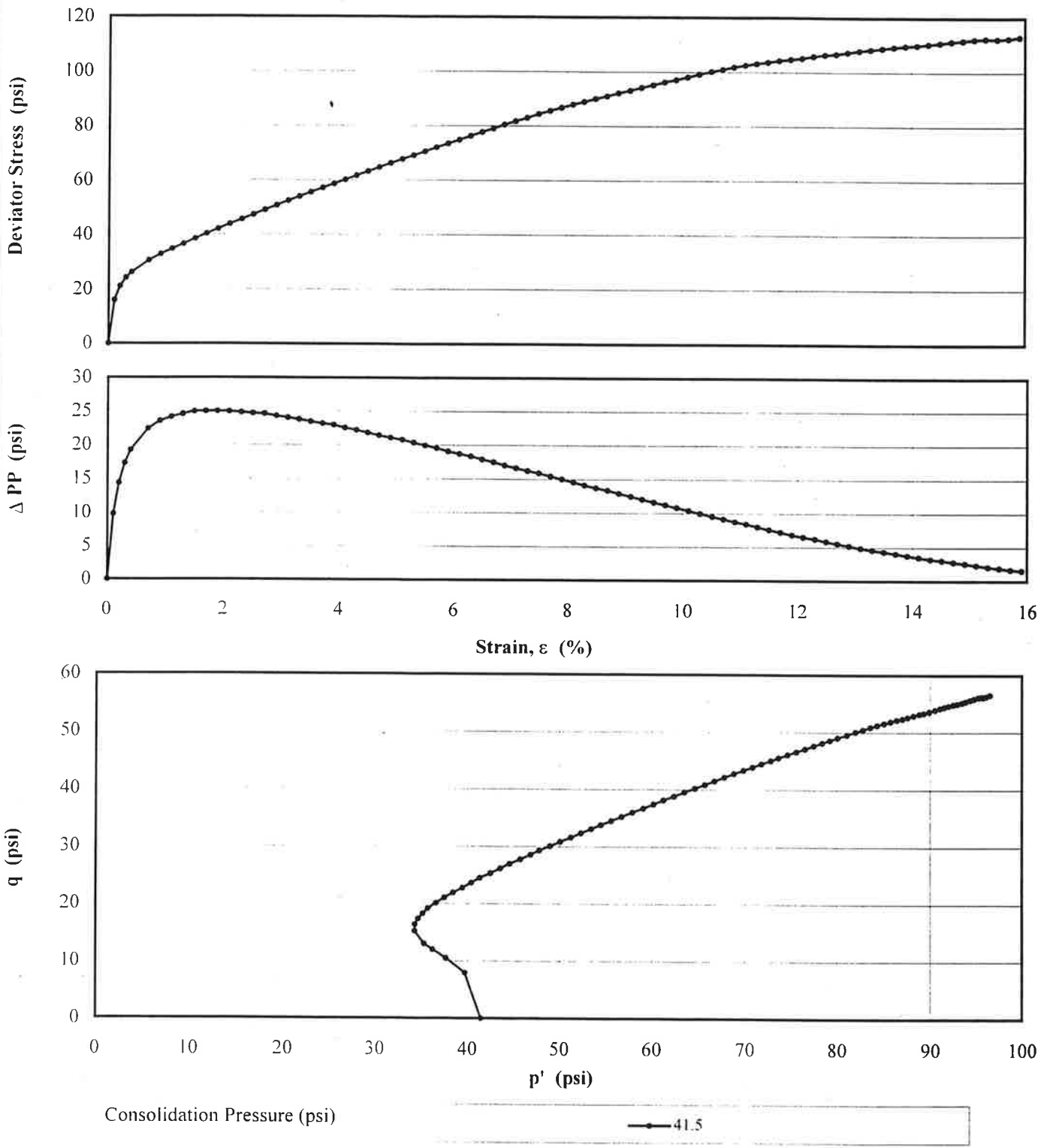
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 3



Note:

TABLE 3

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) (1)

Site Sample ID	Lab Sample No.	Specimen Initial Conditions			Peak			Ultimate			Figure No.	Remarks				
		Height (in.)	Diameter (in.)	Moisture Content (%)	Dry Unit Weight (pcf)	u_i (psi)	σ'_c (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)			u (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)
G-4 (II) (47'-50')	98J42.1	6.93	2.80	25.9	103.1	49.2	41.5					113.1	153.0	15.9	50.8	

Notes:

- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)

1.



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Atlanta, Georgia

FIGURE

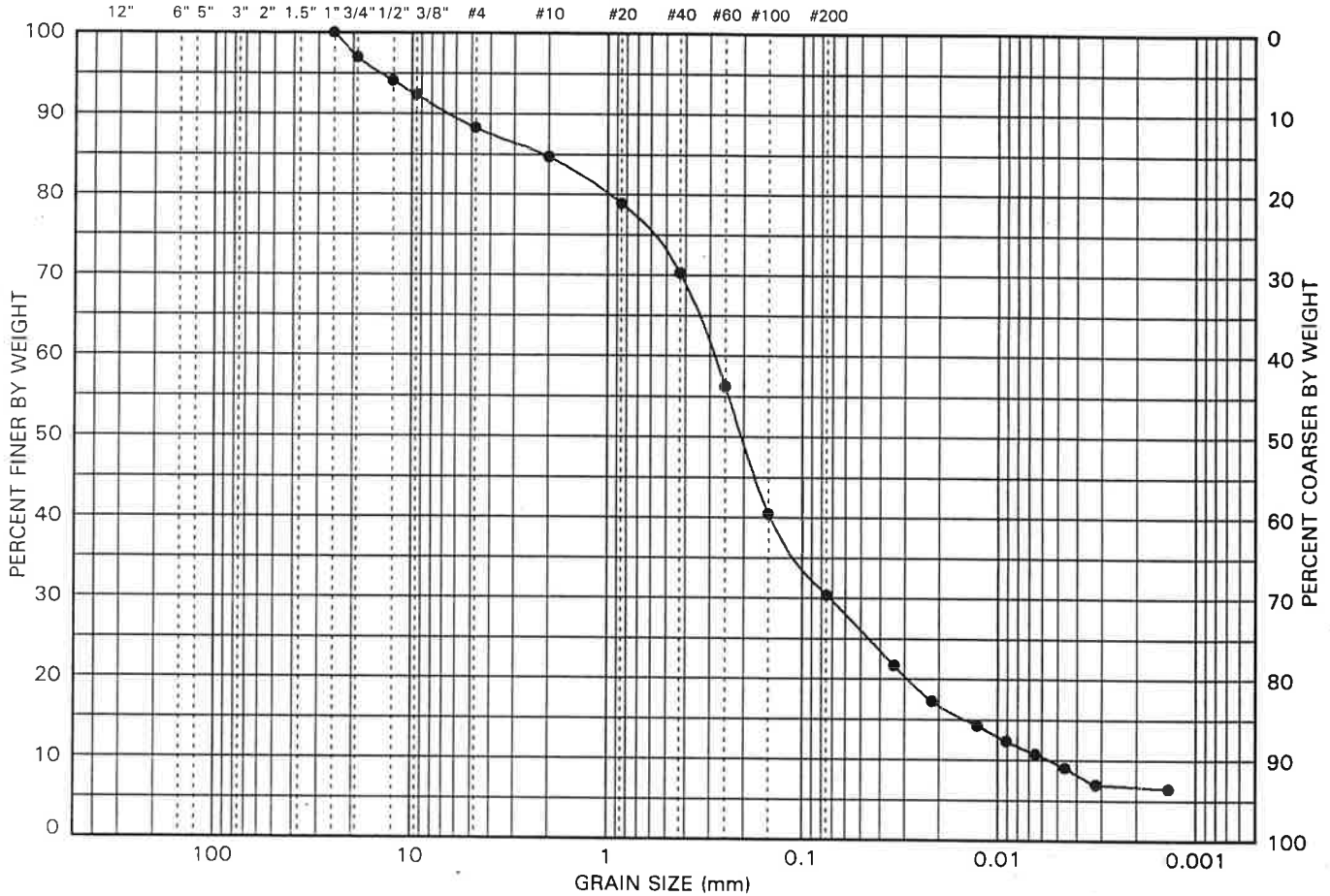
PROJECT: Lake Petit Dam
PROJECT NO.: GL0625
DOCUMENT NO.:

GS FORM:
4PS2 11/05/98

PARTICLE SIZE DISTRIBUTION AND PHYSICAL PROPERTIES

ASTM C 136, D 422, D 2487
D 3042 AND D 4318

U.S. STANDARD SIEVE SIZES AND NUMBERS



BOULDERS	COBBLES	COARSE	FINE	COARSE	MEDIUM	FINE	SILT	CLAY
		GRAVEL		SAND			FINES	

SITE SAMPLE ID *		LIQUID LIMIT (%)		NP	SOIL FRACTIONS	GRAVEL (%)		11.7										
LAB. SAMPLE NO. 98J42		PLASTIC LIMIT (%)		NP		SAND (%)		57.9										
SAMPLE DEPTH (ft)		PLASTICITY INDEX		NP		FINES (%)		30.4										
SOIL CLASSIFICATION: SM - Silty Sand						SILT (%)		23.7										
						CLAY (%)		6.7										
					COEFF. UNIFORMITY (Cu)													
					COEFF. CURVATURE (Cc)													
PERCENT PASSING U.S. STANDARD SIEVE SIZES AND NUMBERS														PERCENT FINER THAN HYDROMETER PARTICLE DIAMETER (mm)				
3"	2"	1.5"	1"	3/4"	1/2"	3/8"	#4	#10	#20	#40	#60	#100	#200	0.050	0.020	0.005	0.002	0.001
PERCENT PASSING SIEVE SIZES (mm)																		
75	50	37.5	25	19	12.5	9.5	4.75	2.00	0.850	0.425	0.250	0.150	0.075	26	17	10	7	
100	100	100	100	97	94	92	88	85	79	70	56	41	30					

NOTES: * G-4(H) (47-50)



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Sample ID: G-1B (E) (20'-22')

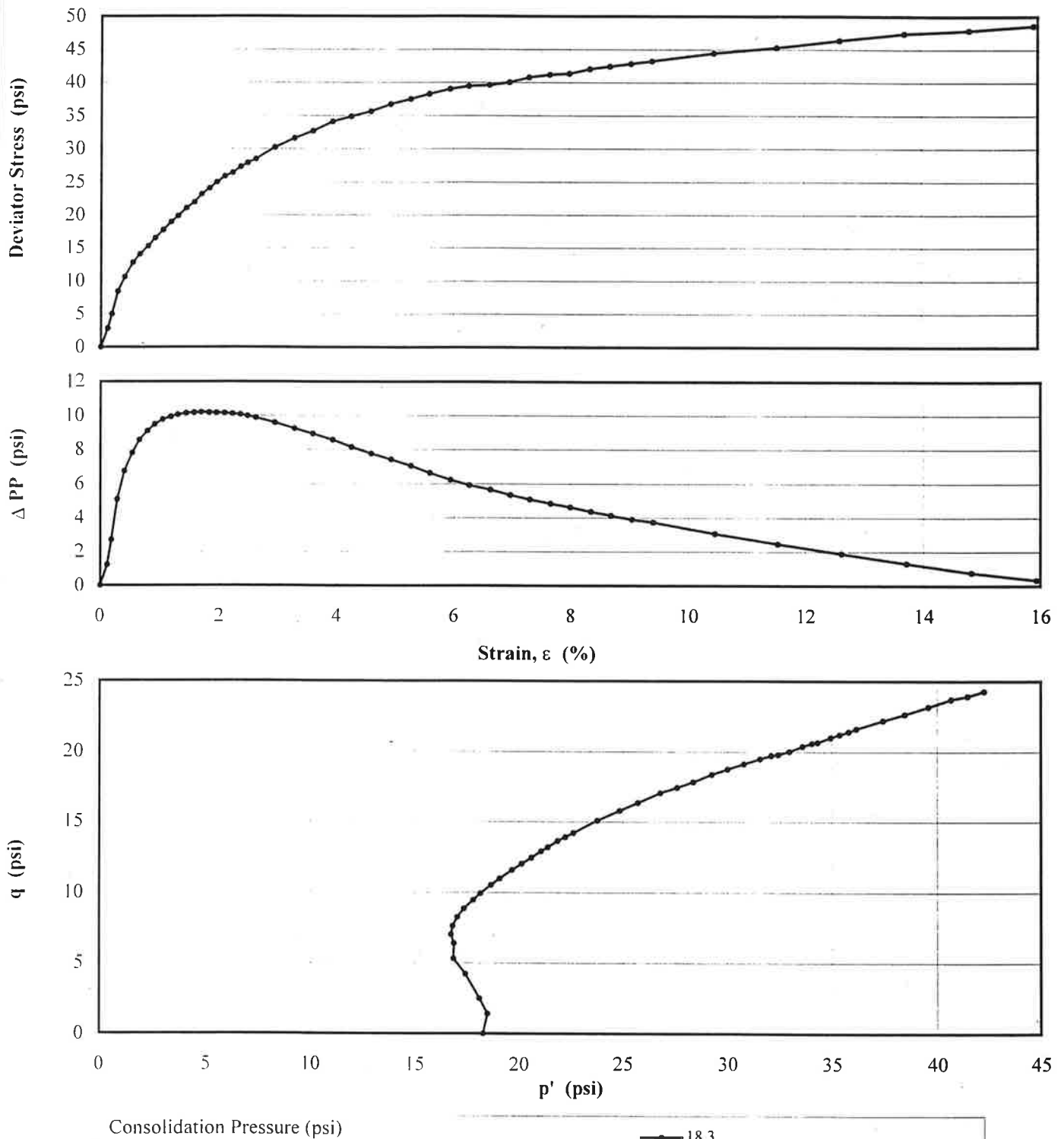
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 4



Note:



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Laboratory

Sample ID: G-1B (E) (20'-22')-Remolded

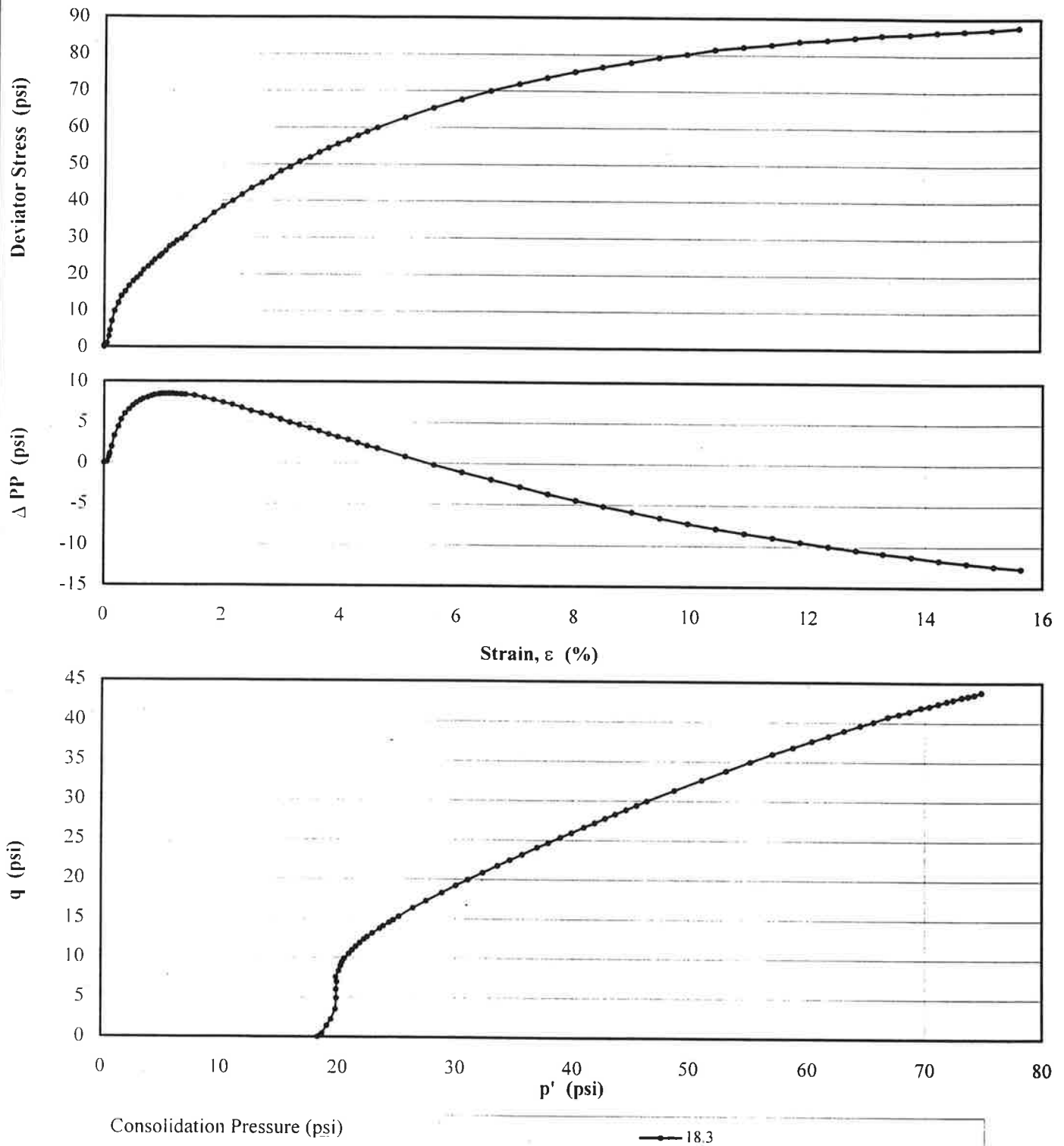
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 5



Note(s):

1. The test specimen was formed/remolded by recycling the tested (sheared) undisturbed Shelby tube specimen. The test material was passed through a U.S. Standard No. 3/8" sieve. The passing portion was remolded at a moisture content of 16.9% and at a dry unit weight of 102.8 pcf.
2. The test specimen was initially consolidated at 23.8 psi, and then was over-consolidated and sheared at 18.3 psi.



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Sample ID: G-1B (H) (38'-40')

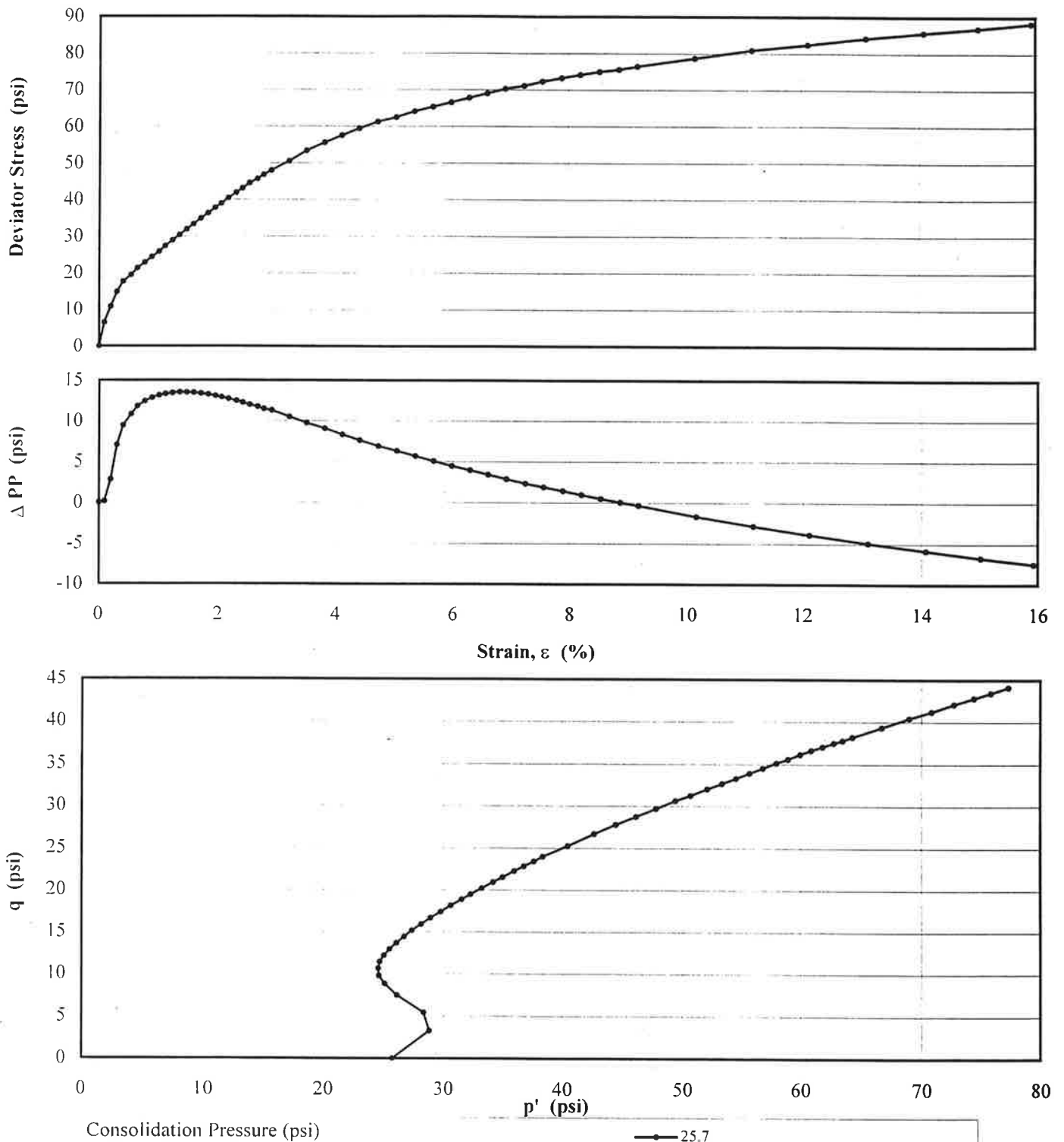
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 6



Note:



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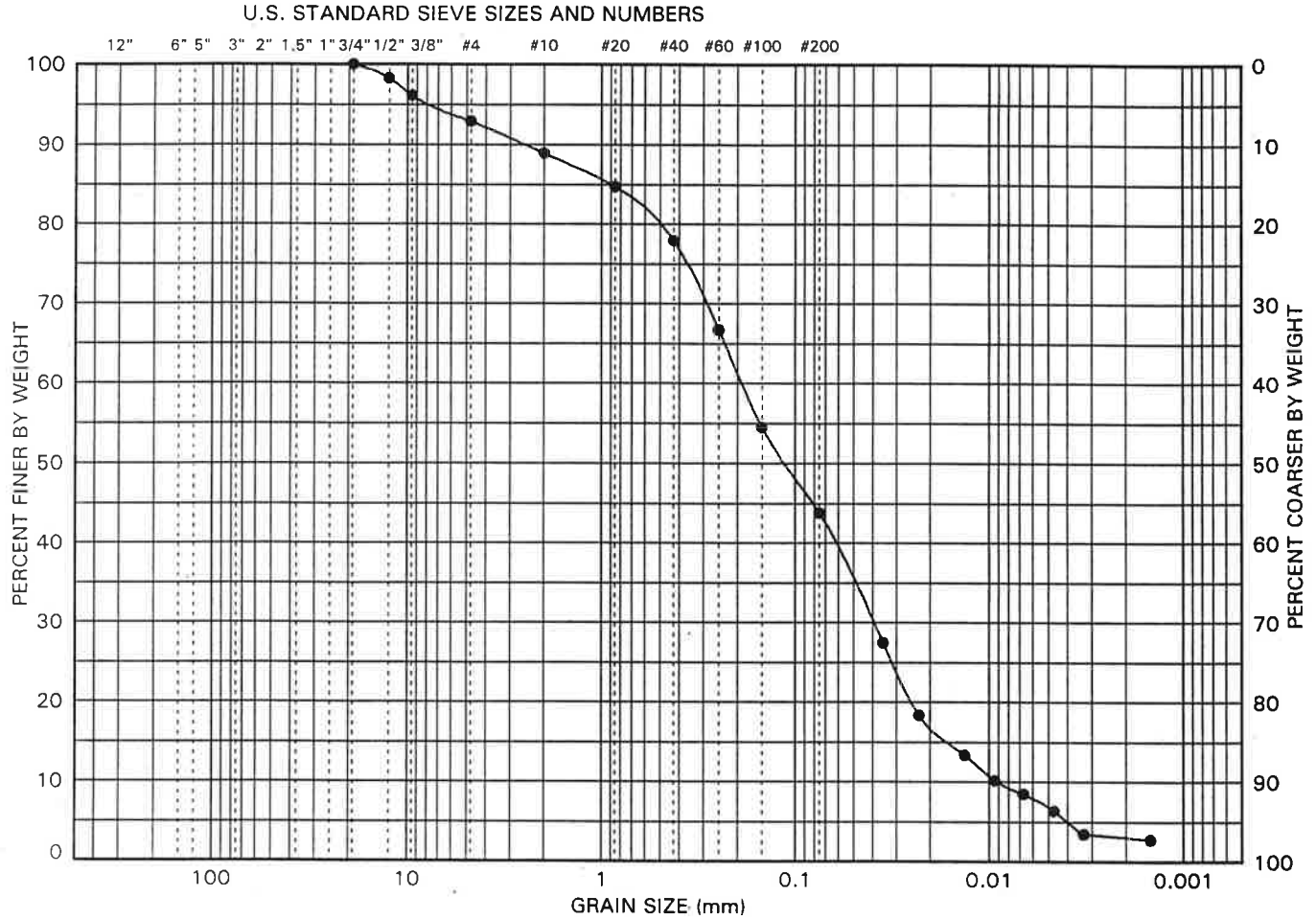
FIGURE

PROJECT: Lake Petit Dam
 PROJECT NO.: GL0625
 DOCUMENT NO.:

GS FORM:
 4PS2 10/26/98

PARTICLE SIZE DISTRIBUTION AND PHYSICAL PROPERTIES

ASTM C 136, D 422, D 2487
 D 3042 AND D 4318



BOULDERS	COBBLES	COARSE	FINE	COARSE	MEDIUM	FINE	SILT	CLAY
		GRAVEL		SAND				

SITE SAMPLE ID	*	LIQUID LIMIT (%)	33	SOIL FRACTIONS	GRAVEL (%)	7.1
LAB. SAMPLE NO.	98J68	PLASTIC LIMIT (%)	30		SAND (%)	49.1
SAMPLE DEPTH (ft)		PLASTICITY INDEX	3		FINES (%)	43.8
SOIL CLASSIFICATION: SM - Silty Sand					SILT (%)	40.7
					CLAY (%)	3.1
				COEFF. UNIFORMITY (Cu)		
				COEFF. CURVATURE (Cc)		

PERCENT PASSING U.S. STANDARD SIEVE SIZES AND NUMBERS														PERCENT FINER THAN HYDROMETER PARTICLE DIAMETER (mm)				
3"	2"	1.5"	1"	3/4"	1/2"	3/8"	#4	#10	#20	#40	#60	#100	#200	0.050	0.020	0.005	0.002	0.001
PERCENT PASSING SIEVE SIZES (mm)																		
75	50	37.5	25	19	12.5	9.5	4.75	2.00	0.850	0.425	0.250	0.150	0.075	35	17	7	3	
100	100	100	100	100	98	96	93	89	85	78	67	55	44					

NOTES: * G-1B(H) (38-40)



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Sample ID: G-1B (P) (80'-81.5')

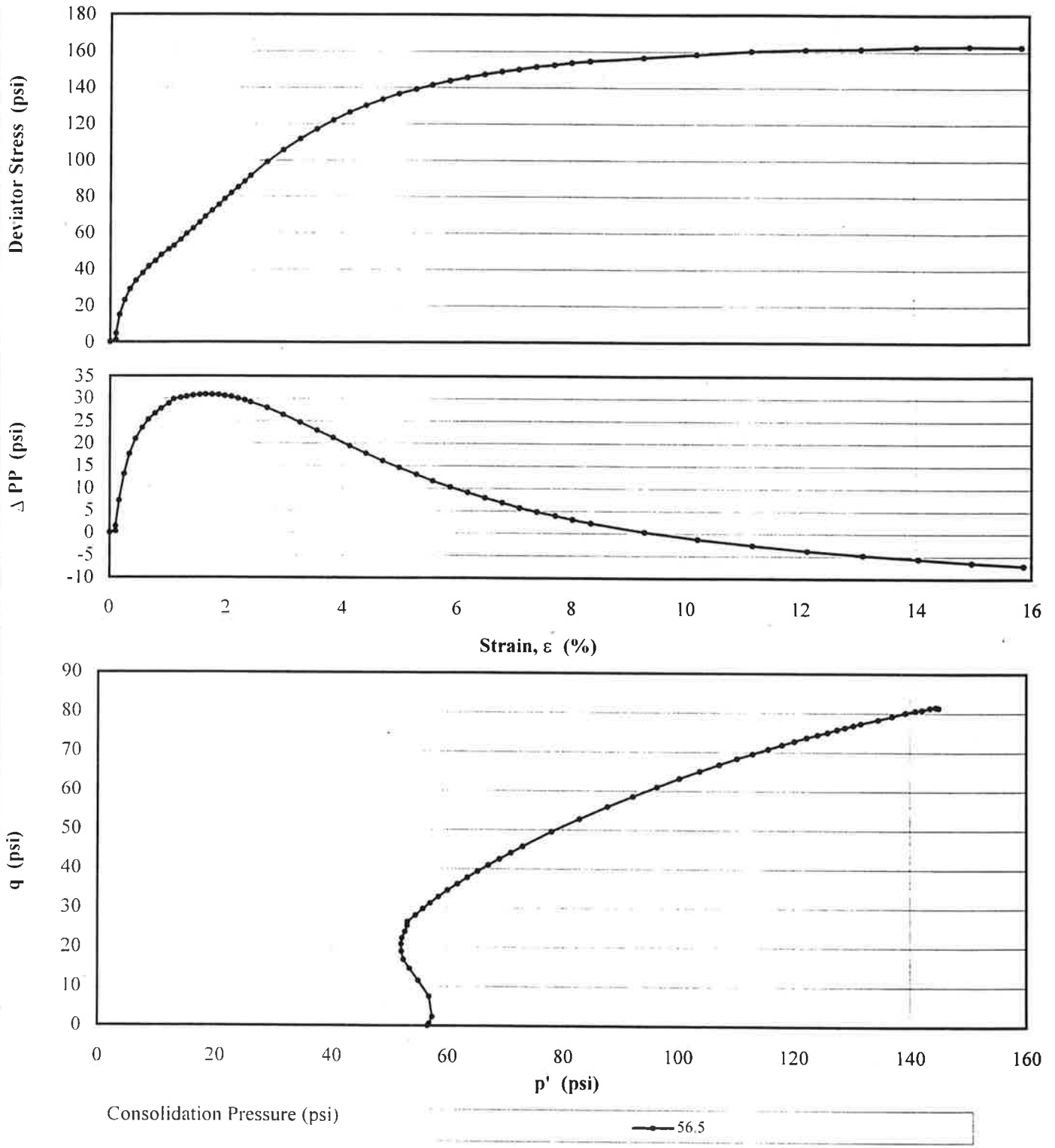
Project Name: LAKE PETIT DAM

Project No.: GLG0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 7



Note:



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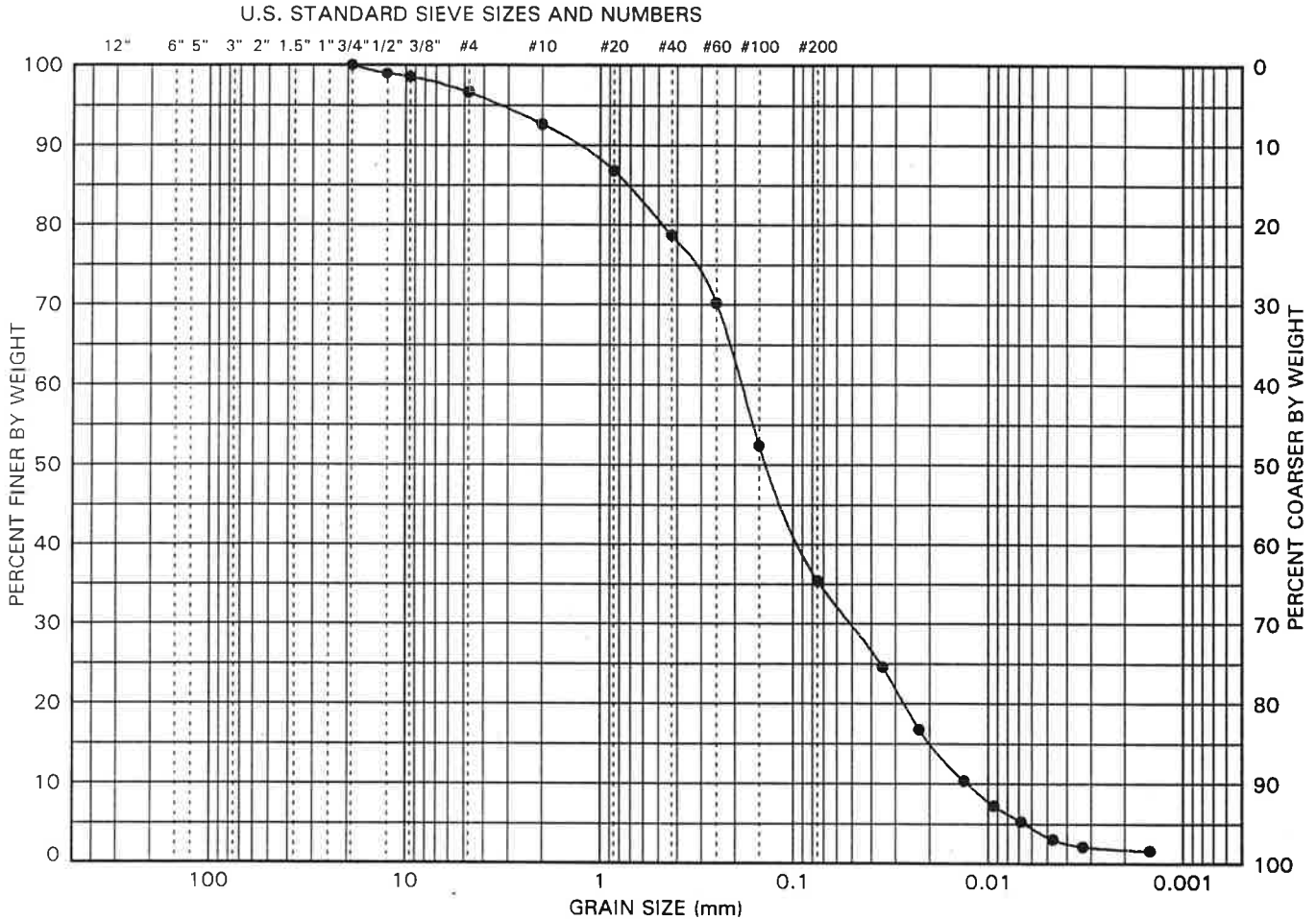
FIGURE

PROJECT: Lake Petit Dam
 PROJECT NO.: GL0625
 DOCUMENT NO.:

GS FORM:
 4PS2 10/26/98

PARTICLE SIZE DISTRIBUTION AND PHYSICAL PROPERTIES

ASTM C 136, D 422, D 2487
 D 3042 AND D 4318



BOULDERS	COBBLES	COARSE	FINE	COARSE	MEDIUM	FINE	SILT		CLAY
		GRAVEL		SAND			FINES		

SITE SAMPLE ID *		LIQUID LIMIT (%)		NP	SOIL FRACTIONS	GRAVEL (%)		3.4										
LAB. SAMPLE NO. 98J75		PLASTIC LIMIT (%)		NP		SAND (%)		61.2										
SAMPLE DEPTH (ft)		PLASTICITY INDEX		NP		FINES (%)		35.4										
SOIL CLASSIFICATION: SM - Silty Sand						SILT (%)		33.5										
					CLAY (%)		1.9											
					COEFF. UNIFORMITY (Cu)													
					COEFF. CURVATURE (Cc)													
PERCENT PASSING U.S. STANDARD SIEVE SIZES AND NUMBERS														PERCENT FINER THAN HYDROMETER PARTICLE DIAMETER (mm)				
3"	2"	1.5"	1"	3/4"	1/2"	3/8"	#4	#10	#20	#40	#60	#100	#200	0.050	0.020	0.005	0.002	0.001
PERCENT PASSING SIEVE SIZES (mm)																		
75	50	37.5	25	19	12.5	9.5	4.75	2.00	0.850	0.425	0.250	0.150	0.075					
100	100	100	100	100	99	99	97	93	87	79	70	52	35	30	15	3	2	

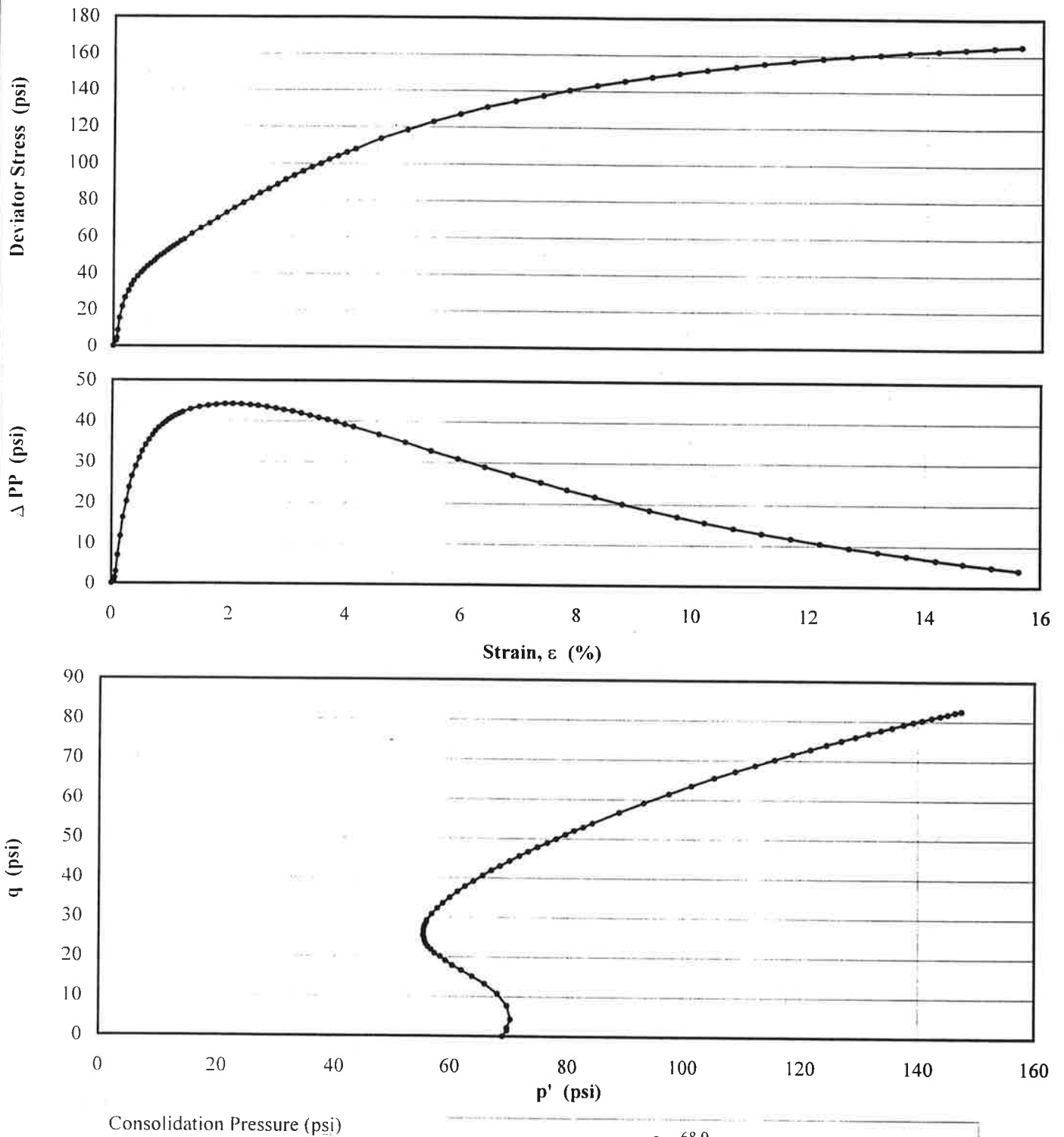
NOTES: * G-1B(P) (80-81.5)



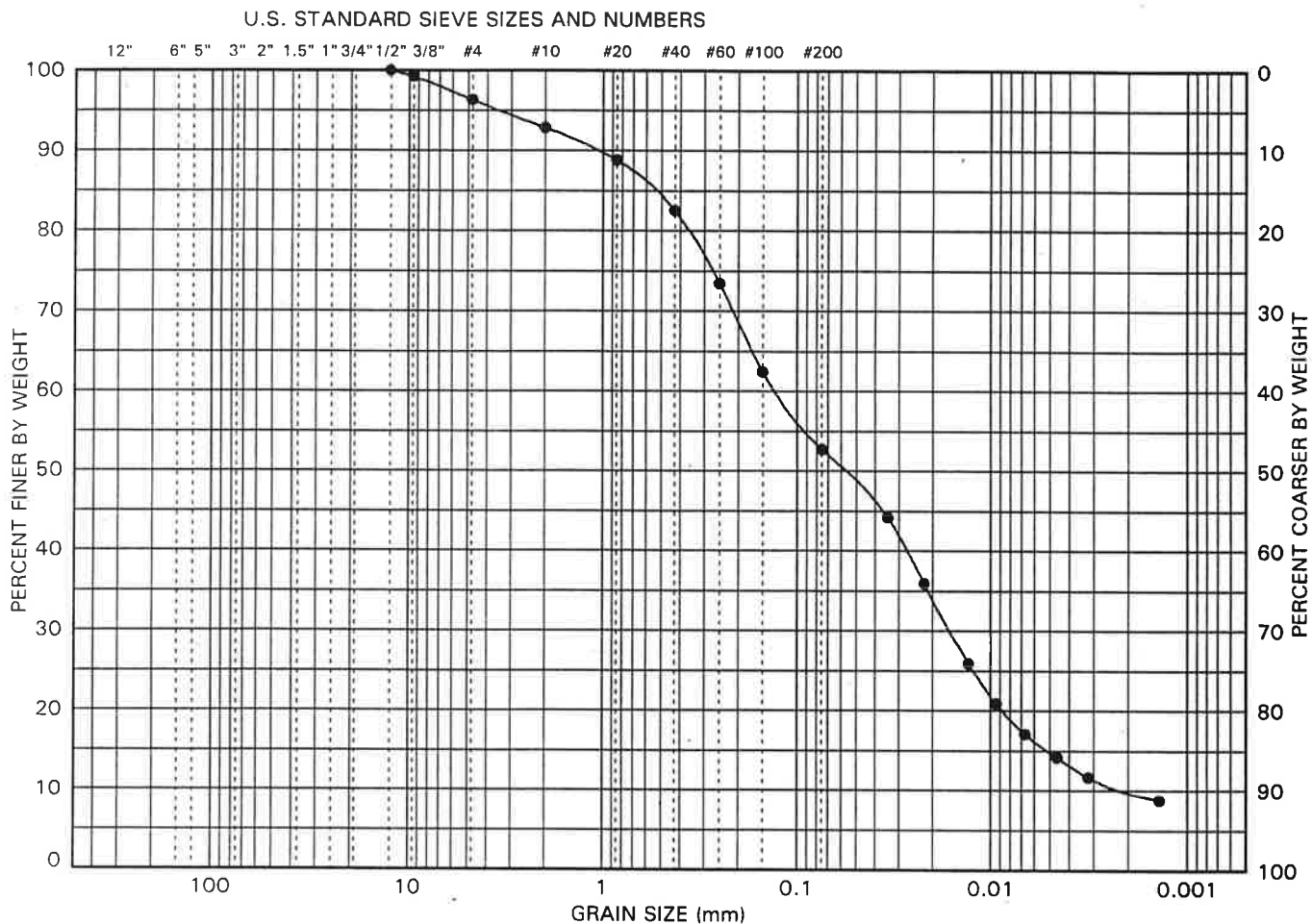
ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 8



Note:



BOULDERS	COBBLES	COARSE	FINE	COARSE	MEDIUM	FINE	SILT	CLAY
		GRAVEL		SAND			FINES	

SITE SAMPLE ID *		LIQUID LIMIT (%)		41		SOIL FRACTIONS	GRAVEL (%)		3.7									
LAB. SAMPLE NO. 98J76		PLASTIC LIMIT (%)		32			SAND (%)		43.6									
SAMPLE DEPTH (ft)		PLASTICITY INDEX		9			FINES (%)		52.7									
SOIL CLASSIFICATION: ML - Sandy Silt							SILT (%)		42.6									
							CLAY (%)		10.1									
						COEFF. UNIFORMITY (Cu)												
						COEFF. CURVATURE (Cc)												
PERCENT PASSING U.S. STANDARD SIEVE SIZES AND NUMBERS														PERCENT FINER THAN HYDROMETER PARTICLE DIAMETER (mm)				
3"	2"	1.5"	1"	3/4"	1/2"	3/8"	#4	#10	#20	#40	#60	#100	#200	0.050	0.020	0.005	0.002	0.001
PERCENT PASSING SIEVE SIZES (mm)																		
75	50	37.5	25	19	12.5	9.5	4.75	2.00	0.850	0.425	0.250	0.150	0.075	48	34	15	10	
100	100	100	100	100	100	99	96	93	89	83	73	62	53					

NOTES: * G-1B(U) (105-107)



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Sample ID: G-5 (G) (27'-30')

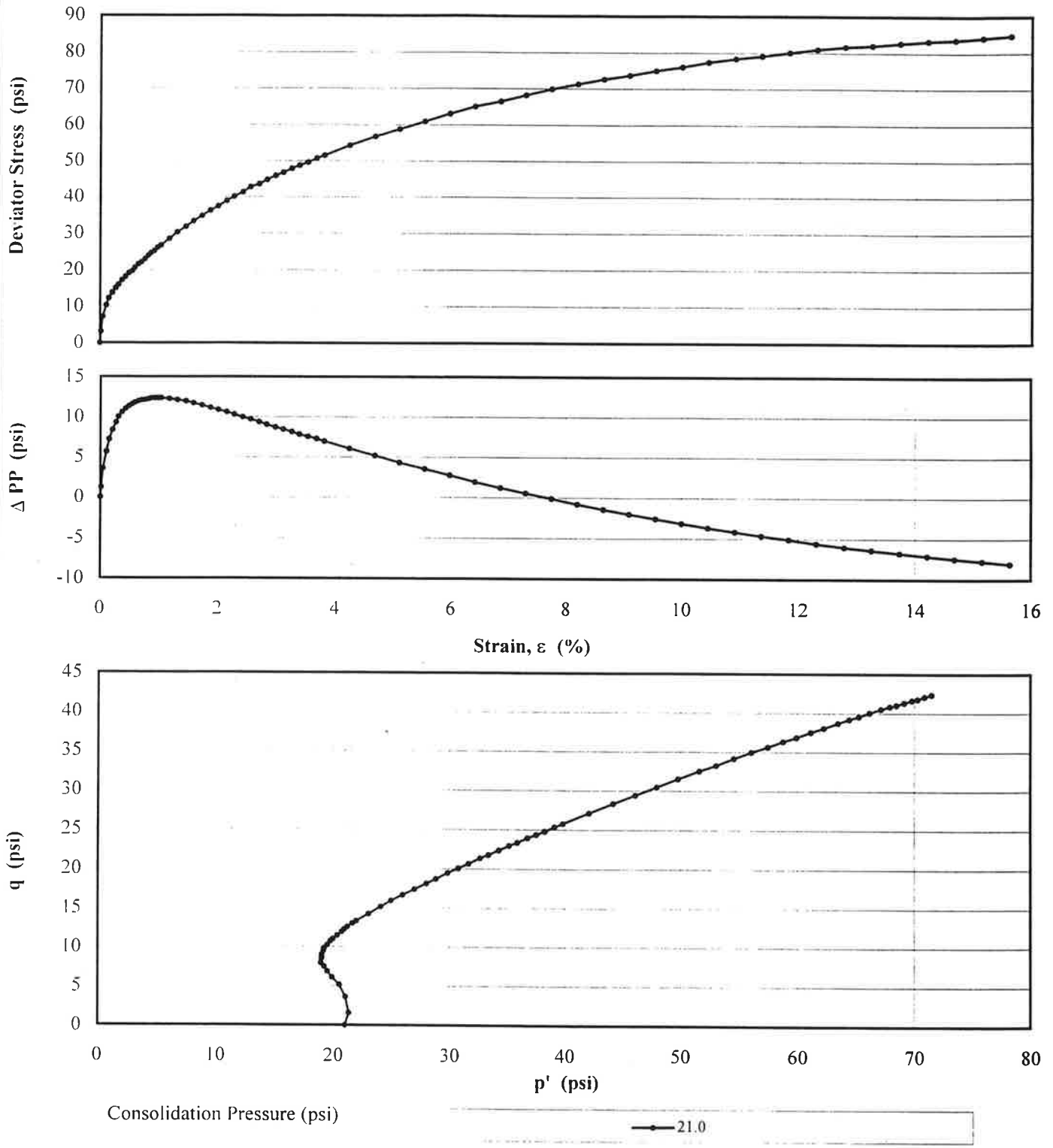
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 9



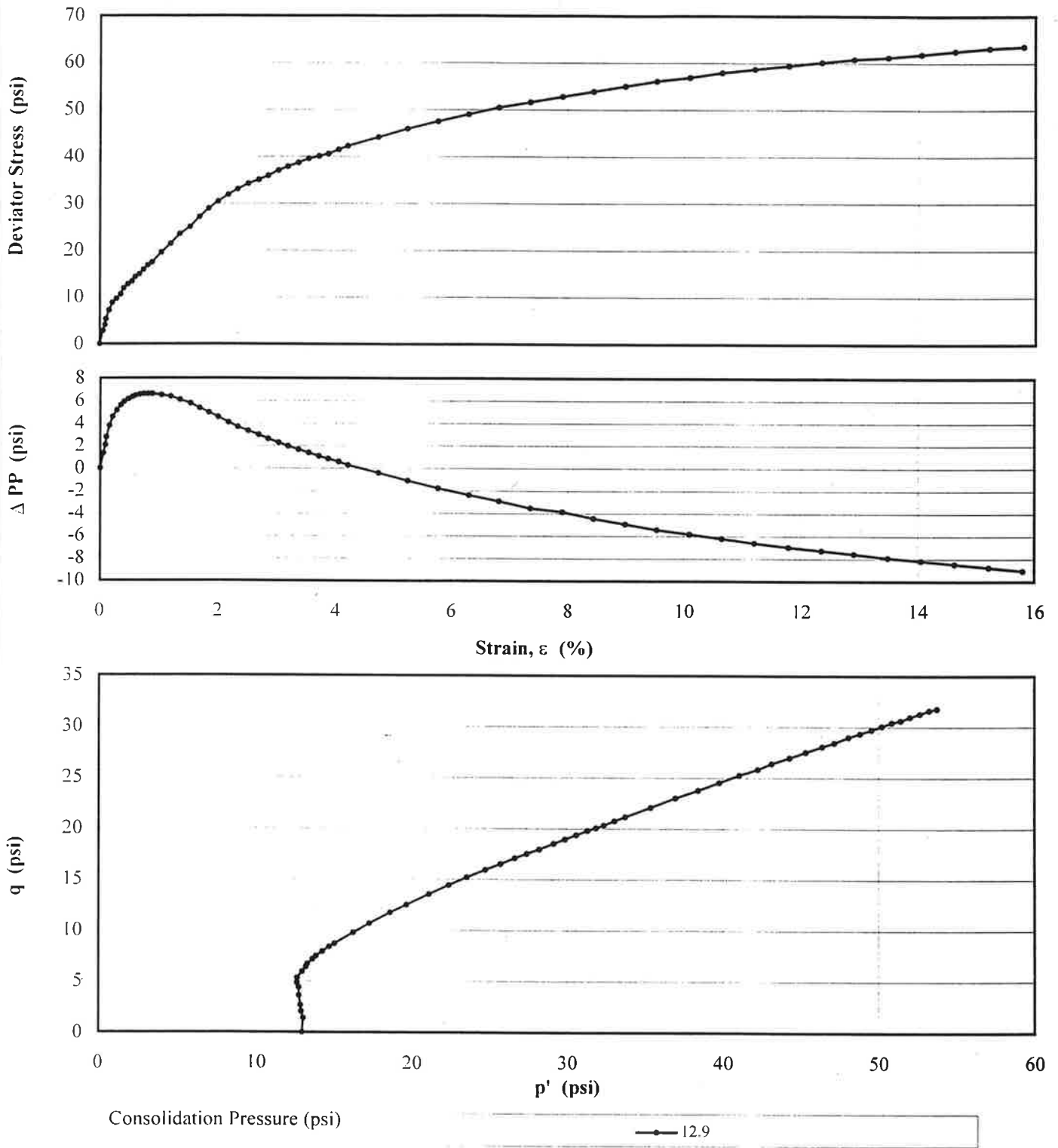
Note:



ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 10



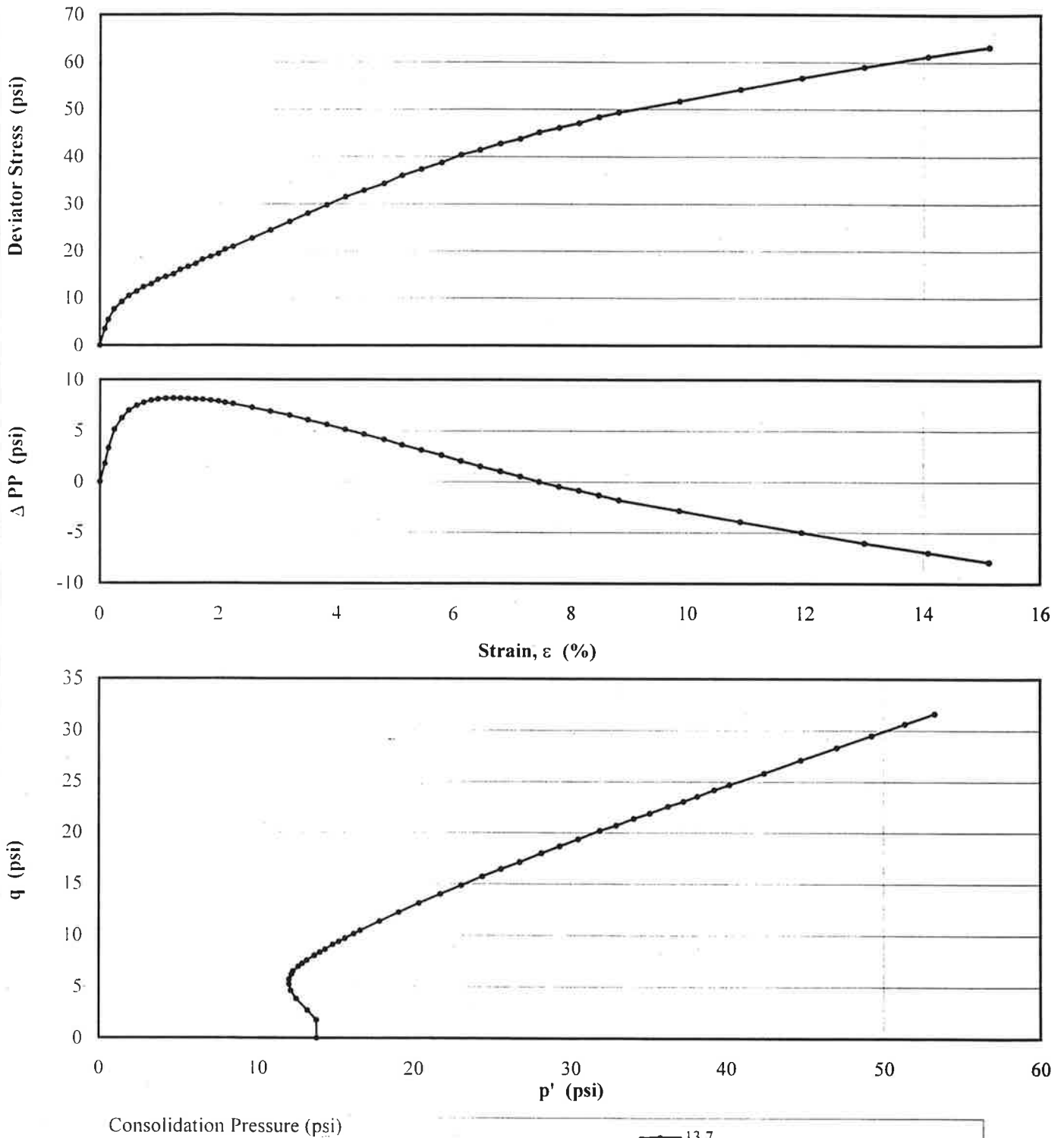
Note:



ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 11



Note:

TABLE 11

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) ⁽¹⁾

Site Sample ID	Lab Sample No.	Specimen Initial Conditions				σ_c (psi)	Peak				Ultimate				Figure No.	Remarks			
		Height (in.)	Diameter (in.)	Moisture Content (%)	Dry Unit Weight (pcf)		u_i (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)	u (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)			u (psi)		
G-3 (D) (15-17)	98J141.1	6.14	2.84	22.5	107.4	51.1	13.7											11	

Notes:

- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)

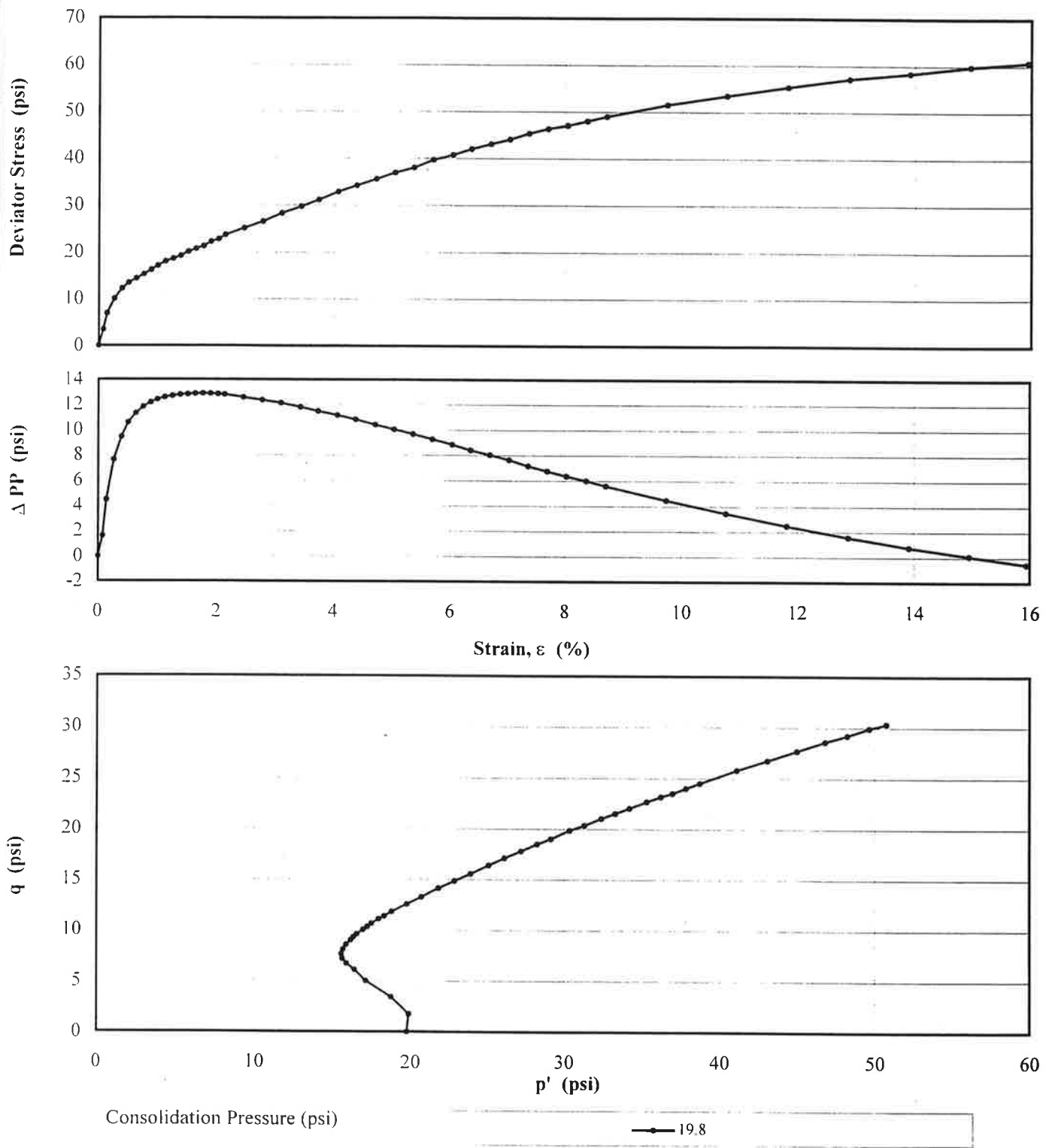
1.



ASTM D 4767

TRIAxIAL COMPRESSION TESTING

Figure 12



Note:



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Laboratory

Sample ID: G-2 (B) (18'-20')

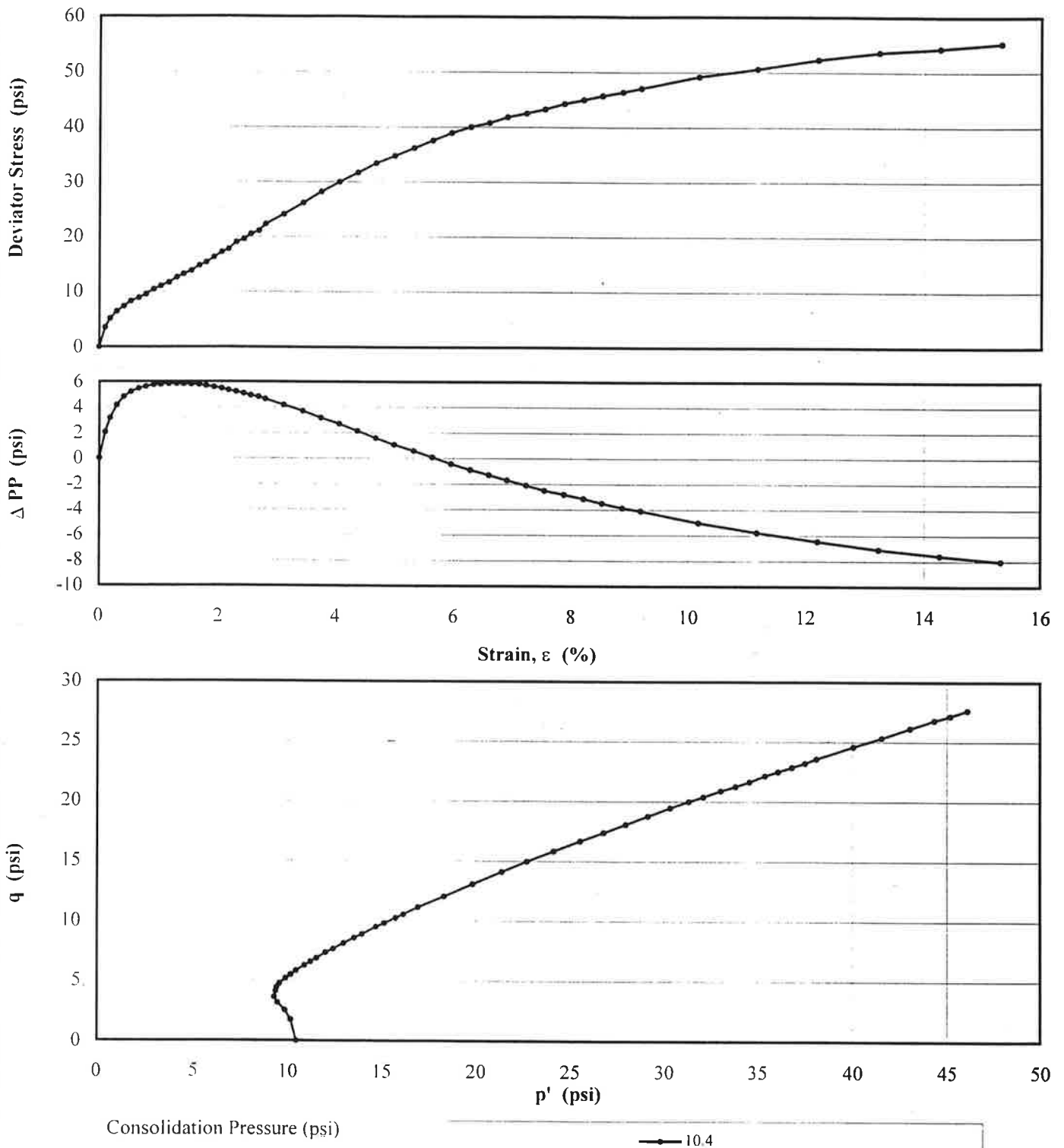
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 13



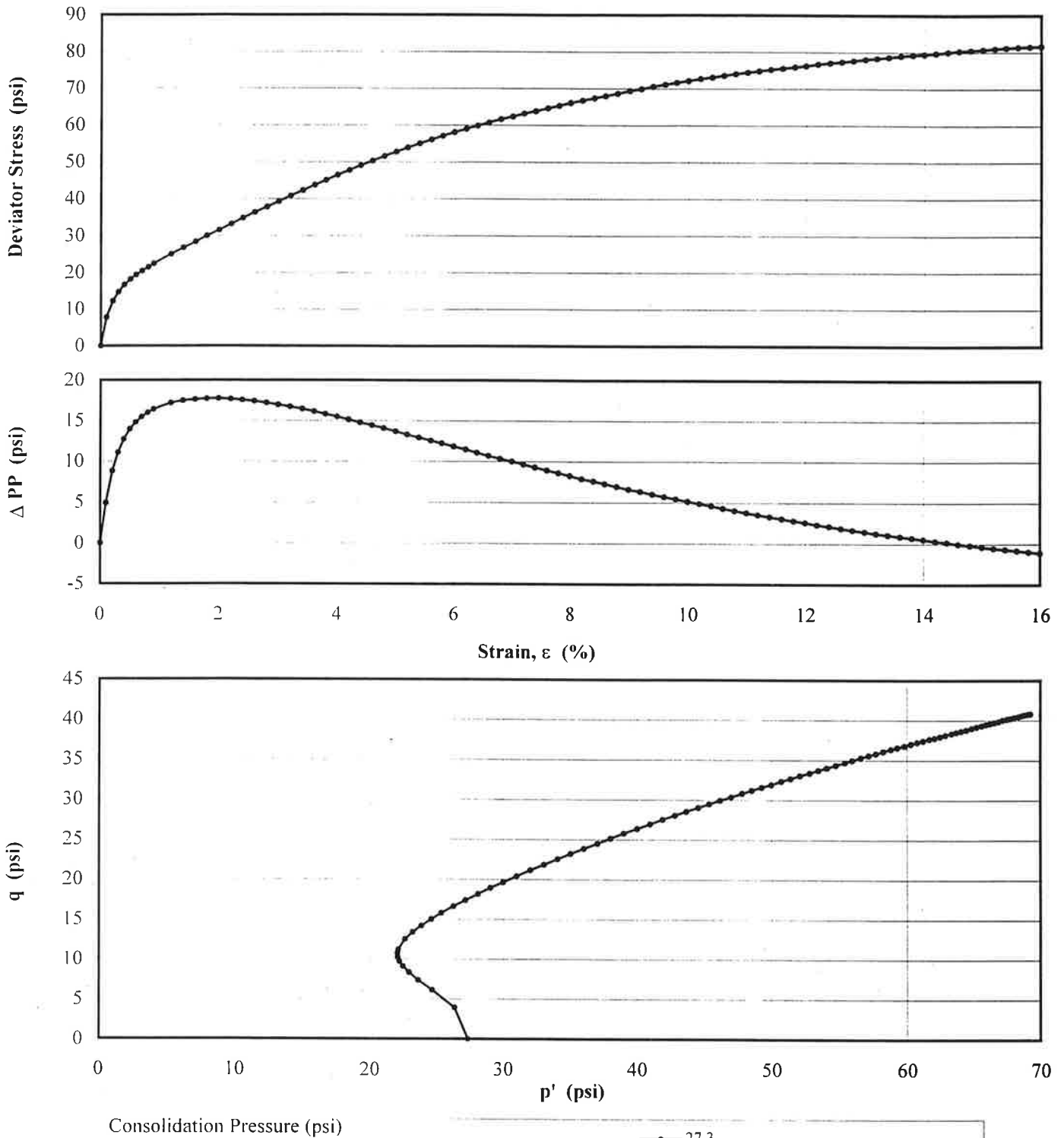
Note:



ASTM D 4767

TRIAxIAL COMPRESSION TESTING

Figure 14



Note:



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Sample ID: G-2 (H) (58'-60')

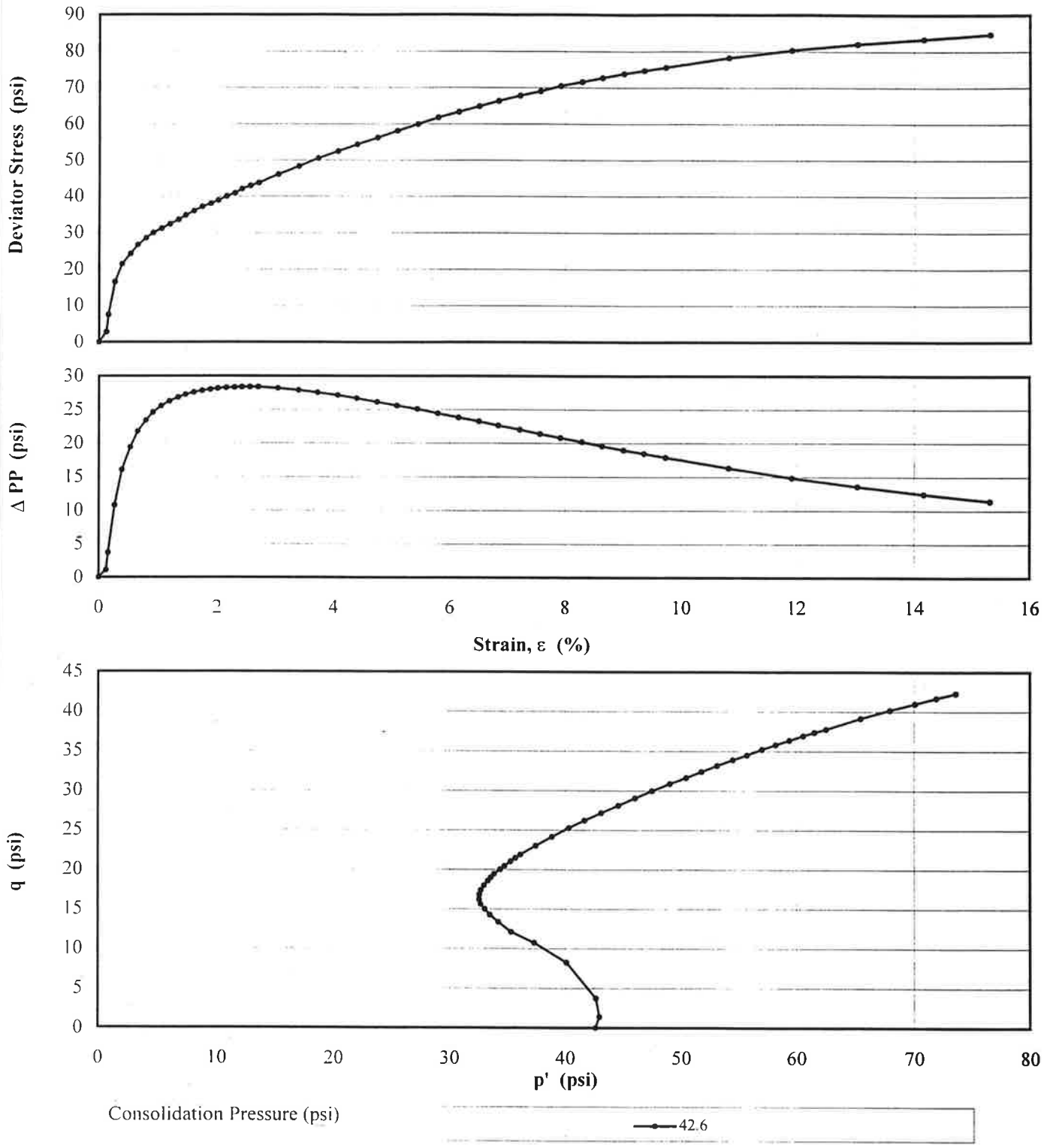
Project Name: LAKE PETIT DAM

Project No.: GL0625

ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 15



Note:

TABLE 15

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) ⁽¹⁾

Site Sample ID	Lab Sample No.	Specimen Initial Conditions			u_i	σ'_c	Peak				Ultimate				Figure No.	Remarks	
		Height (in.)	Diameter (in.)	Moisture Content (%)			Dry Unit Weight (pcf)	$\sigma'_1 - \sigma'_3$	σ'_1	ϵ_a	u	$\sigma'_1 - \sigma'_3$	σ'_1	ϵ_a			u
G-2 (II) (58'-60')	98J159.1	5.67	2.87	21.6	106.0	50.5	42.6	(psi)	(psi)	(psi)	(%)	(psi)	(psi)	(%)	(psi)	15	

Notes:

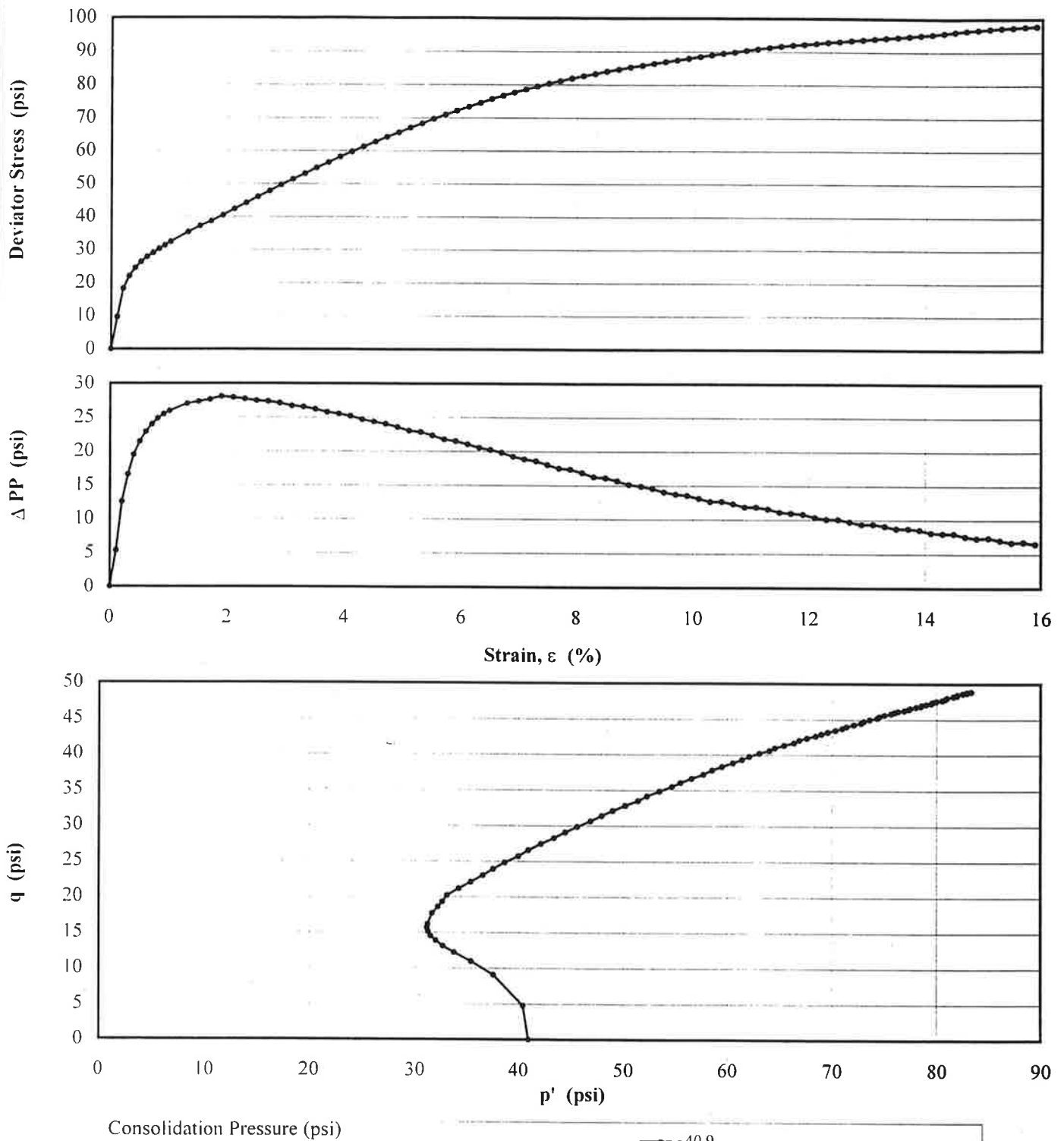
- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)



ASTM D 4767

TRIAXIAL COMPRESSION TESTING

Figure 16



Note:



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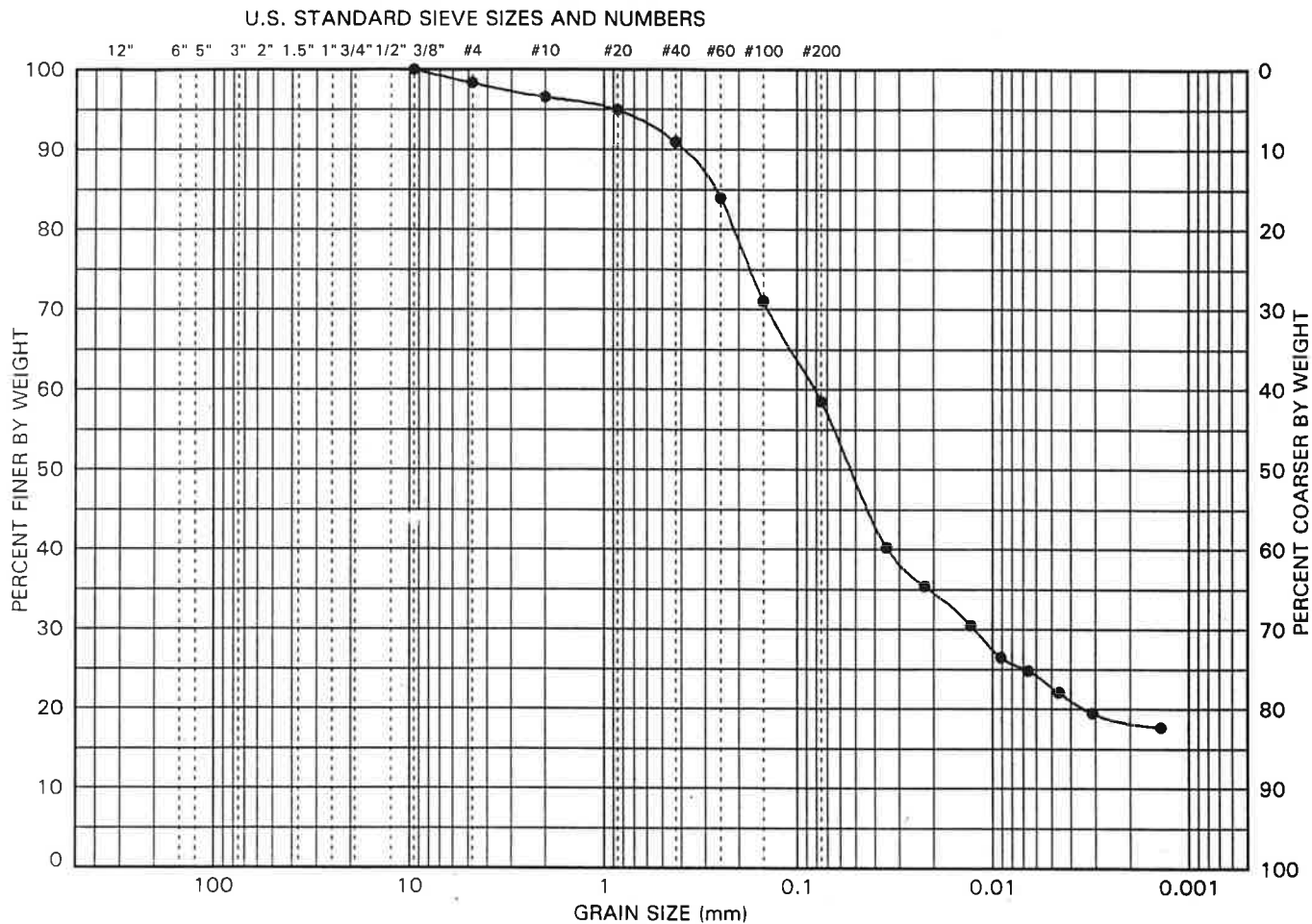
FIGURE

PROJECT: Lake Petit Dam
PROJECT NO.: GLO625
DOCUMENT NO.:

GS FORM:
4PS2 10/26/98

PARTICLE SIZE DISTRIBUTION AND PHYSICAL PROPERTIES

ASTM C 136, D 422, D 2487
D 3042 AND D 4318



BOULDERS	COBBLES	COARSE	FINE	COARSE	MEDIUM	FINE	SILT	CLAY
		GRAVEL		SAND				

SITE SAMPLE ID *		LIQUID LIMIT (%)		45		SOIL FRACTIONS	GRAVEL (%)		1.7									
LAB. SAMPLE NO. 98J162		PLASTIC LIMIT (%)		30			SAND (%)		39.8									
SAMPLE DEPTH (ft)		PLASTICITY INDEX		15			FINES (%)		58.5									
SOIL CLASSIFICATION: ML - Sandy Silt							SILT (%)		40.0									
						CLAY (%)		18.5										
						COEFF. UNIFORMITY (Cu)												
						COEFF. CURVATURE (Cc)												
PERCENT PASSING U.S. STANDARD SIEVE SIZES AND NUMBERS														PERCENT FINER THAN HYDROMETER PARTICLE DIAMETER (mm)				
3"	2"	1.5"	1"	3/4"	1/2"	3/8"	#4	#10	#20	#40	#60	#100	#200	0.050	0.020	0.005	0.002	0.001
PERCENT PASSING SIEVE SIZES (mm)																		
75	50	37.5	25	19	12.5	9.5	4.75	2.00	0.850	0.425	0.250	0.150	0.075	49	34	23	19	
100	100	100	100	100	100	100	98	97	95	91	84	71	59					

NOTES: * G-5(P) (60-62)

TABLE 16

CONSOLIDATED UNDRAINED (ICU) TRIAXIAL COMPRESSION TESTS

SUMMARY OF TEST RESULTS (ASTM D 4767) ⁽¹⁾

Site Sample ID	Lab Sample No.	Specimen Initial Conditions				u_i (psi)	σ'_c (psi)	Peak				Ultimate				Figure No.	Remarks	
		Height (in.)	Diameter (in.)	Moisture Content (%)	Dry Unit Weight (pcf)			$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_v (%)	u (psi)	$\sigma'_1 - \sigma'_3$ (psi)	σ'_1 (psi)	ϵ_a (%)	u (psi)			
G-5 (P) (60'-62')	98J162.1	6.10	2.85	22.0	104.8	50.0	40.9										16	

Notes:

- u_i = Initial pore pressure, (psi)
- u = Pore pressure, (psi)
- σ'_c = Consolidation pressure, (psi)
- σ'_1 = Effective axial stress, (psi)
- σ'_3 = Effective radial stress (confining pressure), (psi)
- ϵ_a = Axial strain, (%)

1.

APPENDIX D

SLEEPAGE ANALYSIS INPUT FILE

```

FILEINFO
SEEPW 4.20
TITLE
Lake Petit Dam
Seepage Analysis Cross Section (DGP 22 Oct
1998)
11/4/98
2:01:10 PM
ANALYSIS
1 1 +6.2400e+001 1 0
CONVERGE
50 +1.0000e+000 +1.0000e+000
+1.1000e+000 +1.0000e-004
TIME 0 +0.0000e+000 +1.0000e+000
+0.0000e+000 +1.0000e+000 1 1 1
MATERIAL 6
1 6 0 +1.0000e-001 +0.0000e+000
2 3 0 +1.0000e+000 +0.0000e+000
3 3 0 +1.0000e-001 +0.0000e+000
4 4 0 +1.0000e+000 +0.0000e+000
5 5 0 +1.0000e+000 +0.0000e+000
6 6 0 +1.0000e+000 +0.0000e+000
KFUNCTION 7
1 13 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
Shell Material
-2.0000e+003 +2.4800e-012
-1.0000e+003 +1.1800e-011
-6.0000e+002 +3.6600e-011
-2.0000e+002 +3.5700e-010
-1.0000e+002 +1.2500e-009
-5.0000e+001 +3.5800e-009
-2.0000e+001 +1.0200e-008
-1.0000e+001 +1.8300e-008
-5.0000e+000 +2.8600e-008
-1.0000e+000 +5.7800e-008
-1.0000e-001 +1.0400e-007
+0.0000e+000 +3.2800e-007
+2.0000e+005 +3.3000e-007
2 2 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
Soil below ballfield
-2.0000e+003 +1.6000e-006
+2.0000e+004 +1.6000e-006
3 13 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
Core Material
-2.0000e+003 +1.2400e-011
-1.0000e+003 +5.9400e-011
-6.0000e+002 +1.8300e-010
-2.0000e+002 +1.7900e-009
-1.0000e+002 +6.2700e-009
-5.0000e+001 +1.7900e-008
-2.0000e+001 +5.1300e-008
-1.0000e+001 +9.1700e-008
-5.0000e+000 +1.4300e-007
-1.0000e+000 +2.8900e-007
-1.0000e-001 +5.2000e-007
+0.0000e+000 +1.6400e-006
+2.0000e+004 +1.6500e-006
4 2 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
Saprolite
-2.0000e+003 +3.3000e-009
+2.0000e+004 +3.3000e-009
5 2 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
Bedrock
-2.0000e+003 +3.3000e-009
+2.0000e+004 +3.3000e-009

```

```

. 6 12 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
SM 1x10-4
-2.0000e+003 +2.0700e-010
-1.0000e+003 +1.7500e-009
-6.0000e+002 +7.8400e-009
-2.0000e+002 +1.1900e-007
-5.0000e+001 +8.2300e-007
-2.0000e+001 +1.4800e-006
-1.0000e+001 +1.9100e-006
-5.0000e+000 +2.2600e-006
-1.0000e+000 +2.7900e-006
-1.0000e-001 +3.1100e-006
+0.0000e+000 +3.2800e-006
+2.0000e+004 +3.3000e-006
7 12 +0.0000e+000 +1.5300e+000 13
-2.0000e+003 +4.0000e+002 0
SP Ks=1x10-3 cm/s
-2.0000e+003 +2.5400e-017
-1.0000e+003 +1.9000e-015
-2.0000e+002 +4.2200e-011
-1.0000e+002 +3.0200e-009
-5.0000e+001 +1.7300e-007
-2.0000e+001 +7.4900e-006
-1.0000e+001 +2.1200e-005
-5.0000e+000 +2.8900e-005
-1.0000e+000 +3.2500e-005
-1.0000e-001 +3.2800e-005
+0.0000e+000 +3.2800e-005
+2.0000e+004 +3.2800e-005
SFUNCTION 0
BFUNCTION 0
MFUNCTION 0
NODE 844
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+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
2 +0.0000e+000 +1.5200e+003
+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
3 +0.0000e+000 +1.5250e+003
+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
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+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
5 +0.0000e+000 +1.5300e+003
+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
6 +3.3000e+001 +1.5110e+003
+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
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+0.0000e+000 +0.0000e+000 000000
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+0.0000e+000
9 +3.3000e+001 +1.5270e+003
+0.0000e+000 +0.0000e+000 000000
+0.0000e+000
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+0.0000e+000 +0.0000e+000 000000
+0.0000e+000
11 +6.0000e+001 +1.5090e+003
+0.0000e+000 +0.0000e+000 200000
+0.0000e+000
12 +6.0000e+001 +1.5175e+003
+0.0000e+000 +0.0000e+000 000000
+0.0000e+000

```

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 +0.0000e+000 +0.0000e+000 200000
 +0.0000e+000
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0	0	2	4	+1.0000e+000	0	0						
	16	25	20	19	24	0	0					
0	0	2	4	+1.0000e+000	0	0						
	17	22	21	26	27	0	0					
0	0	5	4	+1.0000e+000	0	0						
	18	23	22	27	28	0	0					
0	0	6	4	+1.0000e+000	0	0						
	19	24	23	28	29	0	0					
0	0	2	4	+1.0000e+000	0	0						
	20	24	29	30	0	0	0					
0	0	2	3	+1.0000e+000	0	0						
	21	25	24	30	0	0	0					
0	0	2	3	+1.0000e+000	0	0						
	22	25	30	31	0	0	0					
0	0	2	3	+1.0000e+000	0	0						
	23	27	26	32	33	0	0					
0	0	5	4	+1.0000e+000	0	0						
	24	28	27	33	34	0	0					
0	0	6	4	+1.0000e+000	0	0						
	25	35	29	28	34	0	0					
0	0	2	4	+1.0000e+000	0	0						
	26	36	30	29	35	0	0					
0	0	2	4	+1.0000e+000	0	0						
	27	37	31	30	36	0	0					
0	0	2	4	+1.0000e+000	0	0						
	28	33	32	38	39	0	0					
0	0	5	4	+1.0000e+000	0	0						
	29	34	33	39	40	0	0					
0	0	6	4	+1.0000e+000	0	0						

0	65	83	77	76	82	0	0	100	108	118	119	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0	0
0	66	77	83	84	0	0	0	101	109	108	119	0	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	67	84	78	77	0	0	0	102	109	119	120	0	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	68	85	78	84	0	0	0	103	109	120	121	0	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	69	85	86	79	78	0	0	104	110	109	121	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	70	79	86	87	0	0	0	105	110	121	122	0	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	71	81	80	88	89	0	0	106	110	122	123	0	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	72	85	91	92	86	0	0	107	110	123	111	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	73	82	81	89	93	0	0	108	111	123	124	0	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	0	1	3	+1.0000e+000	0	0
0	74	83	82	93	90	0	0	109	113	112	125	126	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	5	4	+1.0000e+000	0	0
0	75	84	83	90	94	0	0	110	114	113	126	127	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	6	4	+1.0000e+000	0	0
0	76	85	84	94	91	0	0	111	115	114	127	128	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	77	86	92	95	87	0	0	112	116	115	128	129	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	78	89	88	96	97	0	0	113	117	116	129	130	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	79	91	99	100	92	0	0	114	118	117	130	131	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	80	93	89	97	101	0	0	115	119	118	131	132	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	81	90	93	101	98	0	0	116	120	119	132	133	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	82	92	100	102	95	0	0	117	121	120	133	134	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	83	94	90	98	103	0	0	118	122	121	134	135	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	84	91	94	103	99	0	0	119	123	122	135	136	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	85	97	96	104	105	0	0	120	124	123	136	137	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	86	101	97	105	106	0	0	121	127	126	138	139	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	0	6	4	+1.0000e+000	0	0
0	87	98	101	106	107	0	0	122	126	125	140	141	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	5	4	+1.0000e+000	0	0
0	88	103	98	107	108	0	0	123	128	127	139	142	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	89	99	103	108	109	0	0	124	129	128	142	144	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	90	99	109	110	100	0	0	125	130	129	144	145	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	91	100	110	111	102	0	0	126	131	130	145	146	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	92	105	104	112	113	0	0	127	132	131	146	147	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	93	106	105	113	114	0	0	128	133	132	147	148	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	94	106	114	115	0	0	0	129	134	133	148	149	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	95	106	115	107	0	0	0	130	135	134	149	150	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	96	107	115	116	0	0	0	131	136	135	150	151	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	97	107	116	117	0	0	0	132	137	136	151	152	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	1	4	+1.0000e+000	0	0
0	98	107	117	108	0	0	0	133	141	140	153	154	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	5	4	+1.0000e+000	0	0
0	99	108	117	118	0	0	0	134	139	138	154	156	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	0	6	4	+1.0000e+000	0	0

135	143	139	156	155	0	0	170	181	180	193	194	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	6	4	+1.0000e+000	0	0
136	144	143	155	157	0	0	171	182	181	194	195	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
137	145	144	157	158	0	0	172	183	182	195	196	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
138	146	145	158	159	0	0	173	188	183	196	197	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
139	147	146	159	160	0	0	174	184	188	197	198	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
140	148	147	160	161	0	0	175	185	184	198	199	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
141	149	148	161	162	0	0	176	186	185	199	200	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
142	150	149	162	163	0	0	177	187	186	200	201	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
143	151	150	163	164	0	0	178	189	187	201	202	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
144	152	151	164	165	0	0	179	189	202	203	190	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
145	154	153	166	167	0	0	180	190	203	204	191	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
146	156	154	167	168	0	0	181	193	192	205	206	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
147	155	156	168	169	0	0	182	194	193	206	207	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	6	4	+1.0000e+000	0	0
148	157	155	169	170	0	0	183	195	194	207	208	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
149	158	157	170	171	0	0	184	196	195	208	209	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
150	159	158	171	172	0	0	185	197	196	209	210	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
151	160	159	172	173	0	0	186	198	197	210	211	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
152	161	160	173	174	0	0	187	199	198	211	212	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
153	162	161	174	175	0	0	188	200	199	212	213	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
154	163	162	175	176	0	0	189	201	200	213	214	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
155	164	163	176	177	0	0	190	202	201	214	215	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
156	165	164	177	178	0	0	191	202	215	216	203	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
157	167	166	179	180	0	0	192	203	216	217	204	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
158	168	167	180	181	0	0	193	206	205	218	219	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
159	169	168	181	182	0	0	194	207	206	219	220	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	6	4	+1.0000e+000	0	0
160	170	169	182	183	0	0	195	208	207	220	221	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
161	173	172	184	185	0	0	196	209	208	221	222	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
162	174	173	185	186	0	0	197	211	223	224	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
163	175	174	186	187	0	0	198	211	224	217	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
164	171	170	183	188	0	0	199	212	224	225	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
165	172	171	188	184	0	0	200	213	212	225	226	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
166	176	175	187	189	0	0	201	214	213	226	227	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
167	176	189	190	177	0	0	202	210	209	222	228	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
168	177	190	191	178	0	0	203	210	228	223	211	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
169	180	179	192	193	0	0	204	215	214	227	229	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0

0	205	0	215	1	229	4	230	216	0	0	0	240	0	272	1	253	4	252	271	0	0
0	206	0	216	1	230	4	231	217	0	0	0	241	0	273	1	254	4	253	272	0	0
0	207	0	219	5	218	4	232	233	0	0	0	242	0	274	1	255	4	254	273	0	0
0	208	0	220	6	219	4	233	234	0	0	0	243	0	255	1	274	4	275	0	0	0
0	209	0	221	1	220	4	234	235	0	0	0	244	0	256	1	255	3	275	0	0	0
0	210	0	222	1	221	4	235	236	0	0	0	245	0	256	1	275	3	276	0	0	0
0	211	0	224	1	223	4	237	239	0	0	0	246	0	256	1	276	3	277	0	0	0
0	212	0	227	1	226	4	238	240	0	0	0	247	0	257	1	256	3	277	0	0	0
0	213	0	225	1	224	4	239	241	0	0	0	248	0	257	1	277	3	278	0	0	0
0	214	0	226	1	225	4	241	238	0	0	0	249	0	257	1	278	3	279	0	0	0
0	215	0	228	1	222	4	236	242	0	0	0	250	0	257	1	279	3	258	0	0	0
0	216	0	223	1	228	4	242	237	0	0	0	251	0	258	1	279	3	280	0	0	0
0	217	0	229	1	227	4	240	243	0	0	0	252	0	258	1	280	3	281	0	0	0
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0	219	0	230	1	244	4	245	231	0	0	0	254	0	259	1	281	3	282	0	0	0
0	220	0	233	5	232	4	246	247	0	0	0	255	0	261	1	260	4	265	266	0	0
0	221	0	234	6	233	4	247	248	0	0	0	256	0	262	6	261	4	266	267	0	0
0	222	0	235	1	234	4	248	249	0	0	0	257	0	268	1	263	4	262	267	0	0
0	223	0	236	1	235	4	249	250	0	0	0	258	0	269	1	264	4	263	268	0	0
0	224	0	242	1	236	4	250	251	0	0	0	259	0	270	1	264	4	269	0	0	0
0	225	0	237	1	242	4	251	252	0	0	0	260	0	278	1	277	4	284	283	0	0
0	226	0	239	1	237	4	252	253	0	0	0	261	0	279	1	278	4	283	285	0	0
0	227	0	238	1	241	4	254	255	0	0	0	262	0	277	1	276	4	286	284	0	0
0	228	0	240	1	238	4	255	256	0	0	0	263	0	280	1	279	4	285	287	0	0
0	229	0	241	1	239	4	253	254	0	0	0	264	0	281	1	280	4	287	288	0	0
0	230	0	243	1	240	4	256	257	0	0	0	265	0	276	1	275	4	289	286	0	0
0	231	0	243	1	257	4	258	244	0	0	0	266	0	266	5	265	4	290	291	0	0
0	232	0	244	1	258	4	259	245	0	0	0	267	0	267	6	266	4	291	292	0	0
0	233	0	247	5	246	4	260	261	0	0	0	268	0	268	1	267	4	292	293	0	0
0	234	0	248	6	247	4	261	262	0	0	0	269	0	269	1	268	4	293	294	0	0
0	235	0	249	1	248	4	262	263	0	0	0	270	0	270	1	269	4	294	295	0	0
0	236	0	250	1	249	4	263	264	0	0	0	271	0	271	1	270	4	295	296	0	0
0	237	0	251	1	250	3	264	0	0	0	0	272	0	272	1	271	4	296	297	0	0
0	238	0	270	1	251	3	264	0	0	0	0	273	0	273	1	272	4	297	298	0	0
0	239	0	271	1	252	3	251	270	0	0	0	274	0	274	1	273	4	298	299	0	0
0	0	0	0	1	0	4	0	0	0	0	0	0	0	0	1	0	4	0	0	0	0

275	275	274	299	289	0	0	310	318	317	335	336	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
276	282	281	288	300	0	0	311	320	319	337	338	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
277	285	283	301	302	0	0	312	319	321	339	337	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
278	283	284	303	301	0	0	313	322	320	338	340	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
279	287	285	302	304	0	0	314	321	323	341	339	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
280	284	286	305	303	0	0	315	324	322	340	342	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
281	288	287	304	306	0	0	316	323	325	343	341	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
282	286	289	307	305	0	0	317	326	324	342	344	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
283	300	288	306	308	0	0	318	325	336	354	343	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
284	289	299	318	307	0	0	319	328	327	345	346	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
285	291	290	309	310	0	0	320	329	328	346	347	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	6	4	+1.0000e+000	0	0
286	292	291	310	311	0	0	321	330	329	347	348	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
287	293	292	311	312	0	0	322	331	330	348	349	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
288	294	293	312	313	0	0	323	332	331	349	350	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
289	295	294	313	314	0	0	324	333	332	350	351	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
290	296	295	314	315	0	0	325	334	333	351	352	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
291	297	296	315	316	0	0	326	335	334	352	353	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
292	298	297	316	317	0	0	327	336	335	353	354	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
293	299	298	317	318	0	0	328	347	355	348	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
294	302	301	319	320	0	0	329	338	337	356	357	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
295	301	303	321	319	0	0	330	337	339	358	356	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
296	304	302	320	322	0	0	331	340	338	357	359	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
297	303	305	323	321	0	0	332	339	341	360	358	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
298	306	304	322	324	0	0	333	342	340	359	361	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
299	305	307	325	323	0	0	334	341	343	362	360	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
300	308	306	324	326	0	0	335	344	342	361	372	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
301	307	318	336	325	0	0	336	343	354	371	362	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
302	310	309	327	328	0	0	337	346	345	363	364	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
303	311	310	328	329	0	0	338	347	346	364	365	0	0
0	0	6	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
304	312	311	329	330	0	0	339	347	365	355	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	3	+1.0000e+000	0	0
305	313	312	330	331	0	0	340	349	348	355	366	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
306	314	313	331	332	0	0	341	350	349	366	367	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
307	315	314	332	333	0	0	342	351	350	367	368	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
308	316	315	333	334	0	0	343	352	351	368	369	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
309	317	316	334	335	0	0	344	353	352	369	370	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0

0	345	0	354	1	353	4	370	371	0	0	0	0	380	0	392	1	391	4	403	405	0	0
0	346	0	367	1	366	3	+1.0000e+000	0	0	0	0	0	381	0	385	4	383	4	421	423	0	0
0	347	0	365	3	389	3	+1.0000e+000	0	0	0	0	0	382	0	422	3	390	4	387	409	0	0
0	348	0	357	1	356	4	+1.0000e+000	0	0	0	0	0	383	0	402	1	407	4	406	400	0	0
0	349	0	356	1	358	4	+1.0000e+000	0	0	0	0	0	384	0	392	1	405	4	408	393	0	0
0	350	0	359	1	357	4	+1.0000e+000	0	0	0	0	0	385	0	389	3	385	4	423	424	0	0
0	351	0	380	1	358	4	+1.0000e+000	0	0	0	0	0	386	0	394	1	395	4	411	410	0	0
0	352	0	361	1	359	4	+1.0000e+000	0	0	0	0	0	387	0	413	1	398	4	393	408	0	0
0	353	0	378	1	360	4	+1.0000e+000	0	0	0	0	0	388	0	402	1	394	4	410	412	0	0
0	354	0	362	1	371	4	+1.0000e+000	0	0	0	0	0	389	0	395	1	396	4	414	411	0	0
0	355	0	364	5	363	4	+1.0000e+000	0	0	0	0	0	390	0	396	1	397	4	415	414	0	0
0	356	0	371	1	370	4	+1.0000e+000	0	0	0	0	0	391	0	397	1	399	4	416	415	0	0
0	357	0	365	4	364	4	+1.0000e+000	0	0	0	0	0	392	0	416	1	399	4	398	413	0	0
0	358	0	370	1	369	4	+1.0000e+000	0	0	0	0	0	393	0	401	3	389	4	424	436	0	0
0	359	0	372	1	361	4	+1.0000e+000	0	0	0	0	0	394	0	405	1	403	3	417	0	0	0
0	360	0	368	1	367	4	+1.0000e+000	0	0	0	0	0	395	0	429	3	403	4	390	422	0	0
0	361	0	369	1	368	4	+1.0000e+000	0	0	0	0	0	396	0	405	1	417	3	408	0	0	0
0	362	0	366	3	355	4	+1.0000e+000	0	0	0	0	0	397	0	407	1	419	4	418	406	0	0
0	363	0	365	3	385	3	+1.0000e+000	0	0	0	0	0	398	0	404	3	401	4	436	438	0	0
0	364	0	373	3	366	4	+1.0000e+000	0	0	0	0	0	399	0	417	1	426	3	408	0	0	0
0	365	0	393	1	377	4	+1.0000e+000	0	0	0	0	0	400	0	412	1	410	4	427	425	0	0
0	366	0	375	1	374	4	+1.0000e+000	0	0	0	0	0	401	0	430	1	413	4	408	426	0	0
0	367	0	376	1	375	4	+1.0000e+000	0	0	0	0	0	402	0	410	1	411	4	428	427	0	0
0	368	0	379	1	376	4	+1.0000e+000	0	0	0	0	0	403	0	411	1	414	4	432	428	0	0
0	369	0	392	1	381	4	+1.0000e+000	0	0	0	0	0	404	0	414	1	415	4	433	432	0	0
0	370	0	398	1	378	4	+1.0000e+000	0	0	0	0	0	405	0	437	3	417	4	403	429	0	0
0	371	0	391	1	384	4	+1.0000e+000	0	0	0	0	0	406	0	434	1	416	4	413	430	0	0
0	372	0	374	1	380	4	+1.0000e+000	0	0	0	0	0	407	0	415	1	416	4	434	433	0	0
0	373	0	386	1	387	3	+1.0000e+000	0	0	0	0	0	408	0	409	3	404	4	438	441	0	0
0	374	0	399	1	380	4	+1.0000e+000	0	0	0	0	0	409	0	419	1	435	4	431	418	0	0
0	375	0	388	1	379	4	+1.0000e+000	0	0	0	0	0	410	0	448	3	422	4	409	441	0	0
0	376	0	402	1	400	3	+1.0000e+000	0	0	0	0	0	411	0	445	3	426	4	417	437	0	0
0	377	0	387	3	373	4	+1.0000e+000	0	0	0	0	0	412	0	439	1	430	3	426	0	0	0
0	378	0	391	1	390	3	+1.0000e+000	0	0	0	0	0	413	0	435	1	442	4	440	431	0	0
0	379	0	383	5	382	4	+1.0000e+000	0	0	0	0	0	414	0	425	1	427	4	443	442	0	0
0													0		0	1		4	+1.0000e+000		0	0

0	415	0	450	3	429	4	422	448	0	0	0	450	0	477	3	463	4	462	476	0	0		
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0	417	0	428	1	4	4	+1.0000e+000	446	444	0	0	0	452	0	481	3	465	4	+1.0000e+000	455	480	0	0
0	418	0	432	1	4	4	+1.0000e+000	447	446	0	0	0	453	0	468	3	465	4	+1.0000e+000	481	482	0	0
0	419	0	449	1	4	4	+1.0000e+000	430	439	0	0	0	454	0	483	3	469	4	+1.0000e+000	470	484	0	0
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0	421	0	421	5	4	4	+1.0000e+000	459	460	0	0	0	456	0	476	1	468	4	+1.0000e+000	482	488	0	0
0	422	0	423	4	4	4	+1.0000e+000	421	461	0	0	0	457	0	472	3	485	4	+1.0000e+000	484	470	0	0
0	423	0	439	3	4	4	+1.0000e+000	445	451	0	0	0	458	0	472	1	473	4	+1.0000e+000	487	485	0	0
0	424	0	424	3	4	4	+1.0000e+000	423	464	0	0	0	459	0	474	1	491	4	+1.0000e+000	487	473	0	0
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0	426	0	436	3	4	4	+1.0000e+000	424	464	466	0	0	461	0	460	3	459	4	+1.0000e+000	492	493	0	0
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0	437	0	463	3	3	4	+1.0000e+000	449	462	0	0	0	472	0	501	3	480	4	+1.0000e+000	479	500	0	0
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0	440	0	451	3	4	4	+1.0000e+000	445	465	468	0	0	475	0	488	3	482	4	+1.0000e+000	503	504	0	0
0	441	0	479	3	4	4	+1.0000e+000	450	448	475	0	0	476	0	511	3	483	4	+1.0000e+000	484	510	0	0
0	442	0	470	1	4	4	+1.0000e+000	469	452	453	0	0	477	0	511	1	512	4	+1.0000e+000	486	483	0	0
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0	444	0	462	3	4	4	+1.0000e+000	451	468	476	0	0	479	0	485	1	487	4	+1.0000e+000	508	509	0	0
0	445	0	454	1	4	4	+1.0000e+000	456	473	472	0	0	480	0	491	1	508	3	+1.0000e+000	487	0	0	0
0	446	0	457	1	4	4	+1.0000e+000	474	473	456	0	0	481	0	505	1	489	4	+1.0000e+000	488	504	0	0
0	447	0	480	3	4	4	+1.0000e+000	455	450	479	0	0	482	0	506	3	490	4	+1.0000e+000	489	505	0	0
0	448	0	458	1	4	4	+1.0000e+000	478	474	457	0	0	483	0	507	3	491	4	+1.0000e+000	490	506	0	0
0	449	0	463	1	3	4	+1.0000e+000	478	458	0	0	0	484	0	508	3	491	4	+1.0000e+000	507	0	0	0
0	450	0	477	3	4	4	+1.0000e+000	463	462	476	0	0	0	0	3	3	463	4	+1.0000e+000	477	0	0	0

485	512	511	514	513	0	0	520	522	524	556	551	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
486	515	509	508	0	0	0	521	524	526	562	556	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
487	509	515	516	510	0	0	522	552	553	534	533	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
488	511	510	516	514	0	0	523	534	553	554	541	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
489	517	518	508	507	0	0	524	543	549	548	539	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
490	507	506	519	517	0	0	525	526	529	566	562	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
491	506	505	521	519	0	0	526	544	550	549	543	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
492	505	504	522	521	0	0	527	541	554	555	546	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
493	504	503	524	522	0	0	528	533	540	564	552	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
494	508	518	525	515	0	0	529	529	530	569	566	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
495	503	502	526	524	0	0	530	530	532	575	569	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
496	502	501	529	526	0	0	531	550	560	561	549	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
497	501	500	530	529	0	0	532	549	561	563	548	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
498	500	499	532	530	0	0	533	540	545	572	564	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
499	513	514	523	520	0	0	534	532	535	579	575	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
500	499	498	535	532	0	0	535	535	538	583	579	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
501	498	497	538	535	0	0	536	554	570	565	555	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
502	497	496	542	538	0	0	537	538	542	588	583	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
503	514	516	527	523	0	0	538	545	551	580	572	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
504	515	527	516	0	0	0	539	560	567	568	561	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
505	496	495	547	542	0	0	540	561	568	571	563	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
506	533	534	518	517	0	0	541	576	577	553	552	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
507	515	525	537	527	0	0	542	553	577	570	554	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
508	493	492	557	558	0	0	543	542	547	593	588	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
509	494	493	558	559	0	0	544	551	556	586	580	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
510	495	494	559	547	0	0	545	552	564	587	576	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
511	523	531	528	520	0	0	546	567	574	578	568	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
512	517	519	540	533	0	0	547	570	584	573	565	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
513	518	534	541	525	0	0	548	556	562	590	586	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
514	527	536	531	523	0	0	549	568	578	582	571	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
515	519	521	545	540	0	0	550	547	559	597	593	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
516	531	543	539	528	0	0	551	562	566	596	590	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
517	521	522	551	545	0	0	552	574	581	585	578	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
518	525	541	546	537	0	0	553	564	572	594	587	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
519	536	544	543	531	0	0	554	559	558	599	597	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0

555	577	592	584	570	0	0	590	603	608	629	624	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
556	558	557	602	599	0	0	591	606	609	631	632	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
557	578	585	589	582	0	0	592	608	611	635	629	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
558	591	592	577	576	0	0	593	610	618	634	623	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
559	584	595	581	573	0	0	594	612	616	636	627	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
560	566	569	598	596	0	0	595	609	613	637	631	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
561	572	580	600	594	0	0	596	605	617	642	630	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
562	569	575	603	598	0	0	597	611	615	640	635	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
563	576	587	601	591	0	0	598	614	623	638	626	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
564	575	579	608	603	0	0	599	616	619	641	636	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
565	580	586	607	600	0	0	600	618	622	639	634	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
566	592	605	595	584	0	0	601	613	621	644	637	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
567	579	583	611	608	0	0	602	615	620	645	640	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
568	585	581	613	609	0	0	603	619	624	646	641	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
569	589	585	609	606	0	0	604	622	627	643	639	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
570	587	594	610	601	0	0	605	617	626	649	642	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
571	604	605	592	591	0	0	606	623	634	647	638	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
572	586	590	612	607	0	0	607	620	625	648	645	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
573	583	588	615	611	0	0	608	621	630	654	644	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
574	581	595	621	613	0	0	609	624	629	651	646	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
575	590	596	616	612	0	0	610	627	636	650	643	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
576	591	601	614	604	0	0	611	625	628	655	648	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
577	588	593	620	615	0	0	612	632	631	653	0	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
578	594	600	618	610	0	0	613	629	635	656	651	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
579	596	598	619	616	0	0	614	634	639	652	647	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
580	593	597	625	620	0	0	615	626	638	660	649	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
581	605	604	617	0	0	0	616	628	633	659	655	0	0
0	0	3	3	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
582	600	607	622	618	0	0	617	631	637	658	653	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
583	601	610	623	614	0	0	618	636	641	657	650	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
584	598	603	624	619	0	0	619	630	642	663	654	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
585	595	605	630	621	0	0	620	635	640	662	656	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
586	597	599	628	625	0	0	621	639	643	661	652	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
587	604	614	626	617	0	0	622	637	644	665	658	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
588	599	602	633	628	0	0	623	641	646	664	657	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
589	607	612	627	622	0	0	624	638	647	668	660	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0

625	640	645	666	662	0	0	660	677	684	705	0	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
626	643	650	667	661	0	0	661	679	686	703	697	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
627	642	649	670	663	0	0	662	681	685	702	699	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
628	646	651	669	664	0	0	663	680	687	704	698	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
629	645	648	671	666	0	0	664	678	688	706	696	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
630	644	654	675	665	0	0	665	683	689	707	700	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
631	647	652	674	668	0	0	666	685	690	709	702	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	3	4	+1.0000e+000	0	0
632	651	656	672	669	0	0	667	687	691	708	704	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
633	650	657	673	667	0	0	668	686	692	710	703	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
634	648	655	676	671	0	0	669	688	694	711	706	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
635	649	660	678	670	0	0	670	689	696	713	707	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
636	658	677	653	0	0	0	671	690	695	712	709	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
637	652	661	679	674	0	0	672	691	699	714	708	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
638	656	662	681	672	0	0	673	692	698	715	710	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
639	655	659	682	676	0	0	674	694	697	716	711	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
640	654	663	683	675	0	0	675	684	693	724	705	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
641	657	664	680	673	0	0	676	695	701	720	712	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
642	658	665	684	677	0	0	677	699	702	717	714	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
643	661	667	686	679	0	0	678	698	704	718	715	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
644	660	668	688	678	0	0	679	697	703	719	716	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
645	662	666	685	681	0	0	680	696	706	721	713	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
646	664	669	687	680	0	0	681	693	700	727	724	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
647	663	670	689	683	0	0	682	702	709	722	717	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
648	666	671	690	685	0	0	683	704	708	723	718	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
649	665	675	693	684	0	0	684	703	710	725	719	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
650	667	673	692	686	0	0	685	706	711	726	721	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
651	669	672	691	687	0	0	686	732	727	700	707	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
652	668	674	694	688	0	0	687	709	712	728	722	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
653	671	676	695	690	0	0	688	708	714	729	723	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
654	670	678	696	689	0	0	689	710	715	730	725	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
655	672	681	699	691	0	0	690	711	716	731	726	0	0
0	0	3	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
656	673	680	698	692	0	0	691	737	732	707	713	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
657	674	679	697	694	0	0	692	714	717	733	729	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
658	675	683	700	693	0	0	693	715	718	734	730	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
659	676	682	701	695	0	0	694	716	719	735	731	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0

695	712	720	736	728	0	0	730	753	756	771	768	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
696	717	722	738	733	0	0	731	752	755	775	773	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
697	718	723	739	734	0	0	732	756	761	772	771	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
698	744	737	713	721	0	0	733	755	759	778	775	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
699	719	725	740	735	0	0	734	761	764	774	772	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
700	723	729	741	739	0	0	735	760	777	757	0	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
701	722	728	742	738	0	0	736	759	762	779	778	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
702	725	730	743	740	0	0	737	764	769	776	774	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
703	721	726	746	744	0	0	738	760	763	781	777	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
704	729	733	745	741	0	0	739	762	765	780	779	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
705	730	734	747	743	0	0	740	765	768	782	780	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
706	726	731	750	746	0	0	741	763	766	784	781	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
707	728	736	748	742	0	0	742	768	771	783	782	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
708	733	738	749	745	0	0	743	766	767	786	784	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
709	724	727	757	0	0	0	744	771	772	785	783	0	0
0	0	1	3	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
710	731	735	752	750	0	0	745	767	770	788	786	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
711	734	739	751	747	0	0	746	772	774	787	785	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
712	727	732	760	757	0	0	747	770	773	790	788	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
713	739	741	753	751	0	0	748	774	776	789	787	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
714	735	740	755	752	0	0	749	773	775	792	790	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
715	738	742	754	749	0	0	750	781	791	777	0	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	1	3	+1.0000e+000	0	0
716	732	737	763	760	0	0	751	775	778	793	792	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
717	740	743	759	755	0	0	752	778	779	794	793	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
718	741	745	756	753	0	0	753	779	780	795	794	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
719	742	748	758	754	0	0	754	780	782	796	795	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
720	737	744	766	763	0	0	755	782	783	797	796	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
721	743	747	762	759	0	0	756	783	785	798	797	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
722	745	749	761	756	0	0	757	781	784	800	791	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
723	744	746	767	766	0	0	758	785	787	799	798	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	4	4	+1.0000e+000	0	0
724	747	751	765	762	0	0	759	784	786	802	800	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
725	749	754	764	761	0	0	760	787	789	801	799	0	0
0	0	4	4	+1.0000e+000	0	0	0	0	5	4	+1.0000e+000	0	0
726	746	750	770	767	0	0	761	786	788	803	802	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
727	751	753	768	765	0	0	762	788	790	804	803	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
728	754	758	769	764	0	0	763	790	792	805	804	0	0
0	0	5	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0
729	750	752	773	770	0	0	764	792	793	806	805	0	0
0	0	1	4	+1.0000e+000	0	0	0	0	1	4	+1.0000e+000	0	0

765	793	794	808	806	0	0	4	255	128	0
0	0	1	4	+1.0000e+000	0	0	5	128	255	255
766	794	795	809	808	0	0	6	128	128	64
0	0	1	4	+1.0000e+000	0	0				
767	795	796	810	809	0	0				
0	0	1	4	+1.0000e+000	0	0				
768	796	797	811	810	0	0				
0	0	1	4	+1.0000e+000	0	0				
769	800	802	807	0	0	0				
0	0	1	3	+1.0000e+000	0	0				
770	797	798	812	811	0	0				
0	0	1	4	+1.0000e+000	0	0				
771	798	799	814	812	0	0				
0	0	4	4	+1.0000e+000	0	0				
772	799	801	815	814	0	0				
0	0	5	4	+1.0000e+000	0	0				
773	802	803	813	807	0	0				
0	0	1	4	+1.0000e+000	0	0				
774	803	804	816	813	0	0				
0	0	1	4	+1.0000e+000	0	0				
775	804	805	817	816	0	0				
0	0	1	4	+1.0000e+000	0	0				
776	805	806	818	817	0	0				
0	0	1	4	+1.0000e+000	0	0				
777	806	808	819	818	0	0				
0	0	1	4	+1.0000e+000	0	0				
778	808	809	820	819	0	0				
0	0	1	4	+1.0000e+000	0	0				
779	809	810	822	820	0	0				
0	0	1	4	+1.0000e+000	0	0				
780	810	811	823	822	0	0				
0	0	1	4	+1.0000e+000	0	0				
781	811	812	824	823	0	0				
0	0	1	4	+1.0000e+000	0	0				
782	812	814	825	824	0	0				
0	0	4	4	+1.0000e+000	0	0				
783	816	817	821	0	0	0				
0	0	1	3	+1.0000e+000	0	0				
784	814	815	827	825	0	0				
0	0	5	4	+1.0000e+000	0	0				
785	817	818	826	821	0	0				
0	0	1	4	+1.0000e+000	0	0				
786	818	819	828	826	0	0				
0	0	1	4	+1.0000e+000	0	0				
787	819	820	829	828	0	0				
0	0	1	4	+1.0000e+000	0	0				
788	820	822	830	829	0	0				
0	0	1	4	+1.0000e+000	0	0				
789	822	823	831	830	0	0				
0	0	1	4	+1.0000e+000	0	0				
790	823	824	836	831	0	0				
0	0	1	4	+1.0000e+000	0	0				
791	824	825	834	836	0	0				
835	0	4	4	+1.0000e+000	0	0				
792	825	827	832	834	0	0				
833	0	5	4	+1.0000e+000	0	0				
793	842	834	832	840	838	833				
837	841	5	4	+1.0000e+000	1	0				
794	844	836	834	842	839	835				
838	843	4	4	+1.0000e+000	1	0				
POLE										
+5.0000e+002 +1.5735e+003										
FLUX										
0										
DENSITY										
+1.0000e+000 +1.0000e+000										
WATERTABLE										
0										
qBOUNDARY										
0										
MATLCOLOR										
6										
1	255	255	128							
2	128	128	255							
3	128	255	128							

APPENDIX B

SLOPE STABILITY ANALYSIS OUTPUT
FILES

2082

LPURFMP 11-06-98 16:03

LAKE PETIT DAM

10 most critical surfaces, MINIMUM BISHOP FOS = 1.516

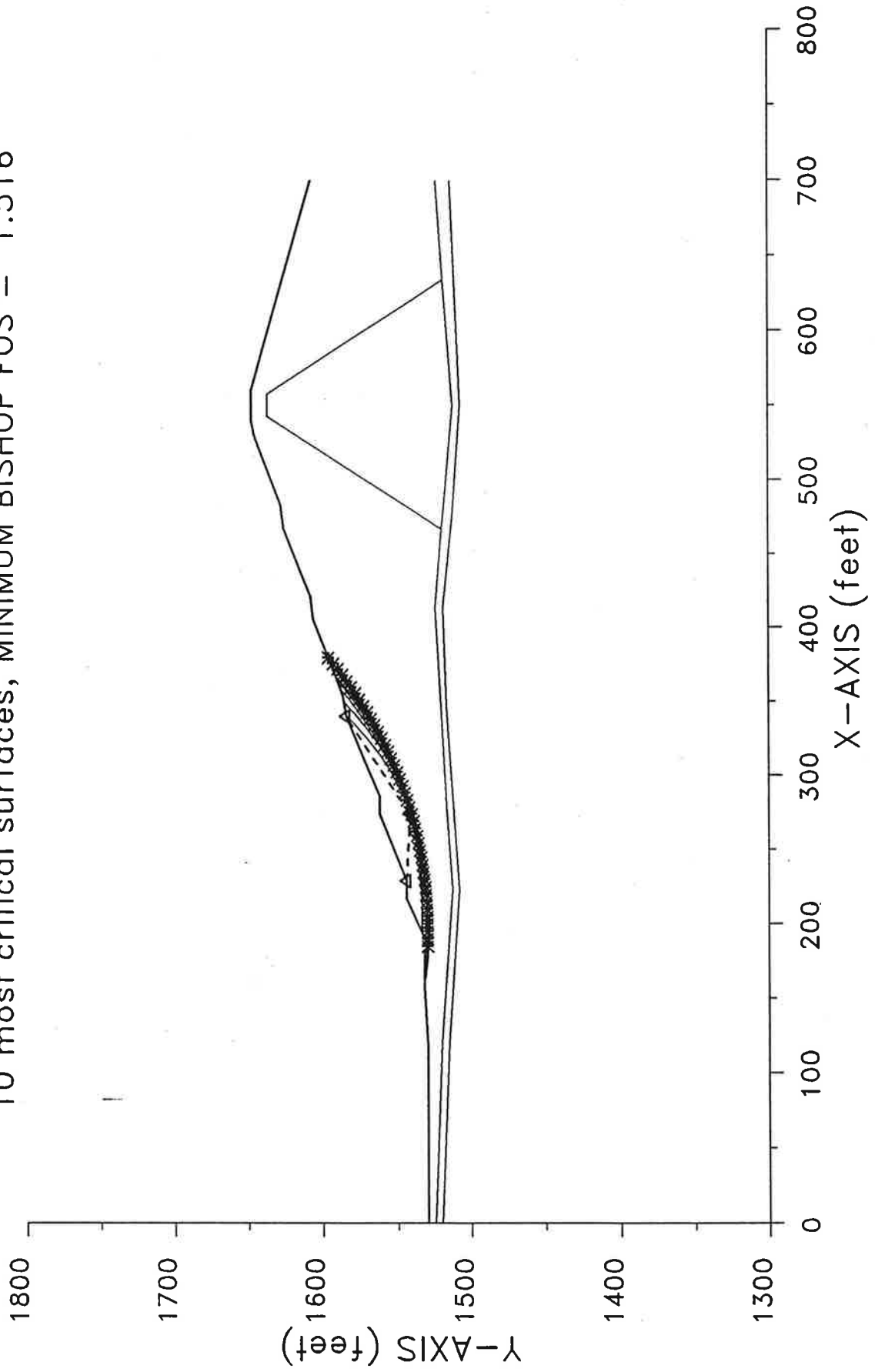


Table with 3 columns of numerical data. Values range from 147.0 to 402.0 in the first column, and 1520.5 to 1532.4 in the second column. The third column contains values ranging from 2003.3 to 2480.2.

Table with 3 columns of numerical data. Values range from 447.9 to 481.5 in the first column, and 1611.2 to 1595.4 in the second column. The third column contains values ranging from -286.5 to 624.7.

Table with 3 columns of numerical data. Values range from 402.0 to 447.9 in the first column, and 1542.2 to 1577.7 in the second column. The third column contains values ranging from 2044.7 to 1072.0.

Table with 3 columns of numerical data. Values range from 481.6 to 509.8 in the first column, and 1603.6 to 1595.5 in the second column. The third column contains values ranging from 113.1 to 839.5.

648.0	1623.0	748.8
648.8	1560.8	1907.4
649.4	1580.5	2853.2
650.0	1613.0	1226.0
653.0	1511.8	6763.6
653.1	1531.0	5500.9
653.3	1554.1	4299.6
653.8	1574.0	3216.3
655.7	1604.3	1673.9
657.3	1526.8	5882.1
657.8	1547.5	4691.5
658.2	1567.5	3585.4
659.3	1500.8	7477.8
661.5	1595.7	2127.0
661.5	1521.0	6242.6
661.8	1541.1	5074.9
662.6	1561.0	3960.0
666.7	1534.0	5506.5
667.0	1512.5	6795.2
667.0	1554.5	4340.2
667.2	1587.0	2595.0

BOUNDARIES THAT LIMIT SURFACE GENERATION HAVE BEEN SPECIFIED

UPPER limiting boundary of 2 segments:

Segment No.	x-left (ft)	y-left (ft)	x-right (ft)	y-right (ft)
1	229.0	1544.0	274.0	1542.0
2	274.0	1542.0	340.0	1584.0

A critical failure surface searching method, using a random technique for generating CIRCULAR surfaces has been specified.

600 trial surfaces will be generated and analyzed.

30 Surfaces initiate from each of 20 points equally spaced along the ground surface between x = 160.0 ft and x = 228.0 ft

Each surface terminates between x = 313.0 ft and x = 380.0 ft

Unless further limitations were imposed, the minimum elevation at which a surface extends is y = 1500.0 ft

5.0 ft line segments define each trial failure surface.

ANGULAR RESTRICTIONS

The first segment of each failure surface will be inclined within the angular range defined by :

Lower angular limit := -45.0 degrees

ycenter = 1735.15 Init. Pt. = 170.74 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 53 slices for surface # 117 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5998) is defined by: xcenter = 219.10 ycenter = 1734.04 Init. Pt. = 170.74 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 46 slices for surface # 133 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5863) is defined by: xcenter = 216.96 ycenter = 1694.00 Init. Pt. = 174.32 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 47 slices for surface # 139 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5972) is defined by: xcenter = 219.15 ycenter = 1695.22 Init. Pt. = 174.32 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 53 slices for surface # 149 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.6871) is defined by: xcenter = 231.61 ycenter = 1694.31 Init. Pt. = 174.32 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 47 slices for surface # 152 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7495) is defined by: xcenter = 231.71 ycenter = 1649.18 Init. Pt. = 177.89 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 55 slices for surface # 157 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7824) is defined by: xcenter = 242.87 ycenter = 1677.02 Init. Pt. = 177.89 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 53 slices for surface # 162 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7367) is defined by: xcenter = 236.94 ycenter = 1677.43 Init. Pt. = 177.89 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 55 slices for surface # 169 (shear strength for these slice(s) set to ZERO)

Upper angular limit := (slope angle - 5.0) degrees

***** WARNING -- WARNING -- WARNING -- WARNING -- (# 49) *****

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 54 slices for surface # 14 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5563) is defined by: xcenter = 201.50 ycenter = 1780.92 Init. Pt. = 160.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 52 slices for surface # 30 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5705) is defined by: xcenter = 204.29 ycenter = 1752.64 Init. Pt. = 160.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 51 slices for surface # 40 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5297) is defined by: xcenter = 198.72 ycenter = 1777.71 Init. Pt. = 163.58 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 53 slices for surface # 56 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5404) is defined by: xcenter = 198.79 ycenter = 1786.71 Init. Pt. = 163.58 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 48 slices for surface # 106 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5985) is defined by: xcenter = 217.19 ycenter = 1700.32 Init. Pt. = 170.74 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 48 slices for surface # 108 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5851) is defined by: xcenter = 215.80 ycenter = 1707.70 Init. Pt. = 170.74 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 47 slices for surface # 109 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5396) is defined by: xcenter = 207.60

Circular surface (FOS= 1.7302) is defined by: xcenter = 218.89 ycenter = 1689.71 Init. Pt. = 177.89 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 48 slices for surface # 171 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7198) is defined by: xcenter = 231.70 ycenter = 1661.60 Init. Pt. = 177.89 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 60 slices for surface # 181 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.1158) is defined by: xcenter = 254.22 ycenter = 1620.50 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 57 slices for surface # 185 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9705) is defined by: xcenter = 250.06 ycenter = 1645.90 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 56 slices for surface # 188 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 4.9827) is defined by: xcenter = 249.17 ycenter = 1617.37 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 65 slices for surface # 189 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.0138) is defined by: xcenter = 261.28 ycenter = 1623.53 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 2 slice(s) out of 62 slices for surface # 192 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 5.7906) is defined by: xcenter = 255.90 ycenter = 1628.02 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for 1 slice(s) out of 64 slices for surface # 193 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.8011) is defined by: xcenter = 260.05 ycenter = 1624.82 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 64 slices for surface # 198
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.1998) is defined by: xcenter = 260.27
ycenter = 1619.94 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 61 slices for surface # 199
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.4161) is defined by: xcenter = 254.98
ycenter = 1618.97 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
2 slice(s) out of 59 slices for surface # 206
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9980) is defined by: xcenter = 253.14
ycenter = 1647.42 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 61 slices for surface # 208
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.2215) is defined by: xcenter = 255.12
ycenter = 1621.37 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 59 slices for surface # 209
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.7326) is defined by: xcenter = 253.69
ycenter = 1612.94 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 56 slices for surface # 210
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.6762) is defined by: xcenter = 250.47
ycenter = 1607.04 Init. Pt. = 181.47 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 41 slices for surface # 212
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5214) is defined by: xcenter = 207.44
ycenter = 1716.80 Init. Pt. = 185.05 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 50 slices for surface # 221
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5163) is defined by: xcenter = 194.87

Circular surface (FOS= 6.5679) is defined by: xcenter = 260.53
ycenter = 1615.36 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 61 slices for surface # 248
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 6.8840) is defined by: xcenter = 264.05
ycenter = 1618.55 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 54 slices for surface # 249
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.0361) is defined by: xcenter = 253.51
ycenter = 1617.75 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 52 slices for surface # 250
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.8354) is defined by: xcenter = 248.86
ycenter = 1668.54 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 56 slices for surface # 251
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.0735) is defined by: xcenter = 256.73
ycenter = 1601.16 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 59 slices for surface # 252
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.3506) is defined by: xcenter = 261.50
ycenter = 1609.46 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 47 slices for surface # 253
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.8611) is defined by: xcenter = 243.81
ycenter = 1645.49 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 44 slices for surface # 254
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.0141) is defined by: xcenter = 244.39
ycenter = 1618.93 Init. Pt. = 188.63 Seg. Length = 5.00

ycenter = 1821.54 Init. Pt. = 185.05 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 49 slices for surface # 238
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.6003) is defined by: xcenter = 222.39
ycenter = 1732.13 Init. Pt. = 185.05 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 49 slices for surface # 241
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.6381) is defined by: xcenter = 229.76
ycenter = 1722.47 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 59 slices for surface # 242
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 8.1603) is defined by: xcenter = 261.15
ycenter = 1600.66 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 44 slices for surface # 243
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7989) is defined by: xcenter = 239.70
ycenter = 1652.08 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 61 slices for surface # 244
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.8157) is defined by: xcenter = 264.45
ycenter = 1608.21 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 42 slices for surface # 245
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7499) is defined by: xcenter = 234.02
ycenter = 1650.12 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 57 slices for surface # 246
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 4.1958) is defined by: xcenter = 257.28
ycenter = 1627.63 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 59 slices for surface # 247
(shear strength for these slice(s) set to ZERO)

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 56 slices for surface # 255
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 5.0254) is defined by: xcenter = 256.95
ycenter = 1620.89 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 51 slices for surface # 256
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7837) is defined by: xcenter = 245.34
ycenter = 1678.61 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 58 slices for surface # 257
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 4.9455) is defined by: xcenter = 259.41
ycenter = 1628.50 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 46 slices for surface # 258
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.5354) is defined by: xcenter = 207.00
ycenter = 1773.62 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 52 slices for surface # 259
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9191) is defined by: xcenter = 252.85
ycenter = 1655.41 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 45 slices for surface # 260
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9858) is defined by: xcenter = 245.94
ycenter = 1625.42 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 55 slices for surface # 261
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 7.9742) is defined by: xcenter = 257.35
ycenter = 1596.86 Init. Pt. = 188.63 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
1 slice(s) out of 51 slices for surface # 262
(shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9215) is defined by: xcenter = 250.66

Circular surface (FOS= 2.3869) is defined by: xcenter = 278.42
 ycenter = 1600.80 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 36 slices for surface # 593
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.6311) is defined by: xcenter = 277.43
 ycenter = 1589.95 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 39 slices for surface # 594
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7030) is defined by: xcenter = 265.99
 ycenter = 1675.56 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 40 slices for surface # 595
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.8368) is defined by: xcenter = 274.33
 ycenter = 1654.06 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 37 slices for surface # 596
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.9130) is defined by: xcenter = 272.34
 ycenter = 1632.10 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 31 slices for surface # 597
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 1.7673) is defined by: xcenter = 262.59
 ycenter = 1630.67 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 43 slices for surface # 598
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.4057) is defined by: xcenter = 286.25
 ycenter = 1611.02 Init. Pt. = 228.00 Seg. Length = 5.00

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 39 slices for surface # 599
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.4709) is defined by: xcenter = 281.20
 ycenter = 1600.67 Init. Pt. = 228.00 Seg. Length = 5.00

**** Simplified BISHOP FOS = 1.516 ****

The following is a summary of the TEN most critical surfaces

Problem Description : LAKE PETIT DAM

	FOS (BISHOP)	Circle x-coord (ft)	Center y-coord (ft)	Radius (ft)	Initial x-coord (ft)	Terminal x-coord (ft)	Resisting Moment (ft-lb)
1.	1.516	194.87	1821.54	291.69	185.05	379.77	4.376E+07
2.	1.521	207.44	1716.80	188.12	185.05	340.80	2.173E+07
3.	1.530	198.72	1777.71	248.21	163.58	358.29	3.252E+07
4.	1.535	207.00	1773.62	242.86	188.63	367.18	3.444E+07
5.	1.540	207.60	1735.15	206.47	170.74	349.69	2.756E+07
6.	1.540	198.79	1786.71	257.13	163.58	364.42	3.568E+07
7.	1.540	206.69	1793.42	262.59	188.63	379.65	4.153E+07
8.	1.556	201.50	1780.92	252.36	160.00	367.96	3.914E+07
9.	1.557	213.58	1779.46	245.53	195.79	374.16	3.336E+07
10.	1.564	215.73	1779.77	246.01	195.79	378.76	3.595E+07

*** END OF FILE ***

ERROR #49: NEGATIVE effective stress calculated for
 1 slice(s) out of 44 slices for surface # 600
 (shear strength for these slice(s) set to ZERO)

Circular surface (FOS= 2.3035) is defined by: xcenter = 286.98
 ycenter = 1619.24 Init. Pt. = 228.00 Seg. Length = 5.00

Factors of safety have been calculated by the :

***** SIMPLIFIED BISHOP METHOD *****

The most critical circular failure surface
 is specified by 44 coordinate points

Point No.	x-surf (ft)	y-surf (ft)
1	185.05	1530.02
2	190.05	1529.90
3	195.05	1529.86
4	200.05	1529.90
5	205.05	1530.01
6	210.04	1530.25
7	215.04	1530.55
8	220.02	1530.94
9	225.00	1531.42
10	229.97	1531.97
11	234.92	1532.62
12	239.87	1533.35
13	244.80	1534.16
14	249.72	1535.06
15	254.63	1536.04
16	259.51	1537.11
17	264.38	1538.26
18	269.22	1539.49
19	274.05	1540.80
20	278.85	1542.20
21	283.62	1543.68
22	288.37	1545.24
23	293.10	1546.88
24	297.79	1548.61
25	302.45	1550.41
26	307.08	1552.29
27	311.68	1554.26
28	316.25	1556.30
29	320.78	1558.42
30	325.27	1560.61
31	329.72	1562.88
32	334.14	1565.23
33	338.51	1567.66
34	342.84	1570.15
35	347.13	1572.73
36	351.37	1575.37
37	355.57	1578.09
38	359.72	1580.88
39	363.82	1583.74
40	367.87	1586.67
41	371.87	1589.67
42	375.82	1592.73
43	379.72	1595.87
44	379.77	1595.91

LAKE PETIT DAM
10 most critical surfaces, MINIMUM BISHOP FOS = 1.464

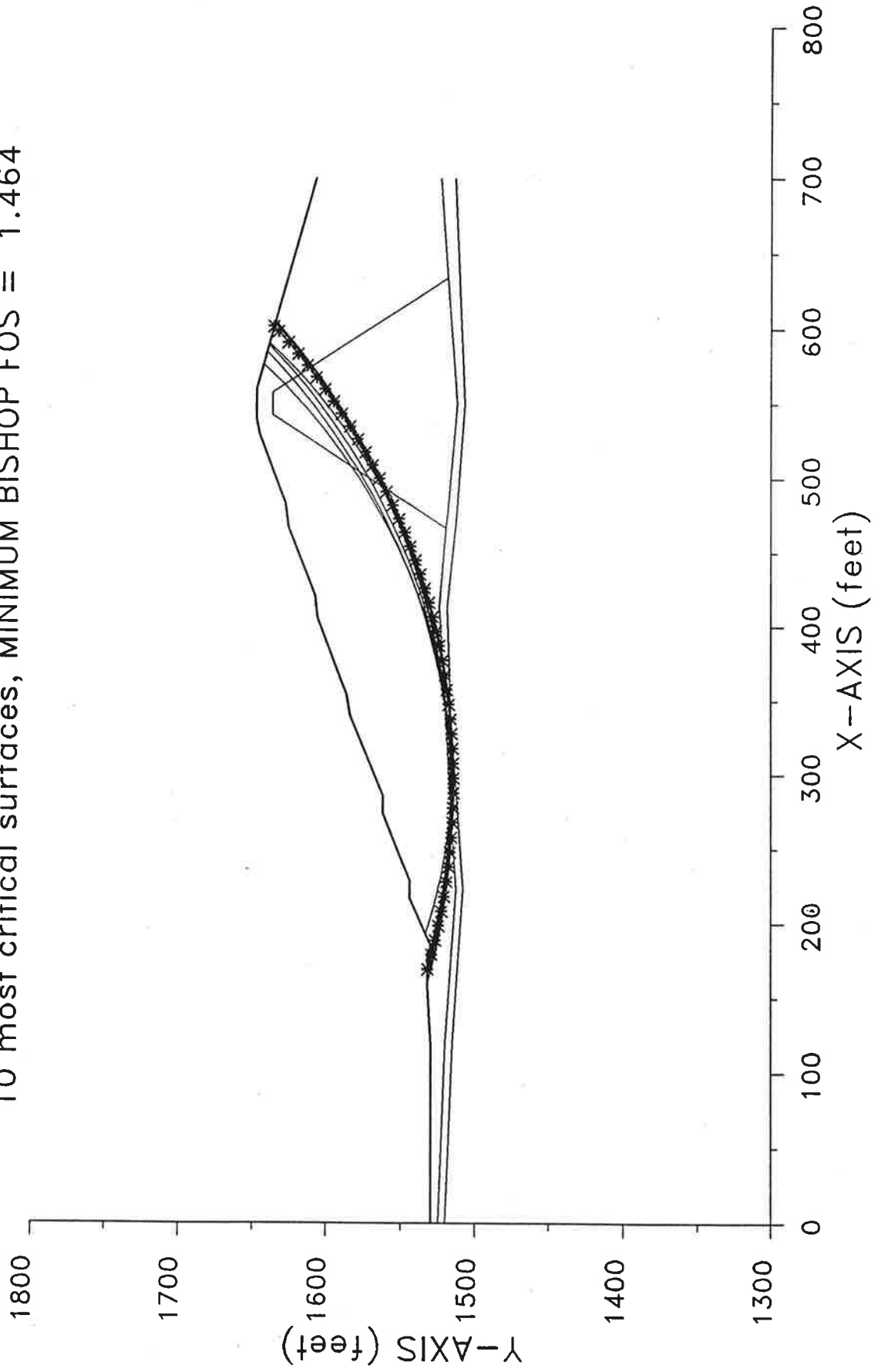


Table with 3 columns of numerical data, ranging from 334.0 to 391.0 on the left and 1610.0 to 1953.1 on the right.

Table with 3 columns of numerical data, ranging from 439.0 to 474.8 on the left and 1528.3 to 1619.8 on the right.

Table with 3 columns of numerical data, ranging from 391.0 to 439.0 on the left and 1730.2 to 3428.9 on the right.

Table with 3 columns of numerical data, ranging from 474.9 to 502.7 on the left and 1573.9 to 1595.5 on the right.

635.5	1580.5	2788.5
639.0	1511.0	6723.3
639.0	1595.7	2026.8
639.5	1532.0	5493.9
639.6	1553.8	4253.4
639.8	1574.0	1151.3
643.7	1525.9	5869.0
644.2	1547.0	4655.7
644.3	1567.4	3526.3
645.0	1500.0	7439.9
645.0	1587.0	2496.1
647.8	1520.0	6234.7
647.9	1540.8	5026.5
648.0	1623.0	748.8
648.8	1560.8	1907.4
649.4	1580.5	2853.2
650.0	1613.0	1226.0
653.0	1511.8	6763.6
653.1	1533.0	5500.9
653.3	1554.1	4299.6
653.8	1574.0	3216.3
655.7	1604.3	1673.9
657.3	1526.8	5882.1
657.8	1547.5	4691.5
658.2	1567.5	3585.4
659.3	1500.8	7477.8
661.5	1595.7	2127.0
661.5	1521.0	6242.6
661.8	1541.1	5074.9
662.6	1561.0	3960.0
666.7	1534.0	5506.5
667.0	1512.5	6795.2
667.0	1554.5	4340.2
667.2	1587.0	2595.0

A horizontal earthquake loading coefficient of .183 has been assigned

A vertical earthquake loading coefficient of .000 has been assigned

A critical failure surface searching method, using a random technique for generating CIRCULAR surfaces has been specified.

600 trial surfaces will be generated and analyzed.

30 Surfaces initiate from each of 20 points equally spaced along the ground surface between x = 160.0 ft and x = 250.5 ft

Each surface terminates between x = 506.5 ft and x = 605.5 ft

Unless further limitations were imposed, the minimum elevation at which a surface extends is y = 1500.0 ft

10.0 ft line segments define each trial failure surface.

36	508.77	1569.30
37	517.51	1574.17
38	526.13	1579.23
39	534.64	1584.49
40	543.03	1589.93
41	551.30	1595.55
42	559.44	1601.36
43	567.45	1607.34
44	575.33	1613.50
45	583.07	1619.84
46	590.66	1626.34
47	598.11	1633.01
48	601.46	1636.15

**** Simplified BISHOP FOS = 1.464 ****

The following is a summary of the TEN most critical surfaces

Problem Description : LAKE PETIT DAM

	FOS (BISHOP)	Circle x-coord (ft)	Center y-coord (ft)	Radius (ft)	Initial x-coord (ft)	Terminal x-coord (ft)	Resisting Moment (ft-lb)
1.	1.464	293.52	1965.63	451.01	169.53	601.46	7.730E+08
2.	1.469	292.58	1978.79	463.42	169.53	603.89	7.949E+08
3.	1.470	296.34	1972.54	457.13	174.29	604.84	7.875E+08
4.	1.483	284.50	2008.68	492.67	160.00	605.47	8.469E+08
5.	1.483	286.90	1996.57	480.36	164.76	603.66	8.195E+08
6.	1.486	309.15	1896.66	381.19	193.34	590.43	6.295E+08
7.	1.486	292.91	1987.56	470.75	174.29	605.05	8.039E+08
8.	1.488	279.03	1949.80	434.42	160.00	584.57	6.952E+08
9.	1.489	289.17	1943.08	426.83	174.29	589.12	6.928E+08
10.	1.493	287.21	1906.49	391.15	174.29	576.54	6.081E+08

*** END OF FILE ***

ANGULAR RESTRICTIONS

The first segment of each failure surface will be inclined within the angular range defined by :

Lower angular limit := -45.0 degrees
Upper angular limit := (slope angle - 5.0) degrees

***** WARNING -- WARNING -- WARNING -- WARNING -- (# 48) *****

USER SELECTED option to maintain strength greater than zero

Factors of safety have been calculated by the :

***** SIMPLIFIED BISHOP METHOD *****

The most critical circular failure surface is specified by 48 coordinate points

Point No.	x-surf (ft)	y-surf (ft)
1	169.53	1532.00
2	179.17	1529.36
3	188.87	1526.93
4	198.62	1524.72
5	208.42	1522.72
6	218.26	1520.94
7	228.14	1519.38
8	238.05	1518.04
9	247.99	1516.93
10	257.95	1516.03
11	267.92	1515.35
12	277.91	1514.89
13	287.91	1514.66
14	297.91	1514.64
15	307.91	1514.85
16	317.90	1515.28
17	327.88	1515.93
18	337.84	1516.80
19	347.78	1517.90
20	357.69	1519.21
21	367.58	1520.74
22	377.42	1522.49
23	387.23	1524.46
24	396.98	1526.65
25	406.69	1529.05
26	416.34	1531.67
27	425.93	1534.50
28	435.46	1537.54
29	444.92	1540.79
30	454.30	1544.25
31	463.60	1547.92
32	472.82	1551.79
33	481.95	1555.87
34	490.99	1560.15
35	499.93	1564.63

LAKE PETIT DAM

10 most critical surfaces, MINIMUM BISHOP FOS = 1.740

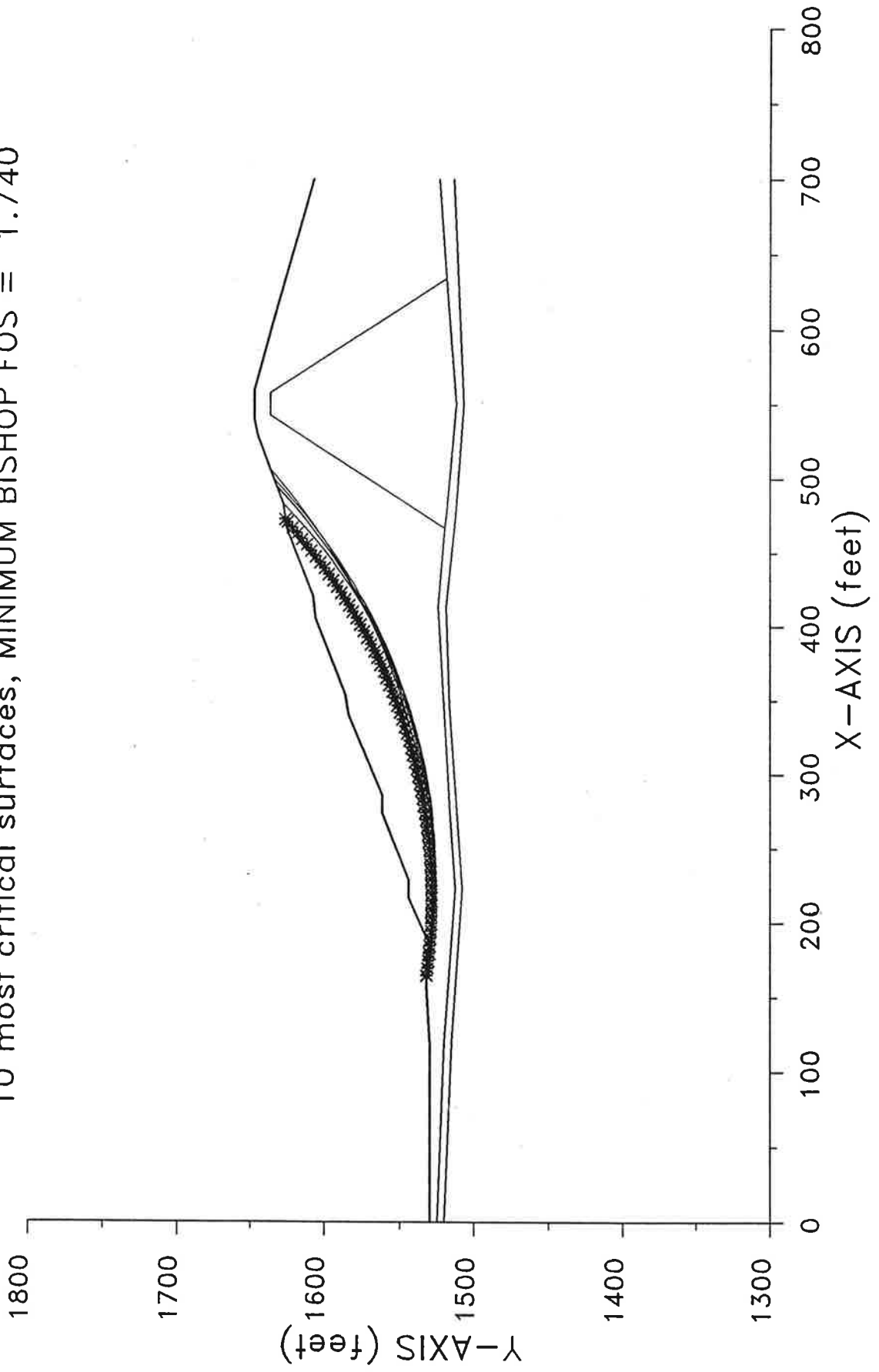


Table with 3 columns: ID, Value 1, Value 2. Contains numerical data for various IDs from 509.9 to 537.0.

Table with 3 columns: ID, Value 1, Value 2. Contains numerical data for various IDs from 558.6 to 594.4.

Table with 3 columns: ID, Value 1, Value 2. Contains numerical data for various IDs from 537.8 to 558.5.

Table with 3 columns: ID, Value 1, Value 2. Contains numerical data for various IDs from 594.5 to 647.9.

648.0	1621.0	748.8
648.8	1560.8	3892.8
649.4	1580.5	2843.2
650.0	1613.0	1224.0
653.0	1511.8	6743.1
653.1	1533.0	5482.1
653.3	1554.1	4284.1
653.8	1574.0	3205.1
655.7	1604.3	1670.2
657.3	1526.8	5863.0
657.8	1547.5	4675.3
658.2	1567.5	3573.0
659.3	1500.8	7458.0
661.5	1599.7	2122.6
661.5	1521.0	6223.5
661.8	1541.1	5058.0
662.6	1561.0	3946.7

A critical failure surface searching method, using a random technique for generating CIRCULAR surfaces has been specified.

600 trial surfaces will be generated and analyzed.

30 Surfaces initiate from each of 20 points equally spaced along the ground surface between x = 160.0 ft and x = 250.5 ft

Each surface terminates between x = 444.0 ft and x = 506.5 ft

Unless further limitations were imposed, the minimum elevation at which a surface extends is y = 1500.0 ft

5.0 ft line segments define each trial failure surface.

ANGULAR RESTRICTIONS

The first segment of each failure surface will be inclined within the angular range defined by :

Lower angular limit := -45.0 degrees
Upper angular limit := (slope angle - 5.0) degrees

Factors of safety have been calculated by the :

***** SIMPLIFIED BISHOP METHOD *****

The most critical circular failure surface is specified by 68 coordinate points

Point No.	x-surf (ft)	y-surf (ft)
-----------	-------------	-------------

**** Simplified BISHOP FOS = 1.740 ****

The following is a summary of the TEN most critical surfaces

Problem Description : LAKE PETIT DAM

	FOS (BISHOP)	Circle x-coord (ft)	Center y-coord (ft)	Radius (ft)	Initial x-coord (ft)	Terminal x-coord (ft)	Resisting Moment (ft-lb)
1.	1.740	215.77	1914.46	385.85	164.76	472.80	1.640E+08
2.	1.740	214.13	1918.63	389.77	164.76	472.15	1.623E+08
3.	1.744	218.36	1900.70	372.57	164.76	470.68	1.602E+08
4.	1.744	227.54	1868.18	341.15	169.53	467.90	1.536E+08
5.	1.746	218.89	1891.61	363.66	164.76	467.34	1.531E+08
6.	1.747	220.18	1961.21	432.77	164.76	506.50	2.299E+08
7.	1.751	224.50	1927.83	401.05	160.00	496.14	2.159E+08
8.	1.752	227.50	1914.04	387.96	160.00	494.36	2.134E+08
9.	1.752	214.06	1881.54	355.45	169.53	483.40	1.896E+08
10.	1.752	228.25	1919.30	393.27	160.00	499.70	2.229E+08

*** END OF FILE ***

1	164.76	1532.00
2	169.72	1531.37
3	174.69	1530.81
4	179.67	1530.31
5	184.65	1529.87
6	189.63	1529.50
7	194.62	1529.19
8	199.62	1528.95
9	204.62	1528.77
10	209.61	1528.66
11	214.61	1528.62
12	219.61	1528.63
13	224.61	1528.72
14	229.61	1528.86
15	234.61	1529.07
16	239.60	1529.35
17	244.59	1529.69
18	249.57	1530.10
19	254.55	1530.57
20	259.52	1531.10
21	264.48	1531.70
22	269.44	1532.37
23	274.39	1533.09
24	279.32	1533.89
25	284.25	1534.74
26	289.16	1535.66
27	294.07	1536.64
28	298.96	1537.69
29	303.83	1538.80
30	308.69	1539.97
31	313.54	1541.21
32	318.36	1542.51
33	323.18	1543.87
34	327.97	1545.29
35	332.74	1546.78
36	337.50	1548.32
37	342.23	1549.93
38	346.95	1551.60
39	351.64	1553.31
40	356.30	1555.12
41	360.95	1556.97
42	365.57	1558.89
43	370.16	1560.86
44	374.73	1562.89
45	379.28	1564.98
46	383.79	1567.13
47	388.28	1569.33
48	392.73	1571.60
49	397.16	1573.92
50	401.56	1576.30
51	405.93	1578.74
52	410.26	1581.23
53	414.56	1583.78
54	418.83	1586.38
55	423.06	1589.04
56	427.26	1591.76
57	431.43	1594.52
58	435.56	1597.35
59	439.65	1600.22
60	443.70	1603.15
61	447.71	1606.13
62	451.69	1609.16
63	455.63	1612.24
64	459.52	1615.38
65	463.38	1618.56
66	467.19	1621.80
67	470.96	1625.08
68	474.80	1626.73

APPENDIX F

SLOPE STABILITY CALCULATIONS FOR
SURFICIAL SLIP SURFACES

Written by: PJS Date: 98 / 12 / 3 Reviewed by: _____ Date: ____ / ____ / ____
YY MM DD YY MM DD
Client: PAO Project: Lake Petit Dam Project/Proposal No.: GL0625 Task No.: 15

STATIC AND SEISMIC STABILITY OF NEAR-SURFACE SOILS

PURPOSE

The purpose of the analyses described in this appendix is to evaluate the static and seismic stability of the near-surface soils on the downstream slope of Lake Petit Dam. The stability analyses consider non-circular wedge-type slip surfaces that extend between adjacent benches on the downstream slope.

METHOD

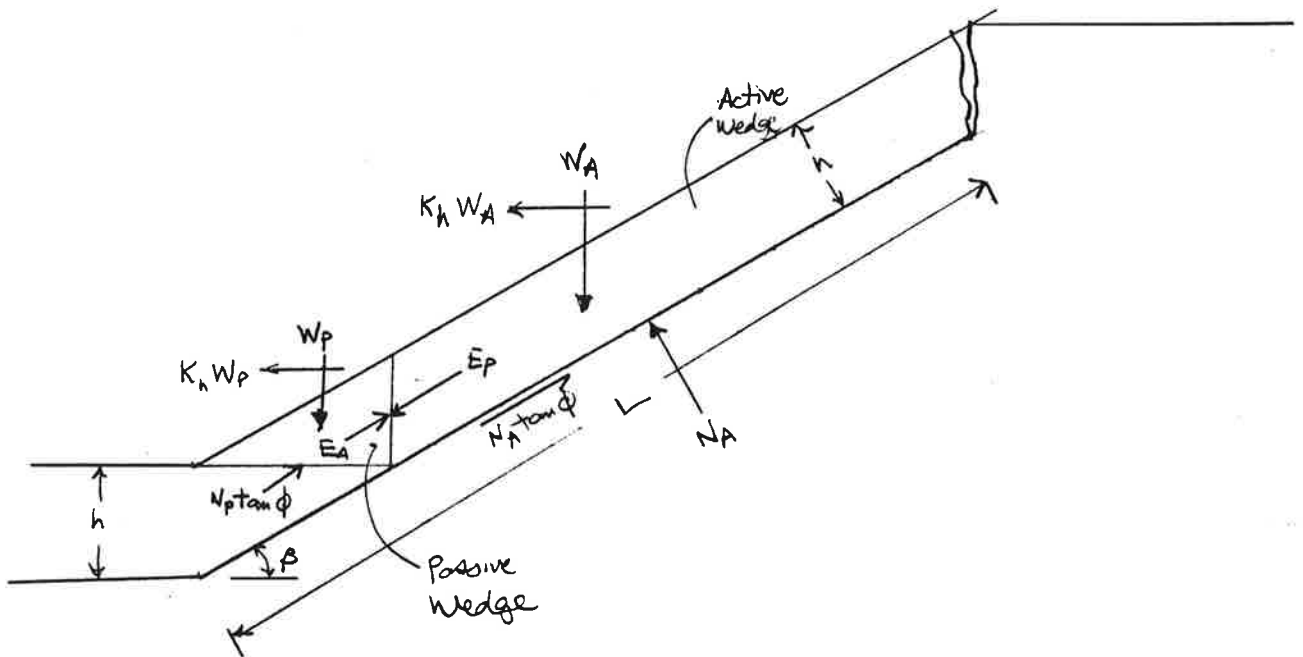
Static and seismic stability were assessed using a two-part wedge analysis. Using the wedge analysis, the static factor of safety and, for seismic stability, the pseudo-static factor of safety is calculated. For the seismic stability analysis, the seismic coefficient is applied as a horizontal force to the potential sliding mass. Herein, analyses of the post-rehabilitation design are performed in which it is assumed that there is no water flow within 3 Ft (1 m) of the slope surface. The analyses presented are based on Koerner and Soong (1998).



Written by: PJS Date: 98 / 12 / 3 Reviewed by: _____ Date: ____ / ____ / ____
YY MM DD YY MM DD

Client: PAO Project: Lake Petitt Dam Project/Proposal No.: GL0625 Task No.: 15

The figure below illustrates a uniform thickness of surficial soil in-between adjacent vertical benches. It includes a passive wedge at the toe and a tension crack at the crest. The analysis herein assumes that sliding occurs on a plane parallel to the surface of the slope located 3 ft below the slope face. It is also assumed that the soil has no cohesive strength, i.e., $c=0$.



Written by: PJS Date: 08 / 12 / 3 Reviewed by: _____ Date: ____ / ____ / ____
YY MM DD YY MM DD

Client: PAO Project: Lake Petit Dam Project/Proposal No.: GL0625 Task No.: 15

The symbols used in this figure are defined below:

W_A = total weight of active wedge

W_P = total weight of passive wedge

N_A = effective force normal to the failure plane of the active wedge

N_P = effective force normal to the failure plane of the passive wedge

γ = unit weight of the soil

h = thickness of soil

L = length of slope

K_h = seismic coefficient

β = slope angle

ϕ = friction angle of the soil

E_A = interwedge force acting on the active wedge from the passive wedge

E_P = interwedge force acting on the passive wedge from the active wedge

FS = factor of safety

By balancing forces in the vertical and horizontal direction and setting $E_A = E_P$, the following is obtained for the static stability factor of safety (i.e., $K_h = 0$):

$$a(FS)^2 + b(FS) + c = 0 \quad (\text{Eq. 1})$$

where:

$$a = (W_A - N_A \cos \beta) \cos \beta \quad (\text{Eq. 2})$$

$$b = - \left[(W_A - N_A \cos \beta) \sin \beta \tan \phi + (N_A \tan \phi) \sin \beta \cos \beta + W_P \tan \phi \sin \beta \right] \quad (\text{Eq. 3})$$

$$c = N_A \tan^2 \phi \sin^2 \beta \quad (\text{Eq. 4})$$



Written by: PJS Date: 9B/12/3 Reviewed by: _____ Date: / / Client: PAO Project: Lake Petri Dam Project/Proposal No.: GLO625 Task No.: 15

The resulting FS value is obtained by solving the quadratic equation:

$$FS = \frac{-b + \sqrt{b^2 - 4ac}}{2a} \quad (\text{Eq. 5})$$

For the pseudo-static FS, a similar development is used which results also in a quadratic equation:

$$a (FS)^2 + b (FS) + c = 0 \quad (\text{Eq. 6})$$

where $a = (K_h W_A + N_A \sin \beta) \cos \beta + K_h W_p \cos \beta \quad (\text{Eq. 7})$

$$b = - \left[(K_h W_A + N_A \sin \beta) \sin \beta \tan \phi + (N_A \tan \phi \cos^2 \beta) + W_p \tan \phi \cos \beta \right] \quad (\text{Eq. 8})$$

$$c = N_A \tan^2 \phi \cos \beta \sin \beta \quad (\text{Eq. 9})$$

The resulting FS is also calculated according to

$$FS = \frac{-b + \sqrt{b^2 - 4ac}}{2a} \quad (\text{Eq. 10})$$

For both analyses, the following forces are used

$$W_A = \gamma h^2 \left(\frac{L}{h} - \frac{1}{\sin \beta} - \frac{\tan \beta}{2} \right) \quad (\text{Eq. 11})$$

$$N_A = W_A \cos \beta \quad (\text{Eq. 12})$$

$$W_p = \frac{\gamma h^2}{\sin \beta} \quad (\text{Eq. 13})$$



Written by: DJS Date: 98 / 12 / 3 Reviewed by: _____ Date: / /
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 Client: PAD Project: Lake Ret + Dam Project/Proposal No.: GL0625 Task No.: 15

PARAMETERS

For the static and seismic analyses of the post-rehabilitation design, the following parameters were used:

- $\gamma = 125 \text{ pcf}$
- $L = 53.8 \text{ ft}$ (length of slope at 2:5H:1V between benches spaced 20' vertical)
- $\beta = 21.8^\circ$
- $\phi = 34^\circ$
- $K_h = 0.183$

RESULTS

• Static

$$W_A = (125 \text{ pcf} \times 3 \text{ ft})^2 \left(\frac{53.8}{3} - \frac{1}{\sin 21.8} - \frac{\tan 21.8}{2} \right) = 16,921 \quad \text{(Eq. 11)}$$

$$N_A = 16,921 \cos 21.8 = 15,711 \quad \text{(Eq. 12)}$$

$$W_p = \frac{(125)(3)^2}{8 \sin 2(21.8)} = 1632 \quad \text{(Eq. 13)}$$

$$a = (16,921 - 15,711 \cos 21.8) \cos 21.8 = 2,167 \quad \text{(Eq. 2)}$$

$$b = - \left[(16,921 - 15,711 \cos 21.8) \sin 21.8 \tan 34^\circ + (15,711 \tan 34^\circ) \sin 21.8 \cos 21.8 + 1632 \tan 34^\circ \sin 21.8^\circ \right] = -4647 \quad \text{(Eq. 3)}$$

$$c = 15,711 \tan^2 34^\circ \sin^2 21.8^\circ = 986 \quad \text{(Eq. 4)}$$

$$FS = \frac{4647 + \sqrt{(-4647)^2 - 4(2167)(986)}}{2(2167)} \quad \text{(Eq. 5)}$$

$FS = 1.90$

A factor of safety of 1.90 exceeds the target minimum static factor of safety of 1.5.



Written by: PJS Date: 98 / 12 / 3 Reviewed by: _____ Date: ____ / ____ / ____
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 Client: PAO Project: Lake Petit Dam Project/Proposal No.: GL0625 Task No.: 15

• Pseudo-Static

$$W_A = 16,921$$

$$N_A = 15,711$$

$$W_P = 1,632$$

$$a = (0.183(16,921) + 15,711 \sin 21.8) \cos 21.8 + 0.183(1,632) \cos 21.8^\circ$$

$$= 8,569 \quad (\text{Eq. 7})$$

$$b = - \left[(0.183)16,921 + 15,711 \sin 21.8 \right] \sin 21.8 \tan 34^\circ +$$

$$(15,711 \tan 34^\circ \cos^2 21.8) + 1,632 \tan 34^\circ \cos 21.8^\circ = -12,395 \quad (\text{Eq. 8})$$

$$c = 15,711 \tan^2 34^\circ \cos 21.8^\circ \sin 21.8^\circ = 2,465 \quad (\text{Eq. 9})$$

$$FS = \frac{12,395 + \sqrt{(12,395)^2 - 4(8,569)(2,465)}}{2(8,569)} \quad (\text{Eq. 10})$$

$$FS = 1.21$$

A factor of safety of 1.21 exceeds the target minimum pseudo-static factor of safety of 1.1.

REFERENCES

Koerner, R.M. and Soong, T.Y. (1998) "Analysis and Design of Veneer Cover Soils", Proceedings of the 6th International Conference on Geosynthetics, March, Atlanta, Georgia, USA

